

Inductorless -2x Boost/Buck Regulator

Features

- Input Range 2.5V to 5.5V
- Regulated Output Options from -3.0 to -5.0V
- Output Current 20mA (max)
- · 200kHz Internal Oscillator Frequency
- · External Synchronizing Clock Input
- · Logic Level Shutdown
 - 1μA (max) Supply Current
- Available in 8-Pin MSOP Package

Applications

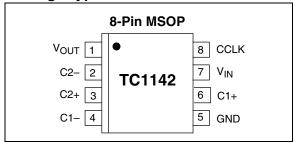
- · Cellular Phones
- Battery Powered/Portable Equipment

Device Selection Table

Part Number	Output Voltage (V)*	Package	Operating Temp. Range
TC1142-3.0EUA	3.0	8-Pin MSOP	-40°C to +85°C
TC1142-4.0EUA	4.0	8-Pin MSOP	-40°C to +85°C
TC1142-5.0EUA	5.0	8-Pin MSOP	-40°C to +85°C

^{*}Other output voltages are available (-3.5V and -4.5V). Please contact Microchip Technology Inc. for details.

Package Type



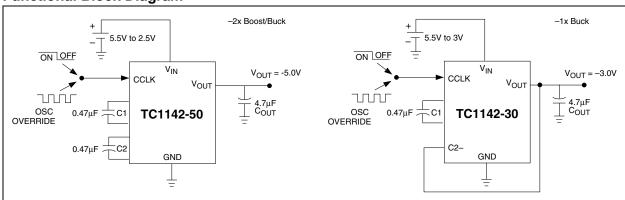
General Description

The TC1142 generates a regulated negative voltage from -3V to -5V at 20mA from an input of 2.5V to 5.5V, using only three external capacitors. Other boost/buck switching regulators must use an inductor, which is larger and radiates EMI. An internal voltage comparator inhibits the charge pump when $V_{\rm OUT}$ is more negative than the regulated value (per the ordering option). The values of flying capacitors C1 and C2 are chosen to be less than $C_{\rm OUT}$ in order to reduce the ripple generated from regulating $V_{\rm OUT}$ in this manner. The TC1142 also can be used as a -1x buck regulator by omitting C2, and connecting the C2 pin to $V_{\rm OUT}$

The part goes into shutdown when the CCLK input is driven low. When in shutdown mode, the part draws a maximum of $1\mu A$. When CCLK is pulled high, the part runs from the internal 200kHz oscillator. The device may be run with an external clock, provided the frequency is greater than 3kHz and less than 500kHz.

The TC1142 comes in a space-saving MSOP package.

Functional Block Diagram



1.0 ELECTRICAL CHARACTERISTICS

Absolute Maximum Ratings*

 *Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operation sections of the specifications is not implied. Exposure to Absolute Maximum Rating conditions for extended periods may affect device reliability.

TC1142 ELECTRICAL SPECIFICATIONS

Electrical Characteristics: $R_L = \infty$, $V_{IN} = 3.2V$, Mode = -2x, C1 = C2 = 0.47 μ F (Note 1), CCLK = V_{IH} , $C_{OUT} = 4.7 \mu$ F, for $V_R = 3V$, $V_{IN} = 3.5V$, $T_A = T_{MIN}$ to T_{MAX} , unless otherwise noted.						
Symbol	Parameter	Min	Тур	Max	Units	Test Conditions
V _{IN}	Supply Voltage	2.5	_	5.5	V	
V _{OUT}	Output Voltage	-(V _R + 0.2)	-V _R	-(V _R - 0.2)	V	I _L = 0mA (Note 2)
V _{P-P}	Output Ripple	_	100	_	mV	$I_L = 10mA$
I _{SUPPLY}	Supply Current	_	200	400	μΑ	
I _{SUPPLY1}		_	0.1	1	μΑ	CCLK = 0V
R _{OUTCL}	Closed-Loop Output Resistance	_	2	6	Ω	
R _{OUT}	Open-Loop Output Resistance	_	30	_	Ω	(Note 3)
fosc	Internal Oscillator Frequency	150	200	275	kHz	
f _{CCLK}	External Clock Frequency, Typical	3	_	500	kHz	(Note 4)
P _{EFF}	Power Efficiency	70	76	_	%	$I_L = 10$ mA, $V_R = 5$ V; (See Equation 3-5)
V _{IH}	CCLK Input High Threshold	2.2	_	_	V	
V _{IL}	CCLK Input Low Threshold	_	_	1.0	V	

- Note 1: Assume C1 and C2 have an ESR of 1Ω .
 - 2: V_R is the voltage output specified in the ordering option.
 - 3: Measured in -1x Mode. For $V_R = 3V$, $V_{IN} = 2.5V$.
 - 4: CCLK is driven with an external clock. Minimum frequency = 1/2t₀ at 50% duty cycle, where t₀ is the counter timeout period.

2.0 PIN DESCRIPTIONS

The descriptions of the pins are listed in Table 2-1.

TABLE 2-1: PIN FUNCTION TABLE

Pin No. (8-Pin MSOP)	Symbol	Description
1	V _{OUT}	Regulated negative output voltage.
2	C2-	Negative terminal of flying capacitor C2.
3	C2+	Positive terminal of flying capacitor C2.
4	C1-	Negative terminal of flying capacitor C1.
5	GND	Power supply ground.
6	C1+	Positive terminal of flying capacitor C1.
7	V _{IN}	Power supply positive voltage input (2.5V to 5.5V).
8	CCLK	Clock control input: If low, the TC1142 is in Shutdown mode (1µA, max). If high, the TC1142 runs off the internal oscillator (200kHz, typ.). CCLK can be overridden by an external oscillator from 3kHz to 500kHz.

3.0 DETAILED DESCRIPTION

The TC1142 inductorless -2x boost/buck regulator is an inverting charge pump that uses a pulse-frequency modulation (PFM) control scheme to produce a regulated negative output voltage, - V_R , between -3V and -5V (depending on the output voltage option) at 20mA maximum load. Output voltage regulation is achieved by gating ON the clock to the charge pump for a single half-clock period whenever the output is more positive than V_R , and gating it OFF when the output is more negative than - V_R . The resulting PFM of the clock applied to the charge pump has a high frequency spectral content consisting only of clock harmonics. When using an external clock, the transient noise is then synchronized to the clock and is easier to filter in sensitive applications.

The TC1142 also can be used as a -1x boost/buck regulator by omitting the C2 capacitor and connecting the C2- pin to V_{OUT} .

The PFM control scheme minimizes supply current at small loads and permits the use of low value flying capacitors, which saves on printed circuit board space and cost. Due to the TC1142's doubling and inverting charge pump mechanism, the output voltage is limited to $-2V_{IN}$. To produce a -5V regulated output, for example, a minimum input voltage of 2.5V is required at V_{IN} .

The CCLK pin of the TC1142 has three functions: It can select the internal 200kHz oscillator (when held HIGH), put the TC1142 into shutdown (when held LOW), or provide an external clock input. To achieve this functionality, an internal counter is reset by any positive transition at the CCLK pin, but will time out in typically 160 µsec (i.e., a frequency higher than about 3kHz). If the counter times out following the last positive transition, then the internal clock will be gated through to the charge pump if CCLK is HIGH, or the device will enter shutdown mode if it is LOW. To enter shutdown, CCLK must be LOW and the counter must have timed out. These timing diagrams are shown in Figure 3-4.

A functional circuit diagram of the TC1142 is shown in Figure 3-1. The output voltage V_{OUT} is compared to an on-chip reference voltage, and the comparator output is used to gate the charge pump clock. The charge pump is a negative voltage doubler and has two phases of operation which are further illustrated in Figure 3-2 and Figure 3-3. In phase 1, shown in Figure 3-2, the flying capacitor C1 charges the flying capacitor C2 while the device load is totally serviced by the charge stored on the reservoir capacitor $C_{OUT}.$ In phase 2, shown in Figure 3-3, the capacitor C1 is recharged to $V_{\mbox{\scriptsize IN}}$ while the capacitor C2 transfers its charge to the reservoir capacitor $C_{\mbox{\scriptsize OUT}}.$

In normal operation, the TC1142 charge pump stays in phase 2 and only switches to phase 1 as required to maintain output voltage regulation.

Shutdown

Clock
Circuit

OSC
Override

FIGURE 3-1: FUNCTIONAL CIRCUIT DIAGRAM

FIGURE 3-2: TC1142 PHASE 1

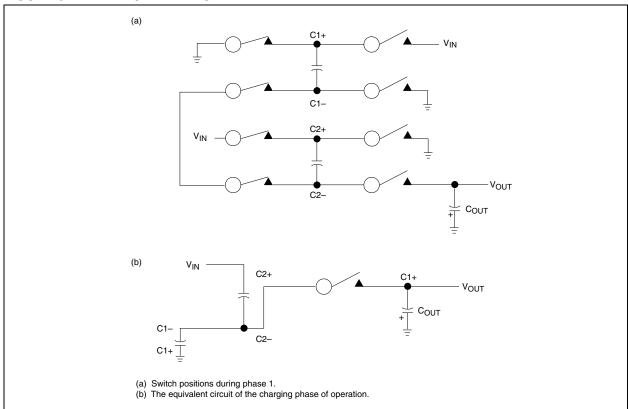
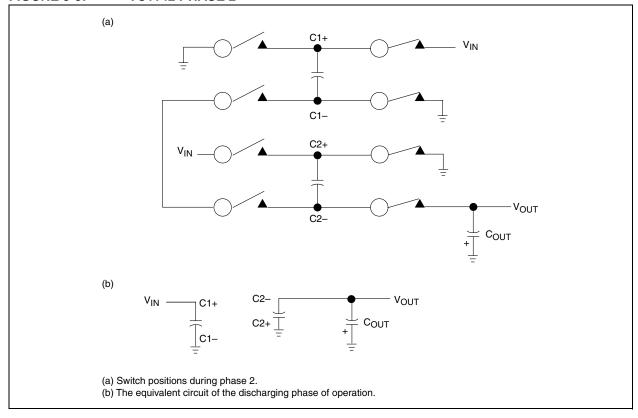


FIGURE 3-3: TC1142 PHASE 2



3.1 Output Voltage and Ripple

For a -2x boost:

a.) For unregulated operation when $V_{IN} \le \left| \frac{V_R}{2} \right|$.

In this case, the output voltage is given by:

EQUATION 3-1:

$$V_{OUT} = -|2VIN| + IOR_{OUT}$$

where
$$R_{OUT} = \frac{1}{f} \left(\frac{1}{C1} + \frac{1}{C2} \right) + \frac{R_SC2}{(C2 + C_{OUT})}$$

Here, f is the clock frequency and R_S is the total ON resistance of the switches connecting C2 to GND and V_{OUT} in phase 2 of the charge pump operating cycle with the equivalent series resistance (ESR) of C2.

The output ripple voltage is given by:

EQUATION 3-2:

$$V_{RIPPLE} = I_{O}R_{RIPPLE}$$

where
$$R_{RIPPLE} = \frac{1}{2f(C2 + C_{OUT})} + \frac{1}{2fC_{OUT}} + \frac{ESR\ C2}{(C2 + C_{OUT})}$$

Here, ESR is the equivalent series resistance of COLIT.

b.) For regulated operation when
$$V_{IN} > \left\lfloor \frac{V_R}{2} \right\rfloor$$
.

In this case, the TC1142 is held in phase 2 until the output voltage drops below V_R . When this occurs, the TC1142 reverts to phase 1 for a half period of the clock, during which C2 is charged from C1. At the end of this half-period, C2 is reconnected to C_{OUT} to boost the output voltage. During the phase 1 time period, the output voltage will drop below V_R before it is boosted back, so the minimum output voltage is approximated by:

EQUATION 3-3:

$$V_{OUTMIN} = -|VR| + I_OR_{OUT}$$

where
$$R_{OUT} = \frac{1}{2fC_{OUT}} + \frac{ESR C2}{(C2 + C_{OUT})}$$

The output ripple voltage is given approximately by:

EQUATION 3-4:

$$V_{RIPPLE} = \frac{(2_{VIN} - |V_R| + ESR I_O C2 \left(\frac{1}{C1} + \frac{1}{C2}\right))}{N}$$

where N =
$$\left(\frac{1}{C1} + \frac{1}{C2}\right)$$
 (C2 + C_{OUT})

For values of V_{IN} higher than $|V_R/2|$ by several hundred mV, the effect on ripple of the ESR of C_{OUT} can be neglected compared to the "overdrive" effect of V_{IN} .

Here, it can be seen that V_{RIPPLE} increases with increasing V_{IN} , but can be minimized by choosing small C1 and C2 values and a large C_{OUT} value.

3.2 Capacitor Selection

To maintain low output impedance and ripple, it is recommended that capacitors with low equivalent series resistance (ESR) be used. Additionally, larger values of the output capacitor and smaller values of the flying capacitors will reduce output ripple. For a capacitor value of 4.7 μF for $C_{OUT},$ and values of 0.47 μF for C1 and C2, the typical output impedance of the TC1142 in regulation is 0.5 Ω . For the capacitor ESR not to have a noticeable effect on output impedance, it should not be larger than 1/2fC $_{OUT}.$ This also makes its effect on ripple voltage negligible. For $V_{IN}=3.2V$ and $V_{R}=$ -5V, the output ripple voltage is less than 70 mV $_{PP}.$ Table 3-1 summarizes output ripple versus capacitor size for an input voltage of 3.2V and a regulated output voltage of -5V.

Surface mount ceramic capacitors are preferred for their small size, low cost and low ESR. Low ESR tantalum capacitors also are acceptable. See Table 3-2 for a list of suggested capacitor suppliers.

TABLE 3-1: VOLTAGE RIPPLE VS. C1/C2 FLYING CAPACITORS AND OUTPUT CAPACITOR C_{OUT} ESR = 0.1Ω , I_{OUT} = 20mA

C1, C2 (μF)	C _{OUT} (μF)	V _{IN} (V)	V _{OUT} (V)	V _{RIPPLE} (mV)
0.1	4.7	3.2	-5	14.6
0.22	4.7	3.2	-5	31.4
0.33	4.7	3.2	-5	46.1
0.47	4.7	3.2	-5	63.9
0.68	4.7	3.2	-5	88.7
1.0	4.7	3.2	-5	123.2
0.1	10	3.2	-5	7.0
0.22	10	3.2	-5	15.1
0.33	10	3.2	-5	22.4
0.47	10	3.2	-5	31.5
0.68	10	3.2	-5	44.7
1.0	10	3.2	-5	63.8

TABLE 3-2: LOW ESR SURFACE-MOUNT CAPACITOR MANUFACTURERS

Manufacturer	Туре	Phone	
AVX Corp.	TPS series surface-mount tantalum	803-448-9411	
	X7R type surface-mount ceramic		
Matsuo	267 series surface-mount tantalum	714-969-2491	
	X7R type surface-mount ceramic		
Sprague	593D, 594D, 595D series surface-mount tantalum	207-324-4140	
Murata	Ceramic chip capacitors	800-831-9172	
Taiyo Yuden	Ceramic chip capacitors	800-348-2496	
Tokin	Ceramic chip capacitors	408-432-8020	

3.3 Power Efficiency

Assuming the output is loaded with at least 20% of the maximum available output current, the power efficiency of the TC1142 can be estimated using the following equation:

EQUATION 3-5:

$$\eta = \frac{|VR|}{2(VIN)}$$

For example, a 3.2 Volt V_{IN} , and a -5 Volt V_{R} will have an efficiency of approximately 78%. For loads less than 20% of the maximum available output current, the power efficiency will be substantially reduced. Other factors that affect the actual efficiency include:

- Losses from power consumed by the internal oscillator (if used).
- I²R losses due to the on-resistance of the MOSFET charge pump switches.
- 3. Charge pump capacitor losses due to ESR.
- Losses that occur during charge transfer (from the flying capacitors to the output capacitor) when a voltage difference exists between these capacitors.

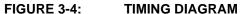
3.4 Choice of -2x or -1x Connections

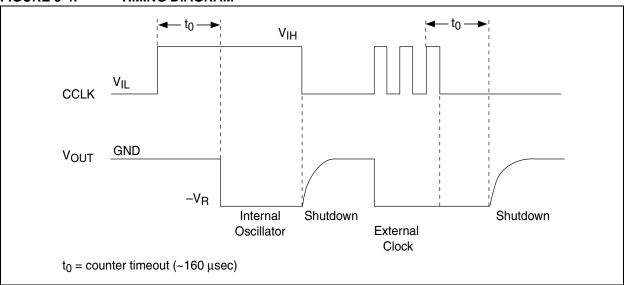
If required output voltage can be achieved using a -1x configuration then this is preferred for the following reasons:

- 1. Power efficiency is improved from $V_R/2V_{IN}$ to V_R/V_{IN}
- 2. Only one flying capacitor needed
- 3. The output ripple becomes proportional to $V_{IN} V_{R}$ rather than 2 $V_{IN} V_{R}$.

3.5 Layout Considerations

Proper layout is important to obtain optimal performance. Mount capacitors as close to their connecting device pins as possible to minimize stray inductance and capacitance. It is recommended that a large ground plane be used to reduce noise leakage into other circuitry.



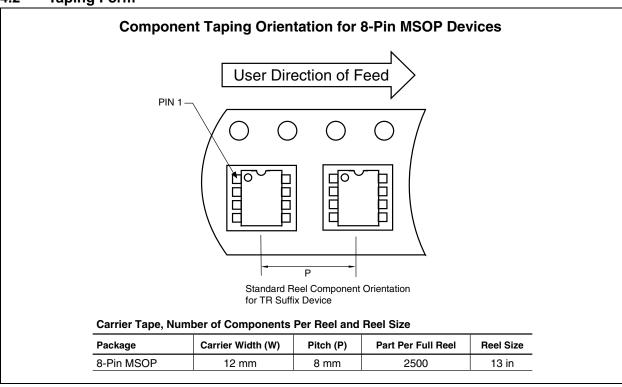


4.0 PACKAGING INFORMATION

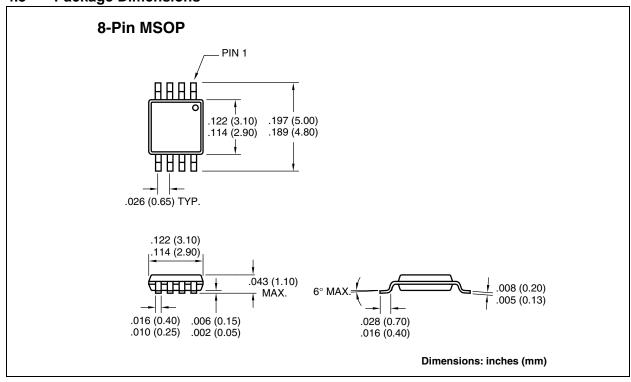
4.1 Package Marking Information

Package marking data not available at this time.

4.2 Taping Form



4.3 Package Dimensions



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TC1142

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AMERICAS

Corporate Office

2355 West Chandler Blvd. Chandler, AZ 85224-6199 Tel: 480-792-7200 Fax: 480-792-7277 Technical Support: 480-792-7627 Web Address: http://www.microchip.com

Rocky Mountain

2355 West Chandler Blvd. Chandler, AZ 85224-6199
Tel: 480-792-7966 Fax: 480-792-7456

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Detroit

Tri-Atria Office Building 32255 Northwestern Highway, Suite 190 Farmington Hills, MI 48334 Tel: 248-538-2250 Fax: 248-538-2260

Kokomo

2767 S. Albright Road Kokomo, Indiana 46902 Tel: 765-864-8360 Fax: 765-864-8387

Los Angeles

18201 Von Karman, Suite 1090 Irvine, CA 92612

Tel: 949-263-1888 Fax: 949-263-1338

New York

150 Motor Parkway, Suite 202 Hauppauge, NY 11788 Tel: 631-273-5305 Fax: 631-273-5335

San Jose

Microchip Technology Inc. 2107 North First Street, Suite 590 San Jose, CA 95131 Tel: 408-436-7950 Fax: 408-436-7955

Toronto

6285 Northam Drive, Suite 108 Mississauga, Ontario L4V 1X5, Canada Tel: 905-673-0699 Fax: 905-673-6509

ASIA/PACIFIC

Australia

Microchip Technology Australia Pty Ltd Suite 22, 41 Rawson Street Epping 2121, NSW Australia

Tel: 61-2-9868-6733 Fax: 61-2-9868-6755

China - Beijing

Microchip Technology Consulting (Shanghai) Co., Ltd., Beijing Liaison Office Unit 915 Bei Hai Wan Tai Bldg.

No. 6 Chaoyangmen Beidajie Beijing, 100027, No. China Tel: 86-10-85282100 Fax: 86-10-85282104

China - Chengdu

Microchip Technology Consulting (Shanghai) Co., Ltd., Chengdu Liaison Office Rm. 2401, 24th Floor, Ming Xing Financial Tower No. 88 TIDU Street Chengdu 610016, China Tel: 86-28-6766200 Fax: 86-28-6766599

China - Fuzhou

Microchip Technology Consulting (Shanghai) Co., Ltd., Fuzhou Liaison Office Unit 28F, World Trade Plaza No. 71 Wusi Road Fuzhou 350001, China Tel: 86-591-7503506 Fax: 86-591-7503521

China - Shanghai

Microchip Technology Consulting (Shanghai) Co., Ltd. Room 701, Bldg. B

Far East International Plaza No. 317 Xian Xia Road Shanghai, 200051

Tel: 86-21-6275-5700 Fax: 86-21-6275-5060

China - Shenzhen

Microchip Technology Consulting (Shanghai) Co., Ltd., Shenzhen Liaison Office Rm. 1315, 13/F, Shenzhen Kerry Centre, Renminnan Lu Shenzhen 518001, China

Tel: 86-755-2350361 Fax: 86-755-2366086

Hong Kong

Microchip Technology Hongkong Ltd. Unit 901-6, Tower 2, Metroplaza 223 Hing Fong Road Kwai Fong, N.T., Hong Kong Tel: 852-2401-1200 Fax: 852-2401-3431

India

Microchip Technology Inc. India Liaison Office Divvasree Chambers 1 Floor, Wing A (A3/A4) No. 11, O'Shaugnessey Road Bangalore, 560 025, India Tel: 91-80-2290061 Fax: 91-80-2290062

Japan

Microchip Technology Japan K.K. Benex S-1 6F 3-18-20, Shinyokohama Kohoku-Ku, Yokohama-shi Kanagawa, 222-0033, Japan Tel: 81-45-471- 6166 Fax: 81-45-471-6122

Korea

Microchip Technology Korea 168-1, Youngbo Bldg. 3 Floor Samsung-Dong, Kangnam-Ku Seoul, Korea 135-882

Tel: 82-2-554-7200 Fax: 82-2-558-5934

Singapore

Microchip Technology Singapore Pte Ltd. 200 Middle Road #07-02 Prime Centre Singapore, 188980

Tel: 65-6334-8870 Fax: 65-6334-8850

Taiwan

Microchip Technology Taiwan 11F-3, No. 207 Tung Hua North Road Taipei, 105, Taiwan Tel: 886-2-2717-7175 Fax: 886-2-2545-0139

EUROPE

Denmark

Microchip Technology Nordic ApS Regus Business Centre Lautrup hoj 1-3 Ballerup DK-2750 Denmark Tel: 45 4420 9895 Fax: 45 4420 9910

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Microchip Technology SARL Parc d'Activite du Moulin de Massy 43 Rue du Saule Trapu Batiment A - Ier Etage 91300 Massy, France Tel: 33-1-69-53-63-20 Fax: 33-1-69-30-90-79

Germany Microchip Technology GmbH Gustav-Heinemann Ring 125 D-81739 Munich, Germany Tel: 49-89-627-144 0 Fax: 49-89-627-144-44

Italy

Microchip Technology SRL Centro Direzionale Colleoni Palazzo Taurus 1 V. Le Colleoni 1 20041 Agrate Brianza Milan, Italy Tel: 39-039-65791-1 Fax: 39-039-6899883

United Kingdom

Arizona Microchip Technology Ltd. 505 Eskdale Road Winnersh Triangle Wokingham Berkshire, England RG41 5TU Tel: 44 118 921 5869 Fax: 44-118 921-5820

03/01/02

