Application Specific Discretes

## FEATURES

. VERY WIDE TEMPERATURE RANGE: tube ignition from -30 to $+85^{\circ} \mathrm{C}$
. SINGLE SHOT IGNITION FROM -30 to $0^{\circ} \mathrm{C}$ : 350mA, 1350V striking pulse
VERY WIDE POWER RANGE:
Fluorescent tube lamp ignition from 18 to 70W
. EFS2B driver compatible with $50 / 60 \mathrm{~Hz}$ operation
SELECTABLE PREHEAT TIME:
EFS2A driver: 1.5 s or $\mathbf{2 . 5 6 s}(50 \mathrm{~Hz})$
EFS2B driver: 0.74s or $1.24 \mathrm{~s}(50 \mathrm{~Hz})$
EFS2B driver: 0.62 s or $1.03 \mathrm{~s}(60 \mathrm{~Hz})$
. 8 STRIKING PULSES CAPABILITY:
for very cold environment or ageing lamp
. STARTER SHUTDOWN WITH FAILED LAMP

## BENEFITS

. Very low component count: 2 chips + 7 passive components
. Meet EN55015 standards WITHOUT EMI capacitor
. Extended life time of the fluorescent lamp due to smooth and single shot ignition
. High inherent reliability and extended life time of the starter

## DESCRIPTION

The EFS Kit is a 2 chips set used with 7 additional passive components, for Glow switch Starter.
The ASD ${ }^{\text {T }}$ (Application Specific Discretes) includes a bi-directional Power Switch and a Power Supply for the driver.
The driver provides a program to ensure a fully optimised linear fluorescent lamp ignition.

PIN CONNECTION (top view)

| SO14 |  |  |  |  | Pentawatt HV |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| State tube detection 1 <br> Preheat select 24 <br> to be grounded 3 <br> Shunt 4 <br> to be grounded 5 <br> to be grounded 65 <br> to be grounded 75 |  | - b | 14 | G1 |  |  |  |  |
|  |  | a | 13 | G2 | Voc 2 | $\square$ |  |  |
|  |  | $\square$ | 12 | Vcc | Tube 3 |  |  | $\bigcirc$ |
|  |  | $\square$ | 11 | GND |  |  |  | $\bigcirc$ |
|  |  | , | 10 | to be grounded | GND G 2 $4^{4}$ | $=$ |  |  |
|  |  |  | 9 | DO NOT CONNECT |  |  |  |  |
|  |  |  | 8 | to be grounded |  |  |  |  |
| DRIVER: EFS2A-CD and :EFS2B-CD |  |  |  |  | ASD ${ }^{\text {TM }}$ : EFS21-TL5 |  |  |  |
|  |  |  |  |  |  |  |  |  |

EFS STARLIGHT-KIT PARTS SELECTION:
The EFS STARLIGHT-KIT answers effectively to linear fluorescent lamp ignition needs:

|  | MAINS FREQUENCY |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 50 Hz |  |  |  | 60 Hz |  |
| DRIVER VERSION | EFS2A |  | EFS2B |  |  |  |
| Pin 2 connection | GND | VCC | GND | VCC | GND | VCC |
| PREHEAT DURATION | 1.5 s | 2.56s | 0.74s | 1.24s | 0.62s | 1.03s |
| ASD ${ }^{\text {¹ }}$ | EFS21 |  |  |  |  |  |
| LAMP POWER RANGE | 18 to 70W (note 2) |  |  |  |  |  |
| AMBIENT TEMPERATURE RANGE | -30 to $85^{\circ} \mathrm{C}$ (note1, note 2) |  |  |  |  |  |

Note 1: below $-20^{\circ} \mathrm{C}$, it is recommended to limit the lamp power range to 58 W .
Note 2: the ignition temperature range is given with starting aid, as required in the IEC 81 and IEC 926 (§6.3.1) standards.

BASIC APPLICATION DIAGRAM


## RECOMMENDED LAMP POWER RANGE APPLICATION



Note 2: the ignition temperature range is given with starting aid, as required in the IEC 81 and IEC 926 (§6.3.1) standards.

ABSOLUTE RATINGS (limiting values)

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| Top | Operating Junction temperature range | -30 to +125 | ${ }^{\circ} \mathrm{C}$ |
| Tstg | Storage temperature range | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |

DRIVER: EFS2 A \& EFS2B

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| Vcc | Maximum supply voltage | 14 | V |
| Ptot | Power dissipation | 500 | mW |
| ESD | Electrostatic discharge between any pins <br> Standard: MIL STD 883C Human Body Model | 1 | kV |
| VSENSE | Input operating range | $\pm 10$ | V |

ASD ${ }^{\text {TM }}$ : EFS21

| Symbol | Parameter | Value | Unit |
| :---: | :---: | :---: | :---: |
| $\mathrm{IT}_{\text {(RMS }}$ | RMS on-state current Tcase $=90^{\circ} \mathrm{C}$ | 1 | A |
| Tcase | $\mathrm{I}_{\text {(RMS })}=1 \mathrm{~A} \quad$ toFF $=0.16 \mathrm{~s} \quad \mathrm{t}_{\text {ON }}=0.75 \mathrm{~s}$ | + 120 | ${ }^{\circ} \mathrm{C}$ |
| ITSM | Surge peak on-state current <br> $\mathrm{T}_{\mathrm{j}}$ initial $=25^{\circ} \mathrm{C}, \mathrm{tp}=10 \mathrm{~ms}$ <br> Minimum repetitive rate periode : 1 min . | 15 | A |
| VDRM <br> VRRM | Repetitive peak off-state voltage | 600 | V |

EFS
ELECTRICAL CHARACTERISTICS $\left(\mathrm{T}_{\mathrm{j}}=25^{\circ} \mathrm{C}\right.$, unless otherwise specified)
DRIVER

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vcc | Supply voltage in preheat mode | 7 |  | 12 | V |
| VuvLO | Under voltage lock-out threshold |  |  | 5 | V |
| $\mathrm{V}_{\text {CCH }}$ | Supply limitation high in standby mode | 6.8 | 7.7 | 8.7 | V |
| $\mathrm{V}_{\text {CCL }}$ | Supply limitation low in standby mode | 6.77 | 7.57 | 8.41 | V |
| Icc | Supply current in standby mode | 440 | 450 | 475 | $\mu \mathrm{A}$ |
| Iso | Ignition current level Rsense $=0.39 \Omega$ | 280 | 350 | 420 | mA |
| LAMP OFF STATE DETECTION |  |  |  |  |  |
| tc | Checking delay after zero crossing lamp voltage |  |  |  |  |
|  | EFS2A version | 2.9 |  | 5.9 | ms |
|  | EFS2B version | 2.5 |  | 7.5 | ms |
| $\mathrm{V}_{\text {REF }}$ | Internal reference voltage | 1.12 |  | 1.26 | V |

ASD

| Symbol | Parameter | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VT + | Positive on-state voltage $\quad \mathrm{I}_{\mathrm{T}}=1.5 \mathrm{~A} \quad \mathrm{tp}=500 \mu \mathrm{~s}$ |  | 2.1 | 3.15 | V |
| VT - | Negative on-state voltage $\mathrm{I}_{\mathrm{T}}=1.5 \mathrm{~A} \quad \mathrm{tp}=500 \mu \mathrm{~s}$ |  | 0.89 | 1.2 | V |
| $V_{\text {BR }}$ | Breakdown positive voltage $l_{\text {DRM }}=5 \mathrm{~mA} \quad \mathrm{t}_{\mathrm{p}}=10 \mathrm{~ms}$ | 1200 | 1350 | 1500 | V |
| $V_{\text {DCM }}$ <br> $V_{\text {RCM }}$ | Non repetitive peak off-state voltage <br> Pin $1=\operatorname{Pin} 2=\operatorname{Pin} 4=\operatorname{Pin} 5$ Repetitive rate : 3 Hz | 800 |  |  | V |
| $\begin{aligned} & \begin{array}{l} \text { IDRM } \\ \text { IRRM } \end{array} \end{aligned}$ | Leakage current, at $V_{\text {DRM }} / V_{\text {RRM }}$ rated $\operatorname{Pin} 1=\operatorname{Pin} 2=\operatorname{Pin} 4=\operatorname{Pin} 5$ |  |  | 20 | $\mu \mathrm{A}$ |
| $\mathrm{IH}_{\mathrm{H}}$ | Holding current $\mathrm{d} / \mathrm{dt}=9 \mathrm{~A} / \mathrm{ms}$ $\operatorname{Pin} 1=\operatorname{Pin} 2=\operatorname{Pin} 4=\operatorname{Pin} 5$ | 350 |  |  | mA |

ORDERING INFORMATION


| ASD $^{\text {TM }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| EFS | $\boldsymbol{2}$ | $\mathbf{1}$ | $\frac{\text { TL5 }}{\square}$ |  |
| Electronic <br> Fluorescent <br> Switch | Kit | Version <br> Digit | TL5: <br> Pentawatt HV Package <br> with lead forming |  |

DEMONSTRATION BOARD DIAGRAM


When the starter has to be protected against over-temperature, over-current or short circuit, it is recommended to implement a thermal fuse in series with the starter.
To meet (IEC 926) standards, a capacitor (f.i. 5nF) can be connected between pin 3 and pin 4 of the ASD.

BOARD ASSEMBLY


PCB with Pentawatt HV and SO14

DRILL and CUT the track
for SHORT preheat -->
for LONG preheat -->

Pin 2 is the preheat time select pin. To select a short preheat time, drill to cut the Vcc to pin 2 track at the metallic hole. To select a long preheat time, drill to cut the GND to pin 2 track. The layout must be configured for either choice to avoid supply short circuit.

## RECOMMENDED COMPONENTS ACCORDING TO APPLICATION CONDITIONS

| Application Conditions |  |  |  |
| :---: | :---: | :---: | :---: |
| AC mains | $\begin{gathered} \text { Single } \\ 230 \mathrm{~V}-50 \mathrm{~Hz} \end{gathered}$ | $\begin{gathered} \text { Single } \\ 120 \mathrm{~V}-60 \mathrm{~Hz} \end{gathered}$ | Twin series $230 \mathrm{~V} / 50 \mathrm{~Hz}$ or single $115 \mathrm{~V} / 50 \mathrm{~Hz}$ |
| Lamp Power Range | 18 to 70W |  | 18 to 36W |
| Ambient Temperature Range | -30 to $+85^{\circ} \mathrm{C}$ (note 3) |  |  |
| Recommended Components |  |  |  |
| ASD version | EFS21 |  |  |
| Driver version | EFS2A or EFS2B | EFS2B | EFS2A or EFS2B |
| R1, R2 | 30k $\Omega$ - 0.125W-5\% | 15k $\Omega-0.125 \mathrm{~W}-5 \%$ |  |
| R3 | 130k $\Omega$-0.125W-5\% |  |  |
| R4 | 2.2k $\Omega-0.25 \mathrm{~W}-5 \%$ | 3.3k $\Omega-0.25 \mathrm{~W}-5 \%$ |  |
| R5 | 0.39 $2-0.25 \mathrm{~W}-5 \%$ (note 4) |  |  |
| R6 | 0.39k $\Omega-0.25 \mathrm{~W}-5 \%$ |  |  |
| C1 | $22 \mu \mathrm{~F}$ - $16 \mathrm{~V}-20 \%$ |  |  |
| C2 | BYD17K (800V) |  |  |

Note 3: below $-20^{\circ} \mathrm{C}$, it is recommended to limit the lamp power range to 58 W .
Note 4: R5(Rsense) should have a 8 A, 10 ms surge capability.

## EFS STARLIGHT-KIT APPLICATION NOTE

## 1/ THE AC POWER SWITCH: FUNCTIONAL DESCRIPTION

he Starter is a bi-directional switch which performs two functions:
. the preheat of the tube,
. the ignition of the tube.


The mains voltage is applied


Preheating of the tube


Striking of the tube

During the preheat period, the $A S D^{\text {тм }}$ is fully conducting. The tube lamp is short circuited by the starter, and the current flows through its filaments. In these conditions, the lamp can not light up, but the temperature of the lamp electrodes increases.
At the end of the preheat period, lamp filaments are warm enough to emit electrons in the gas and to permit the lamp ignition in good conditions. The ASD ${ }^{\text {TM }}$ switches off the preheating current. At this moment, the ballast is equivalent to a current generator ( $\mathrm{I}=\mathrm{I}$ so, Iso $=$ Switched Off current). As the ASD ${ }^{\text {TM }}$ switches off, the starter voltage increases. The amplitude of this high voltage spike is then clamped by the $\mathrm{ASD}^{\mathrm{TM}}\left(\mathrm{V}_{\mathrm{BR}}{ }^{\prime} 1350 \mathrm{~V}\right)$. As the starter and the lamp are in parallel, the striking pulse is directly applied to the lamp. The electromagnetic energy of the ballast is then discharged through the lamp and the ASDT.

## 2/ WHAT'S NEW IN THIS SWITCH?

The AC SWITCH merges an auxiliary power supply for the driver, a power clamping device (1350V) and a bi-directional switch with his execution pilot block.

## Striking pulse



NEW EFS ASD


Present solutions work with a unidirectional switch, like MOS transistors or GTO (Gate Turn Off thyristor). As a starter is a bi-directional switch, it is necessary to use a rectifier bridge ( 4 diodes of 1500 V ). More, 2 or 3 diodes in series with the GTO are required to get the necessary switch off effect, and the whole is controlled with an analog timer built around a small SCR.
The interest of a bi-directional switch arises itself: a drastic reduction of the number of components, and of course, a reduction of power losses (only 1 forward voltage instead of 5).

Conventional discrete circuit (minimal version)


## 3/ LAMP IGNITION FEATURE:

A lamp requires a minimum energy level to be ignited, but this energy depends especially on the lamp temperature. The lower the temperature is, the more energetic the lamp strike is.
This energy stored in the ballast is directly proportional to the Switched Off current $I_{\text {SO }}\left(E=\frac{L . I_{S O}}{2}\right)$.
In other words, the required energy and of course the Iso level, are maximum for the minimum temperature. Results based on experiments show that it is necessary to switch off a current of 350 mA to strike a 58 W tube at $-30^{\circ} \mathrm{C}$ (with a voltage amplitude clamped at 1200 V and starting aid).
Therefore, the best way to strike a tube independently of the temperature is to keep the maximum Iso level for all the temperature range. Unfortunately, the solution is not so simple to implement because the energy level at ambient or warm temperature would be much important: the lamp would be ignited, but the lamp lifetime would be shortened. This is why one of the innovations of the ASD ${ }^{\text {TM }}$ is to modulate the striking energy versus temperature (see feature hereafter).


For freezing temperatures, the $I_{s o}$ level is maintained at 350 mA , and for positive temperatures, the $I_{\text {so }}$ level decreases slowly.

## 4/ AUXILIARY POWER SUPPLY:

In order to reduce the number of components, an auxiliary power supply is integrated in the ASD ${ }^{\text {TM }}$. This active power supply works directly on the mains and requires only a low voltage capacitor $16 \mathrm{~V}-22 \mu \mathrm{~F}$. The operating mode of this supply varies with the starter operating phase:

## POWER SUPPLY SCHEMATIC



## Supply operation during preheat phase:

During preheat phase, the driver manages alone the supply function (neither the driver nor D1 and R6 are involved). A part of the current flowing through the ASD ${ }^{\text {TM }}$ is used, at the beginning and at the end of each positive mains half cycle, to charge the output capacitor.

## Supply operation during standby phase:

When the lamp is lit, the monitors its supply voltage ( Vcc ). At the beginning of each positive mains half cycle, when Vcc is lower than 7.57 V , the driver closes the ASD ${ }^{\text {TM }}$ supply switch. The capacitor is charged to provide the standby current of the driver. During this phase the tube lamp is short circuited by the ASD ${ }^{\text {TM }}$. When the supply voltage reaches 7.68 V , the driver opens the ASD ${ }^{\text {TM }}$ supply switch. Since this current is also flowing in the ballast, the supply turn off provides across the lamp an additional voltage spike. After running few minutes the lamp becomes warm and this spike voltage naturally decreases.

SUPPLY DURING PREHEAT PHASE


SUPPLY DURING STANDBY PHASE
(Without E.M.I. Capacitor nor R6 nor D1)


To reduce dramatically this repetitive voltage spikes across the lamp, the R6 resistor with the diode D1 provide a part of the supply current. Thus, the ripple voltage of the supply voltage is reduced, as well as the level of the switched off current. On the other hand, this increases the safety margin of the RF noise (versus the IEC 55015 limits)

## 5/ THE DRIVER: FUNCTIONAL DESCRIPTION

## EFS2A DRIVER Internal block diagram (50Hz operation)



## ALGORITHM

## 1. At switch on:

At switch on, an integrated Under Voltage Lock Out function (UVLO) resets the driver as long as the supply voltage stays below a safety level.

## 2. Preheat:

The ignition sequence begins with the preheat phase. Two different duration's can be selected with PIN 2 (see table EFS STARLIGHT-KIT PARTS SELECTION page 2).
During this phase, the driver maintains the ASDTM in a full ON-state making the starter equivalent to a bi-directional conducting switch.

## 3. Ignition of the fluorescent tube:

At the end of the preheat period, the starter strikes the fluorescent lamp.
For that, the driver reads continuously the current through the starter. When the current reaches the Switch Off level (Iso $=350 \mathrm{~mA}$ ), the driver turns off the ASDTM. This induces a high voltage pulse across the lamp. This pulse amplitude is limited by the ASDTM ('1350V).

## 4. If the lamp fails to strike:

The driver detects the state of the tube (lit or off). If it stays off during 8 mains cycles (loop 1), a new preheat period, shorter than the first one, starts again (loop 3), followed by a new ignition attempt.


* see the preheat duration table § 6 The driver will try to fire the tube 8 times. If none of the 8 attempts succeeds in striking the lamp, the driver turns in standby mode, and the whole starter is fully stopped until the next mains removal and power supply reset.


## 5. If the lamp is ignited:

If the lamp is ignited, the driver stays in standby mode while monitoring the state of the lamp (loop 2). During normal operation of the tube, this short pulse is masked by the lamp conduction. If the mains interruption is really long enough to turn off completely the lamp, a new ignition sequence starts again (loop 3) with 8 other new possible attempts.

## 6/ PREHEAT PHASE DURATION $50-60 \mathrm{~Hz}$ :

The driver determines the preheat duration by counting mains cycles. This numeric solution brings naturally a good precision depending only on the mains frequency tolerance.

With the 2 driver versions, the EFS startlight-kit provides a choice of 4 preheat duration's. The following table gives the preheat duration before the first ignition attempt. The seven next preheat duration's, in case of unsuccessful ignition attempt, last the half of the first one

|  | PREHEAT DURATION |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| MAINS FREQUENCY | 50 Hz |  |  |  | 60 Hz |  |
| DRIVER VERSION | EFS2A |  | EFS2B |  | EFS2B |  |
| Pin 2 connection | GND | VCC | GND | VCC | GND | VCC |
|  | 1.5 s | 2.56 s | 0.74 s | 1.24 s | 0.62 s | 1.03 s |

## 7/ TUBE STATE DETECTION:

During the ignition sequence or once the lamp is lit, the starter checks the state of the lamp (lit or off). To determine this state, the driver reads the lamp voltage through the resistor bridge ( $R 1+R 2+R 3, R 4$ ).

- If the lamp is off, its voltage equal the mains voltage.
- If the lamp is lit, its voltage is only 80 V (for a 58 W lamp).

Thus the lamp state is determined by comparison of the lamp voltage with a programmed detection level.

## Tolerance effects:

Tolerances on resistors (R1, R2, R3 and R4) as well as on the integrated comparator bring a tolerance on the set detection level. Thus the detection level is included in a range delimited by the maximum and the minimum detection levels (DLmax DLmin)

The driver checks the state of the lamp when mains voltage is maximum, that is to say 5 ms after the zero crossing mains voltage $(50 \mathrm{~Hz})$. Here again internal tolerances bring a tolerance on the real checking moment (TCmin TCmax).

CORRECT SETTING = NO WAVEFORM ACROSS THE GREY AREA


## How to set the detection level?

Only the R4 resistor value can be set to adjust the detection level. Values of resitors R1 to R3 must match values of the table RECOMMENDED COMPONENTS ACCORDING TO APPLICATION CONDITIONS of the page 5. Practically the R4 resistor value has to be set so that neither the OFF lamp voltage nor the LIT lamp voltage cross the grey area.
The DLmax and DLmin limits can be calculated as follows:
$D L_{\text {MAX }}=\frac{1.265 \times\left(R 4_{\text {min }}+R 1_{\text {max }}+R 2_{\text {max }}+R 3_{\text {max }}\right)}{R 4_{\text {min }}}$ and $D L_{\text {min }}=\frac{1.122_{x\left(R 4_{\text {mAX }}+R 1_{\text {min }}+R 2_{\text {min }}+R 3_{\text {min }}\right)}^{R 4_{\text {max }}}}{\text { m }}$

## 8/ E.M.I. CAPACITOR:

As required in the IEC 926 standard (§11.5), "starters which are interchangeable with glow starters in accordance with IEC 155 shall contain means for radio interference suppression, the effect of which is equivalent to that of the radio interference suppression capacitor prescribed in 7.12 of IEC 155".

The EFS starlight-kit is compatible with this $5 n F$ E.M.I. Capacitor which must be connected directly across the ASD ${ }^{\text {TM }}$ (between pin 3 "TUBE" and pin 4 "GND").
On the other hand, this E.M.I. capacitor increases the striking pulse width of about $55 \%$ on positive temperatures.


### 8.1. Operation in single lamp configuration

The EFS STARLIGHT-KIT is ideal in the following configurations:

- Single Starter / 230V / 50Hz - Single Starter / 230V / 60Hz - Single Starter / 120V / 60Hz


Note 4: the different driver versions should be chosen according to the table "EFS STARLIGHT KIT PARTS SELECTION" page 2.
Note 5: Components to choose are listed in the table "RECOMMENDED COMPONENTS ACCORDING TO APPLICATION CONDITIONS" page 5.

### 8.2. Operation with capacitor for power factor correction:

The EFS STARLIGHT-KIT is also suitable for magnetic ballast including front end parallel capacitor.
The EFS STARLIGHT-KIT is NOT suitable for magnetic ballast including front end serial capacitor.

## LEADING MAGNETIC BALLAST WITH SERIAL CAPACITOR



## MAGNETIC BALLAST WITH SHUNT PARALLEL CAPACITOR



## EFS

### 8.3. Operation on the $230 \mathrm{~V} / 50 \mathrm{~Hz}$ AC mains in twin tubes configuration

The EFS STARLIGHT-KIT is also suitable for the configurations Twin tubes Starter
Note 5: Components to choose are listed in the table "RECOMMENDED COMPONENTS ACCORDING TO APPLICATION CONDITIONS" page 5.
The only electrical diagram difference consists of the R4 resistor which needs to be changed from 1 to $2.2 \mathrm{k} \Omega$. Without this modification, the starter will generate only one ignition attempt instead of 8 in case of defective lamp; the loop 3 is removed from the algorithm described in page 9.


In the Twin Series $230 \mathrm{~V} / 50 \mathrm{~Hz}$ configuration, the polarity of the two starters must be respected:
In case of no operation of starters, rotate one of the starters of $180^{\circ}$ on its socket.

PACKAGE MECHANICAL DATA
SO14 (Driver)

|  |  |  | limete |  |  | nches |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dim. | Min. | Typ. | Max. | Min. | Typ. | Max. |
|  | A |  |  | 1.75 |  |  | 0.069 |
| $\rightarrow \longrightarrow$ | a1 | 0.1 |  | 0.2 | 0.004 |  | 0.008 |
| c. $入^{\text {c1 }}$ | a2 |  |  | 1.6 |  |  | 0.063 |
|  | b | 0.35 |  | 0.46 | 0.014 |  | 0.018 |
|  | b1 | 0.19 |  | 0.25 | 0.007 |  | 0.010 |
| e3 | C |  | 0.5 |  |  | 0.020 |  |
|  | c1 |  |  | $45^{\circ}$ | typ.) |  |  |
|  | D | 8.55 |  | 8.75 | 0.336 |  | 0.334 |
|  | E | 5.8 |  | 6.2 | 0.228 |  | 0.244 |
|  | e |  | 1.27 |  |  | 0.050 |  |
| $1{ }^{7}$ | e3 |  | 7.62 |  |  | 0.300 |  |
| Uपए | F | 3.8 |  | 4.0 | 0.150 |  | 0.157 |
|  | G | 4.6 |  | 5.3 | 0.181 |  | 0.208 |
|  | L | 0.5 |  | 1.27 | 0.020 |  | 0.050 |
|  | M |  |  | 0.68 |  |  | 0.027 |
|  | S |  |  | $8^{\circ}$ ( | max.) |  |  |

PACKAGE MECHANICAL DATA
Pentawatt HV with lead forming - TL5 (ASDTM)


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