# PWM STEP-UP DC/DC CONVERTER RH5RH $\times \times 1$ A $/ \times \times 2 B / \times \times 3 B$ SERIES 

## APPLICATION MANUAL

## RH5RH $\times \times 1$ A/ $\times \times 2$ B $/ \times \times 3$ B SERIES

## OUTLINE

The RH5RH $\times \times 1 \mathrm{~A} / \times \times 2 \mathrm{~B} / \times \times 3$ B Series are PWM Step-up DC/DC converter ICs by CMOS process.
The RH5RH $\times \times 1$ A IC consists of an oscillator, a PWM control circuit, a driver transistor (Lx switch), a reference voltage unit, an error amplifier, a phase compensation circuit, resistors for voltage detection, a soft-start circuit, and an Lx switch protection circuit. A low ripple, high efficiency step-up DC/DC converter can be constructed of this RH5RH $\times \times 1$ A IC with only three external components, that is, an inductor, a diode and a capacitor.

These RH5RH $\times \times 1 \mathrm{~A} / \times \times 2 \mathrm{~B} / \times \times 3$ B ICs can achieve ultra-low supply current (no load) -TYP. $15 \mu \mathrm{~A}$-by a newly developed PWM control circuit, equivalent to the low supply current of a VFM (chopper) Step-up DC/DC converter.

Furthermore, these ICs can hold down the supply current to TYP. $2 \mu \mathrm{~A}$ by stopping the operation of the oscillator when the input voltage $>$ (the output voltage set value + the dropout voltage by the diode and the inductor).

These $\mathrm{RH} 5 \mathrm{RH} \times \times 1 \mathrm{~A} / \times \times 2 \mathrm{~B} / \times \times 3 \mathrm{~B}$ Series ICs are recommendable to the user who desires a low ripple PWM $\mathrm{DC} / \mathrm{DC}$ converter, but cannot adopt a conventional PWM DC/DC converter because of its too large supply current.

The RH5RH $\times \times 2$ B/ $\times \times 3$ B Series ICs use the same chip as that employed in the RH5RH $\times \times 1 \mathrm{~A}$ IC and are provided with a drive pin (EXT) for an external transistor. Because of the use of the drive pin (EXT), an external transistor with a low saturation voltage can be used so that a large current can be caused to flow through the inductor and accordingly a large output current can be obtained. Therefore, these RH5RH $\times \times 2 B / \times \times 3 B$ Series ICs are recommendable to the user who need a current as large as several tens mA to several hundreds mA .

The RH5RH $\times \times 3$ B IC also includes an internal chip enable circuit so that it is possible to set the standby supply current at MAX. $0.5 \mu \mathrm{~A}$.

These RH5RH $\times \times 1 \mathrm{~A} / \times \times 2 \mathrm{~B} / \times \times 3$ B ICs are suitable for use with battery-powered instruments with low noise and low supply current.

## FEATURES

- Small Number of External Components ..........Only an inductor, a diode and a capacitor (RH5RH $\times \times 1 \mathrm{~A})$
-Low Supply Current..........................................TYP. 15 1 A (RH5RH301A)
- Low Ripple and Low Noise
- Low Start-up Voltage (when the output current is 1 mA ) ..................MMAX. 0.9 V
- High Output Voltage Accuracy $\cdots \cdots . . . . . . . . . . . . . . . . . . . . . . ~ \pm 2.5 \% ~$
- High Efficiency ............................................................... 85P.
- Low Temperature-Drift Coefficient of Output Voltage .....................TTYP. $\pm 50 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Soft-Start…........................................................MIN. 500 H
-Small Packages .................................................SOT-89 (RH5RH $\times \times 1$ A, RH5RH $\times \times 2$ B), SOT-89-5 (RH5RH $\times \times 3 \mathrm{~B}$ )


## APPLICATIONS

- Power source for battery-powered equipment.
- Power source for cameras, camcorders, VCRs, PDAs, electronic data banks, and hand-held communication equipment.
- Power source for instruments which require low noise and low supply current, such as hand-held audio equipment.
- Power source for appliances which require higher cell voltage than that of batteries used in the appliances.


## RH5RH

## BLOCK DIAGRAM



Error Amp．（Error Amplifier）has a DC gain of 80dB，and Phase Comp．（Phase Compensation Circuit） provides the frequency characteristics including the 1 st pole（ $\mathrm{fp}=0.25 \mathrm{~Hz}$ ）and the zero point（ $\mathrm{fz}=2.5 \mathrm{kHz}$ ）． Furthermore，another zero point（ $\mathrm{fz}=1.0 \mathrm{kHz}$ ）is also obtained by the resistors and a capacitor connected to the OUT pin．
（Note）Lx Pin ．．．．．．．．．．．．only for RH5RH $\times \times 1$ A and RH5RH $\times \times 3$ B
EXT Pin $\cdots \cdots \cdot$ only for RH5RH $\times \times 2$ B and RH5RH $\times \times 3$ B
$\overline{\text { CE Pin }} \cdots \cdots \cdots \cdot$ only for RH5RH $\times \times 3 \mathrm{~B}$

## SELECTION GUIDE

In RH5RH Series，the output voltage，the driver，and the taping type for the ICs can be selected at the user＇s request．The selection can be made by designating the part number as shown below ：


| Code | Description |
| :---: | :---: |
| a | Setting Output Voltage（Vout）： <br> Stepwise setting with a step of 0.1 V in the range of 2.7 V to 7.5 V is possible． |
| b | Designation of Driver： <br> 1A：Internal Lx Tr．Driver（Oscillator Frequency 50 kHz ） <br> 2B：External Tr．Driver（Oscillator Frequency 100 kHz ） <br> 3B：Internal Tr．／External Tr．（selectively available）（Oscillator Frequency 100kHz，with chip enable function） |
| c | Designation of Taping Type ： <br> Ex．SOT－89 ：T1，T2 <br> SOT－89－5 ：T1，T2 <br> （refer to Taping Specifications） <br> ＂T1＂is prescribed as a standard． |

For example，the product with Output Voltage 5．0V，the External Driver（the Oscillator Frequency 100 kHz ） and Taping Type T1，is designated by Part Number RH5RH502B－T1．

## PIN CONFIGURATION

- SOT-89

-SOT-89-5



## PIN DESCRIPTION

| Pin No. |  |  | Symbol | Description |
| :---: | :---: | :---: | :---: | :---: |
| $\times \times 1 \mathrm{~B}$ | $\times \times 2 \mathrm{~B}$ | $\times \times 3$ B |  |  |
| 1 | 1 | 5 | Vss | Ground Pin |
| 2 | 2 | 2 | OUT | Step-up Output Pin, Power Supply (for device itself) |
| 3 | - | 4 | Lx | Switching Pin (Nch Open Drain) |
| - | 3 | 3 | EXT | External Tr. Drive Pin (CMOS Output) |
| - | - | 1 | $\overline{\mathrm{CE}}$ | Chip Enable Pin (Active Low) |

## ABSOLUTE MAXIMUM RATINGS

| Symbol | Item | Rating | Unit | Note |
| :---: | :--- | :--- | :---: | :---: |
| Vout | Output Pin Voltage | +12 | V |  |
| VLX | Lx Pin Voltage | +12 | V | Note1 |
| VEXT | EXT Pin Voltage | -0.3 to VouT +0.3 | V | Note2 |
| VCE | $\overline{\text { CE Pin Voltage }}$ | -0.3 to VouT +0.3 | V | Note3 |
| ILX | Lx Pin Output Current | 250 | mA | Note1 |
| IEXT | EXT Pin Current | $\pm 50$ | mA | Note2 |
| Pd | Power Dissipation | -300 to +80 | mW |  |
| Topt | Operating Temperature Range | -55 to +125 | ${ }^{\circ} \mathrm{C}$ |  |
| Tstg | Storage Temperature Range | $260^{\circ}{ }^{\circ} \mathrm{C}, 10 \mathrm{~s}$ | ${ }^{\circ} \mathrm{C}$ |  |
| Tsolder | Lead Temperature(Soldering) |  |  |  |

(Note 1) Applicable to RH5RH $\times \times 1$ A and RH5RH $\times \times 3$ B. (Note 2) Applicable to RH5RH $\times \times 2$ B and RH5RH $\times \times 3$ B.
(Note 3) Applicable to RH5RH $\times \times 3 \mathrm{~B}$.

## ABSOLUTE MAXIMUM RATINGS

Absolute Maximum ratings are threshold limit values that must not be exceeded even for an instant under any conditions. Moreover, such values for any two items must not be reached simultaneously. Operation above these absolute maximum ratings may cause degradation or permanent damage to the device. These are stress ratings only and do not necessarily imply functional operation below these limits.

## ELECTRICAL CHARACTERISTICS

- RH5RH301A

Vout=3.0V

| Symbol | Item | Conditions | MIN. | TYP. | MAX. | Unit | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vout | Output Voltage |  | 2.925 | 3.000 | 3.075 | V |  |
| Vin | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Start-up Voltage | Iout $=1 \mathrm{~mA}, \mathrm{VIN}$ : $0 \rightarrow 2 \mathrm{~V}$ |  | 0.8 | 0.9 | V |  |
| Vhold | Hold-on Voltage | Iout $=1 \mathrm{~mA}, \mathrm{VIN}: 2 \rightarrow 0 \mathrm{~V}$ | 0.7 |  |  | V |  |
| IdD1 | Supply Current 1 | To be measured at OUT Pin (excluding Switching Current) |  | 15 | 25 | $\mu \mathrm{A}$ |  |
| IdD2 | Supply Current 2 | To be measured at OUT Pin (excluding Switching Current) Vin=3.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| ILX | Lx Switching Current | VLx=0.4V | 60 |  |  | mA |  |
| LLXleak | Lx Leakage Current | VLX=6V,VIN=3.5V |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| fosc | Oscillator Frequency |  | 40 | 50 | 60 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | on (Vlx "L" ) side | 70 | 80 | 90 | \% |  |
| $\eta$ | Efficiency |  | 70 | 85 |  | \% |  |
| tstart | Soft-Start Time | Time required for the rising of Vout up to 3 V . | 0.5 | 2.0 |  | ms | Note1 |
| VLxlim | VLX Voltage Limit | Lx Switch ON | 0.65 | 0.8 | 1.0 | V | Note2 |

Unless otherwise provided, $\mathrm{VIN}=1.8 \mathrm{~V}, \mathrm{VSS}=0 \mathrm{~V}$, IouT $=10 \mathrm{~mA}, \mathrm{Topt}=25^{\circ} \mathrm{C}$, and use External Circuit of Typical Application (FIG. 1).
(Note 1) Soft-Start Circuit is operated in the following sequence :
(1) VIN is applied.
(2) The voltage (Vref) of the reference voltage unit is maintained at OV for about $200 \mu \mathrm{~s}$ after the application of Vin.
(3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
(4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
(Note 2) ILx is gradually increased after Lx Switch is turned ON. In accordance with the increase of ILx, VLx is also increased. When VLx reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.

## RH5RH

－RH5RH501A
Vout $=5.0 \mathrm{~V}$

| Symbol | Item | Conditions | MIN． | TYP． | MAX． | Unit | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vout | Output Voltage |  | 4.875 | 5.000 | 5.125 | V |  |
| Vin | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Start－up Voltage | Iout $=1 \mathrm{~mA}, \mathrm{Vin}: 0 \rightarrow 2 \mathrm{~V}$ |  | 0.8 | 0.9 | V |  |
| Vhold | Hold－on Voltage | Iout $=1 \mathrm{~mA}, \mathrm{Vin}: 2 \rightarrow 0 \mathrm{~V}$ | 0.7 |  |  | V |  |
| IDD1 | Supply Current 1 | To be measured at OUT Pin （excluding Switching Current） |  | 30 | 45 | $\mu \mathrm{A}$ |  |
| IDD2 | Supply Current 2 | To be measured at OUT Pin （excluding Switching Current） VIN=5.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| ILX | Lx Switching Current | $\mathrm{VLX}=0.4 \mathrm{~V}$ | 80 |  |  | mA |  |
| ILXleak | Lx Leakage Current | $\mathrm{VLX}=6 \mathrm{~V}, \mathrm{VIN}=5.5 \mathrm{~V}$ |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| fosc | Oscillator Frequency |  | 40 | 50 | 60 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | on（VLX＂L＂）side | 70 | 80 | 90 | \％ |  |
| $\eta$ | Efficiency |  | 70 | 85 |  | \％ |  |
| tstart | Soft－Start Time | Time required for the rising of Vout up to 5 V ． | 0.5 | 2.0 |  | ms | Note1 |
| VLXlim | VLX Voltage Limit | Lx Switch ON | 0.65 | 0.8 | 1.0 | V | Note2 |

Unless otherwise provided，Vin $=3 \mathrm{~V}, \mathrm{Vss}=0 \mathrm{~V}$ ，IouT $=10 \mathrm{~mA}$ ，Topt $=25^{\circ} \mathrm{C}$ ，and use External Circuit of Typical Application（FIG．1）．
（Note 1）Soft－Start Circuit is operated in the following sequence ：
（1）VIN is applied．
（2）The voltage（Vref）of the reference voltage unit is maintained at 0 V for about $200 \mu \mathrm{~s}$ after the application of Vin．
（3）The output of Error Amp．is raised to＂H＂level during the maintenance of the voltage（Vref）of the reference voltage unit．
（4）After the rise of Vref，the output of Internal Error Amp．is gradually decreased to an appropriate value by the function of Internal Phase Compensation Circuit，and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp．
（Note 2）ILx is gradually increased after Lx Switch is turned ON．In accordance with the increase of Ilx，VLx is also increased．When VLx reaches VLXlim， Lx Switch is turned OFF by an Lx Switch Protection Circuit．

| Vout $=3.0 \mathrm{~V}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Conditions | MIN. | TYP. | MAX. | Unit | Note |
| Vout | Output Voltage |  | 2.925 | 3.000 | 3.075 | V |  |
| VIN | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Oscillator Start-up Voltage | EXT no load,Vout : $0 \rightarrow 2 \mathrm{~V}$ |  | 0.7 | 0.8 | V |  |
| IDD1 | Supply Current 1 | EXT no load,Vout $=2.88 \mathrm{~V}$ |  | 30 | 50 | $\mu \mathrm{A}$ |  |
| IDD2 | Supply Current 2 | EXT no load,Vout=3.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| IExth | EXT "H" Output Current | Vext=Vout-0.4V |  |  | -1.5 | mA |  |
| IExtL | EXT "L" Output Current | VExT=0.4V | 1.5 |  |  | mA |  |
| fosc | Oscillator Frequency |  | 80 | 100 | 120 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | Vext "H" side | 70 | 80 | 90 | \% |  |
| tstart | Soft-Start Time | Time required for the rising of Vout up to 3 V | 0.5 | 2.0 |  | ms | Note1 |

Unless otherwise provided, VIN $=1.8 \mathrm{~V}, \mathrm{~V}$ SS $=0 \mathrm{~V}$, IouT $=10 \mathrm{~mA}$, Topt $=25^{\circ} \mathrm{C}$, and use External Circuit of Typical Application (FIG. 2).

| 5RH502B Vout=5.0V |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Conditions | MIN. | TYP. | MAX. | Unit | Note |
| Vout | Output Voltage |  | 4.875 | 5.000 | 5.125 | V |  |
| VIN | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Oscillator Start-up Voltage | EXT no load,Vout : $0 \rightarrow 2 \mathrm{~V}$ |  | 0.7 | 0.8 | V |  |
| IDD1 | Supply Current 1 | EXT no load,VouT=4.8V |  | 60 | 90 | $\mu \mathrm{A}$ |  |
| IDD2 | Supply Current 2 | EXT no load,Vout=5.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| IExth | EXT "H" Output Current | Vext=Vout-0.4V |  |  | -2 | mA |  |
| IExtL | EXT "L" Output Current | VExt $=0.4 \mathrm{~V}$ | 2 |  |  | mA |  |
| fosc | Oscillator Frequency |  | 80 | 100 | 120 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | Vext "H" side | 70 | 80 | 90 | \% |  |
| tstart | Soft-Start Time | Time required for the rising of Vout up to 5 V | 0.5 | 2.0 |  | ms | Note1 |

Unless otherwise provided, VIN $=3 \mathrm{~V}$, Vss $=0 \mathrm{~V}$, Iout $=10 \mathrm{~mA}$, Topt $=25^{\circ} \mathrm{C}$ and use External Circuit of Typical Application (FIG. 2).

- (Note 1) refer to page 5 (Note 1)
- RH5RH303B

| Symbol | Item | Conditions | MIN. | TYP. | MAX. | Unit | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vout | Output Voltage |  | 2.925 | 3.000 | 3.075 | V |  |
| Vin | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Start-up Voltage | Iout $=1 \mathrm{~mA}, \mathrm{VIN}: 0 \rightarrow 2 \mathrm{~V}$ |  | 0.8 | 0.9 | V |  |
| Vhold | Hold-on Voltage | Iout $=1 \mathrm{~mA}, \mathrm{VIN}: 2 \rightarrow 0 \mathrm{~V}$ | 0.7 |  |  | V |  |
| $\eta$ | Efficiency |  | 70 | 85 |  | \% |  |
| IdD1 | Supply Current 1 | To be measured at OUT pin |  | 30 | 50 | $\mu \mathrm{A}$ |  |
| IdD2 | Supply Current 2 | To be measured at OUT pin VIN=3.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| ILX | Lx Switching Current | $\mathrm{VLx}=0.4 \mathrm{~V}$ | 60 |  |  | mA |  |
| ILXIeak | Lx Leakage Current | VLX=6V,VIN=3.5V |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| Iexth | EXT "H" Output Current | Vext=Vout-0.4V |  |  | -1.5 | mA |  |
| IextL | EXT "L" Output Current | VEXT $=0.4 \mathrm{~V}$ | 1.5 |  |  | mA |  |
| VCeh1 | $\overline{\mathrm{CE}}$ "H" Level 1 | Vout $\geq 1.5 \mathrm{~V}$ | Vout-0.4 |  |  | V |  |
| Vcel1 | $\overline{\mathrm{CE}}$ "L" Level 1 | Vout $\geq 1.5 \mathrm{~V}$ |  |  | 0.4 | V |  |
| Vceh2 | $\overline{\mathrm{CE}}$ "H" Level 2 | $0.8 \mathrm{~V} \leq$ Vout $<1.5 \mathrm{~V}$ | Vout-0.1 |  |  | V |  |
| VCel2 | $\overline{\mathrm{CE}}$ "L" Level 2 | $0.8 \mathrm{~V} \leq$ Vout $<1.5 \mathrm{~V}$ |  |  | 0.1 | V |  |
| Iceh | $\overline{\mathrm{CE}}$ "H" Input Current | $\overline{\mathrm{CE}}=3 \mathrm{~V}$ |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| Icel | $\overline{\mathrm{CE}}$ "L" Input Current | $\overline{\mathrm{CE}}=0 \mathrm{~V}$ | -0.5 |  |  | $\mu \mathrm{A}$ |  |
| fosc | Oscillator Frequency |  | 80 | 100 | 120 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | on (VLX "L" )side | 70 | 80 | 90 | \% |  |
| tstart | Soft-Start Time | Time required for the rising of Vout up to 3 V . | 0.5 | 2.0 |  | ms | Note1 |
| VLxlim | VLx Voltage Limit | Lx Switch ON | 0.65 | 0.8 | 1.0 | V | Note2 |

Unless otherwise provided, Vin $=1.8 \mathrm{~V}, \mathrm{Vss}=0 \mathrm{~V}$, IouT $=10 \mathrm{~mA}$, Topt $=25^{\circ} \mathrm{C}$, and use External Circuit of Typical Application (FIG. 3).
(Note 1) Soft-Start Circuit is operated in the following sequence :
(1) VIN is applied.
(2) The voltage (Vref) of the reference voltage unit is maintained at 0 V for about $200 \mu \mathrm{~s}$ after the application of VIN.
(3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
(4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Com pensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
(Note 2) ILX is gradually increased after Lx Switch is turned ON. In accordance with the increase of ILX, VLX is also increased. When VLX reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.

- RH5RH503B

Vout $=5.0 \mathrm{~V}$

| Symbol | Item | Conditions | MIN. | TYP. | MAX. | Unit | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vout | Output Voltage |  | 4.875 | 5.000 | 5.125 | V |  |
| VIN | Input Voltage |  |  |  | 8 | V |  |
| Vstart | Start-up Voltage | IouT $=1 \mathrm{~mA}, \mathrm{VIN}: 0 \rightarrow 2 \mathrm{~V}$ |  | 0.8 | 0.9 | V |  |
| Vhold | Hold-on Voltage | Iout $=1 \mathrm{~mA}, \mathrm{VIN}: 2 \rightarrow 0 \mathrm{~V}$ | 0.7 |  |  | V |  |
| $\eta$ | Efficiency |  | 70 | 85 |  | \% |  |
| IDD1 | Supply Current 1 | To be measured at OUT pin |  | 60 | 90 | $\mu \mathrm{A}$ |  |
| IDD2 | Supply Current 2 | To be measured at OUT pin VIN=5.5V |  | 2 | 5 | $\mu \mathrm{A}$ |  |
| ILX | Lx Switching Current | VLX=0.4V | 80 |  |  | mA |  |
| ILXleak | Lx Leakage Current | $\mathrm{VLX}=6 \mathrm{~V}, \mathrm{VIN}=5.5 \mathrm{~V}$ |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| IExth | EXT "H" Output Current | Vext=Vout-0.4V |  |  | -2.0 | mA |  |
| IEXtL | EXT "L" Output Current | VExT $=0.4 \mathrm{~V}$ | 2.0 |  |  | mA |  |
| Vcehi | CE "H" Level 1 | Vout $\geq 1.5 \mathrm{~V}$ | Vout-0.4 |  |  | V |  |
| VCEL1 | $\overline{\mathrm{CE}}$ "L" Level 1 | VouT $\geq 1.5 \mathrm{~V}$ |  |  | 0.4 | V |  |
| Vceh2 | CE "H" Level 2 | $0.8 \mathrm{~V} \leq$ Vout $<1.5 \mathrm{~V}$ | Vout-0.1 |  |  | V |  |
| VCEL2 | $\overline{\mathrm{CE}}$ "L" Level 2 | $0.8 \mathrm{~V} \leq$ Vout $<1.5 \mathrm{~V}$ |  |  | 0.1 | V |  |
| ICEH | $\overline{\mathrm{CE}}$ "H" Input Current | $\overline{\mathrm{CE}}=5 \mathrm{~V}$ |  |  | 0.5 | $\mu \mathrm{A}$ |  |
| ICEL | $\overline{\mathrm{CE}}$ "L" Input Current | $\overline{\mathrm{CE}}=0 \mathrm{~V}$ | -0.5 |  |  | $\mu \mathrm{A}$ |  |
| fosc | Oscillator Frequency |  | 80 | 100 | 120 | kHz |  |
| Maxdty | Oscillator Maximum Duty Cycle | on (VLX "L" )side | 70 | 80 | 90 | \% |  |
| tstart | Soft-Start Time | Time required for the rising of Vout up to 5 V . | 0.5 | 2.0 |  | ms | Note1 |
| VLXlim | VLX Voltage Limit | Lx Switch ON | 0.65 | 0.8 | 1.0 | V | Note2 |

Unless otherwise provided, Vin $=3 \mathrm{~V}, \mathrm{Vss}=0 \mathrm{~V}$, IouT $=10 \mathrm{~mA}$, Topt $=25^{\circ} \mathrm{C}$, and use External Circuit of Typical Application (FIG. 3).
(Note 1) Soft-Start Circuit is operated in the following sequence :
(1) VIN is applied.
(2) The voltage (Vref) of the reference voltage unit is maintained at 0 V for about $200 \mu \mathrm{~s}$ after the application of VIN .
(3) The output of Error Amp. is raised to "H" level during the maintenance of the voltage (Vref) of the reference voltage unit.
(4) After the rise of Vref, the output of Internal Error Amp. is gradually decreased to an appropriate value by the function of Internal Phase Com pensation Circuit, and the Output Voltage is gradually increased in accordance with the gradual decrease of the output of Internal Error Amp.
(Note 2) ILx is gradually increased after Lx Switch is turned ON. In accordance with the increase of ILx, VLx is also increased. When VLx reaches VLxlim, Lx Switch is turned OFF by an Lx Switch Protection Circuit.

## RH5RH

## OPERATION OF STEP-UP DC/DC CONVERTER

Step-up DC/DC Converter charges energy in the inductor when Lx Transistor (LxTr) is on, and discharges the energy with the addition of the energy from Input Power Source thereto, so that a higher output voltage than the input voltage is obtained.

The operation will be explained with reference to the following diagrams :


Step 1 : LxTr is turned ON and current IL (= i1 ) flows, so that energy is charged in L . At this moment, $\operatorname{IL}(=\mathrm{i} 1$ ) is increased from ILmin $(=0)$ to reach ILmax in proportion to the on-time period (ton) of LxTr.
Step 2 : When LxTr is turned OFF, Schottky diode (SD) is turned ON in order that L maintains IL at ILmax, so that current IL (=i2) is released.

Step 3 : IL (=i2) is gradually decreased, and in the case of discontinuous mode, IL reaches ILmin (=0) after a time period of topen, so that SD is turned OFF. However, in the case of a continuous mode which will be mentioned later, the time period (toff) runs out before IL reaches ILmin ( $=0$ ), so that LxTr is turned ON in the next cycle, and SD is turned OFF. In this case, ILmin does not reach zero, and IL (=i1) increases from ILmin (>0).

In the case of PWM control system, the output voltage is maintained constant by controlling the on-time period (ton), with the oscillator frequency (fosc) being maintained constant.

## - Discontinuous Conduction Mode and Continuous Conduction Mode

In the above two diagrams, the maximum value (ILmax) and the minimum value (ILmin) of the current which flows through the inductor are the same as those when LxTr is ON and also when LxTr is OFF .

The difference between ILmax and ILmin, which is represented by $\Delta I$, is :
$\Delta \mathrm{I}=\mathrm{IL} m a x-\mathrm{ILmin}=\mathrm{VIN} \cdot \mathrm{ton} / \mathrm{L}=(\mathrm{VoUT}-\mathrm{VIN}) \cdot$ topen/L ........................................ERuation 1
wherein $\mathrm{T}=1 /$ fosc=ton+toff
duty $(\%)=$ ton $/ \mathrm{T} \cdot 100=$ ton $\cdot$ fosc $\cdot 100$
topen<toff
In Equation 1, VIN $\cdot$ ton/L and (VouT-VIN) $\cdot$ topen/L are respectively show the change in the current at ON, and the change in the current at OFF.

When the output current (IOUT) is relatively small, topen<toff as illustrated in the above diagram. In this case, the energy charged in the inductor during the time period of ton is discharged in its entirely during the time period of toff, so that ILmin becomes zero (ILmin=0). When IoUT is gradually increased, topen eventually becomes equal to toff (topen=toff), and when Iout is further increased. ILmin becomes larger than zero (ILmin>0). The former mode is referred to as the discontinuous mode and the latter mode is referred to as the continuous mode.

In the continuous mode, when Equation 1 is solved for ton and the solution is tonc,

When ton<tonc, the mode is the discontinuous mode, and when ton=tonc, the mode is the continuous mode.

## - Output Current in Discontinuous Mode

In the discontinuous mode, when LxTr is on, the energy Pon charged in the inductor is provided by Equation 3 as follows :

$$
\begin{aligned}
& \text { PON }=\int_{0}^{\mathrm{ton}} \mathrm{VIN} \cdot \mathrm{IL}(\mathrm{t}) \mathrm{dt}=\int_{0}^{\mathrm{ton}}\left(\mathrm{VIN}^{2} \cdot \mathrm{t} / \mathrm{L}\right) \mathrm{dt} \\
& =\mathrm{VIN}^{2} \cdot \operatorname{ton}^{2} /(2 \cdot \mathrm{~L}) \\
& \text { Equation } 3
\end{aligned}
$$

In the case of the step-up $\mathrm{DC} / \mathrm{DC}$ converter, the energy is also supplied from the input power source at the time of OFF.

Thus, PoFF $=\int_{0}^{\text {topen }}$ VIN $\cdot \mathrm{IL}(\mathrm{t}) \mathrm{dt}=\int_{0}^{\text {topen }}(($ VOUT-VIN $) \cdot \mathrm{t} / \mathrm{L}) \mathrm{dt}$

$$
=\text { VIN } \cdot(\text { Vout-VIN }) \cdot \text { topen }^{2} /(2 \cdot \mathrm{~L})
$$

Here, topen=VIN $\cdot$ ton/(VouT-VIN) from Equation 1, and when this is substituted into the above equation.

$$
\begin{aligned}
& =\mathrm{VIN}^{3} \cdot \operatorname{ton}^{2} /(2 \cdot \mathrm{~L} \cdot(\text { Vout }-\mathrm{VIN}) \cdot \\
& \text { Equation } 4
\end{aligned}
$$

Input power is $(\mathrm{PON}+\mathrm{PofF}) / \mathrm{T}$. When this is converted in its entirely to the output.

Pin=(Pon+Poff)/T=Vout • IouT=Pout ....................................................................ERuation 5

Equation 6 can be obtained as follows by solving Equation 5 for Iout by substituting Equations 3 and 4 into Equation 5 :

The peak current which flows through $\mathrm{L} \cdot \mathrm{LxTr} \cdot \mathrm{SD}$ is

ILmax=VIN • ton/L
Equation 7

## RH5RH

Therefore it is necessary that the setting of the input/output conditions and the selection of peripheral components should be made with ILmax taken into consideration.

## - Output Current in Continuous Conduction Mode

When the operation enters into the continuous conduction mode by increasing the IoUT, ILmin becomes equal to Iconst ( $>0$ ), and this current always flows through the inductor. Therefore, Vin • Iconst is added to Pin in Equation 5.

Thus, $\operatorname{Pin}=$ Vin $\cdot$ Iconst+ $($ Pon + Poff $) / T=$ Vout $\cdot$ IouT $=$ Pout

When the above Equation is solved for Iout,


The peak current which flows through $\mathrm{L} \cdot \mathrm{LxTr} \cdot \mathrm{SD}$ is

ILmax=ViN $\cdot$ ton/L+Iconst
Equation 9

From Equations 6 and 9, the larger the value of L, the smaller the load current at which the operation enters into the continuous mode, and the smaller the difference between ILmax and ILmin, and the smaller the value of ILmax.

Therefore, when the load current is the same, the larger the value of $L$, the easier the selection of peripheral components with a small allowable current becomes, and the smaller the ripple of the peripheral components can be made. In this case, however, it must be noted from Equation 6 that Iout becomes small when the allowable current of the inductor is small or when Vin is so small that the operation cannot enter into the continuous mode.

## HINTS

The above explanation is directed to the calculation in an ideal case where there is no energy loss caused by the resistance in the external components and LxSW. In an actual case, the maximum output current will be 50 to $80 \%$ of the above calculated maximum output current. In particular, care must be taken because Vin is decreased in an amount corresponding to the voltage drop caused by LxSW when IL is large or Vin is low. Furthermore, it is required that with respect to Vout, Vf of the diode (about 0.3 V in the case of a Schottky type diode) be taken into consideration.

## TYPICAL CHARACTERISTICS

1）Output Voltage vs．Output Current







## RH5RH

2) Efficiency vs. Output Current





3) Supply Curret (No Load) vs. Input Voltage


4) Output Current vs.Ripple Voltage


RH5RH301A




## RH5RH


5) Start-up/Hold-on Voltage vs. Output Current (Topt=25 ${ }^{\circ} \mathrm{C}$ )



6) Output Voltage vs.Temperature



7) Start-up Voltage vs. Temperature


11) Lx Switching Current vs.Temperature

8) Hold-on Voltage vs. Temperature

RH5RH501A

10) Supply Current 2 vs.Temperature

RH5RH501A

12) Lx Leakage Current vs.Temperature

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13) Oscillator Frequency vs. Temperature


14) Oscillator Duty Cycle vs. Temperature




15) Vıx Voltage Limit vs. Temperature

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16) EXT " H " Output Current vs. Temperature RH5RH501A

17) EXT "L" Output Current vs. Temperature RH5RH501A

18) Load Transient Response




## RH5RH

19) Distribution of Output Voltage

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20) Distribution of Oscillator Frequency

RH5RH501A


## TYPICAL APPLICATIONS

- RH5RH $\times \times 1$ A


| Components Inductor (L) | $: 120 \mu \mathrm{H}$ (Sumida Electric Co., Ltd.) |
| :---: | :--- |
| Diode (D) | $:$ MA721 (Matsushita Electronics Corporation, Schottky Type) |
| Capacitor (CL) | $: 22 \mu F$ (Tantalum Type) |

FIG. 1

- RH5RH $\times \times 2$ B


| Components Inductor (L) | $: 28 \mu \mathrm{H}$ (Troidal Core) |
| :--- | :--- |
| Diode (D) | $:$ HRP22 (Hitachi, Schottky Type) |
| Capacitor (CL) | $: 100 \mu \mathrm{~F}$ (Tantalum Type) |
| Transistor (Tr) | $: 2 \mathrm{SD} 1628 \mathrm{G}$ |
| Base Resistor (Rb) | $: 300 \Omega$ |
| Base Capacitor (Cb) | $: 0.01 \mu \mathrm{~F}$ |

FIG. 2

## RH5RH

## - RH5RH $\times \times 3$ B



| Components Inductor (L) | $: 120 \mu \mathrm{H}$ (Sumida Electric Co., Ltd.) |
| :---: | :--- |
| Diode (D) | $:$ MA721 (Matsushita Electronics Corporation, Schottky Type) |
| Capacitor (CL) | $: 22 \mu \mathrm{~F}$ (Tantalum Type) |

FIG. 3


| Components Inductor (L) | $: 28 \mu \mathrm{H}$ (Troidal Core) |
| :--- | :--- |
| Diode (D) | $:$ HRP22 (Hitachi, Schottky Type) |
| Capacitor (CL) | $: 100 \mu \mathrm{~F}$ (Tantalum Type) |
| Transistor (Tr) | $: 2 \mathrm{SD} 1628 \mathrm{G}$ |
| Base Resistor (Rb) | $: 300 \Omega$ |
| Base Capacitor (Cb) | $: 0.01 \mu \mathrm{~F}$ |

FIG. 4

## - $\overline{\mathrm{CE}}$ pin Drive Circuit



FIG. 5

## RH5RH

## APPLICATION CIRCUITS

-12V Step-up Circuit

(Note) When the Output Current is small or the Output Voltage is unstable, use the Rzd for flowing the bias current through the Zener diode ZD.
FIG. 6

## - Step-down Circuit


(Note) When the Lx pin Voltage is over the rating at the time PNP Tr is OFF, use a RH5RH $\times \times 2 \mathrm{~B}$ and drive the PNP Tr. by the external NPN Tr.
FIG. 7

- Step-up/Step-down Circuit with Flyback

(Note) Use a RH5RH $\times \times 2 \mathrm{~B}$,depend on the Output Current.
FIG. 8
*The Starter Circuit is necessary for all above circuits.
1.for Step-up Circuit.

2.for Step-down and Step-up/Step-down Circuit.


[^0]
[^0]:    ZDst $2.5 \mathrm{~V} \leq$ ZDDst $\leq$ Designation of Output Voltage
    Rst Input Bias Current of ZDst and Tr. (several $k \Omega$ to several hundreds $k \Omega$ )

