

## Description

The ACPM-7833 is a fully matched CDMA Power amplifier module. Designed around Agilent Technologies' new Enhancement Mode pHEMT process, the ACPM-7833 offers premium performance in a very small form factor. Fully matched to 50 Ohms on the input and output.

The amplifier has excellent ACPR and efficiency performance at max Pout and low quiescent

Agilent ACPM-7833 Power Amplifier Module
current with a single bias control voltage. For even lower quiescent current, a dynamic bias control circuit can be used by varying the voltage on the Vcntl pin between 1.2 V to 2.5 V .

Designed in a surface mount RF package, the ACPM-7833 is cost and size competitive.

The ACPM-7833 is another key component of the Agilent CDMAdvantage RF chipset.

Features

- Operating frequency: 1850-1910 MHz
- 28.5 dBm linear output power @ 3.4V
- High efficiency: 40\% PAE
- Dynamic bias control for low midpower Idd
- Very low quiescent current with single control voltage
- Internal 50 ohm matching networks for both RF IN/OUT
- 3.2-4.2V linear operation
- cdma2000 1xRTT capable
- Only 3 SMT parts needed
- $4.0 \times 4.0 \times 1.1$ mm SMT package


## Applications

- CDMA handsets
- Datacards
- PDAs


Single control bias setting for low Idq and $40 \%$ PAE at Pout $=28.5 \mathrm{dBm}$

## Agilent Technologies

## Maximum Ratings ${ }^{[1]}$

| Parameter | Min. | Max. |
| :--- | :--- | :--- |
| Vdd Supply Voltage | 6.0 V |  |
| Power Dissipation ${ }^{[2]}$ | 2.5 W |  |
| Bias Current | 1.5 A |  |
| Control Voltage (Vcntl) | 3.0 V |  |
| Amplifier Input RF Power | 10 dBm |  |
| Junction Temperature | $+150^{\circ} \mathrm{C}$ |  |
| Storage Temperature (case temperature) | $-40^{\circ} \mathrm{C}$ | $+100^{\circ} \mathrm{C}$ |

## Package Marking and Dimensions



Note:
YYWWDD: year - work week - day
XXXX: lot code


All units are in mm

Electrical Characterization Information
All tests are done in $50 \Omega$ system at $\mathrm{Vdd} 1=\mathrm{Vdd} 2=\mathrm{V}$ bias $=3.4 \mathrm{~V}, 25^{\circ} \mathrm{C}$, unless noted otherwise.

| Parameter | Units | Min | Тур | Max | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PCS CDMA |  |  |  |  |  |
| Frequency Range | MHz | 1850 |  | 1910 |  |
| Gain (Fixed Cntl Voltage) |  |  |  |  |  |
| $\mathrm{P}_{\text {out }}=28.5 \mathrm{dBm}$ | dB | 25.5 | 27.5 | 29.5 | Ventl $=2.5 \mathrm{~V}$ |
| $\mathrm{P}_{\text {out }}=16 \mathrm{dBm}$ |  | 24 | 26 | 28 | V cntl$=1.8 \mathrm{~V}$ |
| Power Added Efficiency |  |  |  |  |  |
| $\mathrm{P}_{\text {out }}=28.5 \mathrm{dBm}$ | \% | 38 | 40 |  | Ventl $=2.5 \mathrm{~V}$ |
| $\mathrm{P}_{\text {out }}=16 \mathrm{dBm}$ | \% | 7.5 | 8.5 |  | Vcntl $=1.8 \mathrm{~V}$ |
| Total Supply Current | mA |  | 520 | 550 | $\mathrm{P}_{\text {out }}=28.5 \mathrm{dBm}, \mathrm{Vcntl}=2.5 \mathrm{~V}$ |
|  | mA |  | 135 | 156 | $\mathrm{P}_{\text {out }}=16 \mathrm{dBm}, \mathrm{V}$ cntl $=1.8 \mathrm{~V}$ |
|  | mA |  | 31 |  | $P_{\text {out }}=-5 \mathrm{dBm}, \mathrm{Vcntl}=1.2 \mathrm{~V}$ |
| ACPR @ $\pm 1.25 \mathrm{MHz}$ offset | dBc/30 kHz | -45 | -48 |  | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}$ |
| ACPR @ $\pm 1.98 \mathrm{MHz}$ offset | $\mathrm{dBc} / 30 \mathrm{kHz}$ | -53 | -55 |  | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}$ |
| Quiescent Current | mA |  | 62 | 80 | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}, \mathrm{Vcntl}=2.5 \mathrm{~V}$ |
|  | mA |  | 47 | 60 | V cntl $=1.8 \mathrm{~V}$ |
|  | mA |  | 25 |  | $\mathrm{Vcntl}=1.2 \mathrm{~V}$ |
| Ventl Current | mA |  | 2.0 | 2.7 | Ventl $=2.5 \mathrm{~V}$ |
| Input VSWR ( $\mathrm{P}_{\text {out }}=28.5 \mathrm{dBm}$ ) |  |  | 2.0:1 |  |  |
| Noise Figure | dB |  | 4.5 |  |  |
| Noise Power @ 80 MHz offset in 1930-1990 MHz | $\mathrm{dBm} / \mathrm{Hz}$ |  | -141 | -138 |  |
| Stability (Spurious): Load VSWR 5:1 | dBc | -50 |  |  | All phases |
| Harmonic Suppression: 2Fo | dBc | -30 | -38 |  |  |

Typical Performance, data measured in $50 \Omega$ system, $\mathrm{Vdd} 1=\mathrm{Vdd} 2=\mathrm{V}$ bias $=3.4 \mathrm{~V}, \mathrm{Vcntl}=2.5 \mathrm{~V}, \mathrm{~T}=25^{\circ} \mathrm{C}$ and Freq $=1880 \mathrm{MHz}$ unless noted otherwise.


Figure 1. Gain vs. Pout.


Figure 4. Idd vs. Output Power.


Figure 7. ACPR (1.98 MHz offset) vs. Pout.


Figure 2. Gain vs. Vcntl.


Figure 5. Idd vs. Output Power.


Figure 8. 2nd/3rd Harmonics vs. Pout.


Figure 3. PAE vs. Pout.


Figure 6. ACPR (1.25 MHz offset) vs. Pout.

## Ordering Information

| Part Number | No. of Devices | Container |
| :--- | :--- | :--- |
| ACPM-7833-BLK | 10 | Bulk |
| ACPM-7833-TR1 | 1000 | 7" Tape and Reel |

Tape Dimensions and Orientation


Notes:

1. Measured from centerline of sprocket hole to centerline of pocket
2. Cumulative tolerance of 10 sprocket holes is $\pm 0.2 \mathrm{~mm}$
3. All dimensions in millimeters unless otherwise stated.


## Reel Drawing



FRONT VIEW


NOTES:

1. Reel shall be labeled with the following information (as a minimum).
a. manufacturers name or symbol
b. Agilent Technologies part number
c. purchase order number
d. date code
e. quantity of units
2. A certificate of compliance (c of c) shall be issued and accompany each shipment of product.
3. Reel must not be made with or contain ozone depleting materials.
4. All dimensions in millimeters (mm)

## Application Information

The following material is presented to assist in general design and use of the APCM-7833.

- 3.0V Characterization, for use in Data Card Applications
- cdma2000 1XRTT Description and Characterization data
- Design tips on various methods to control the bias on Ventl pin
- Description of ACPR measurement methods
- Description of Agilent evaluation demoboard for ACPM-7833
- IR Reflow Profile (applicable for all Agilent E-pHEMT PAs)


### 3.0 V Characterization, Data Card Applications

## Electrical Data

All tests are done in $50 \Omega$ system at $\mathrm{Vdd} 1=\mathrm{Vdd} 2=\mathrm{V}$ bias $=3.0 \mathrm{~V}, 25^{\circ} \mathrm{C}$, unless noted otherwise.

| Parameter | Units | Min | Typ | Max | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1900 MHz CDMA |  |  |  |  |  |
| Frequency Range | MHz | 1850 |  | 1910 |  |
| Gain (Fixed Cntl Voltage) |  |  |  |  |  |
| ( $\mathrm{P}_{\text {out }}=28.5 \mathrm{dBm}$ ) | dB |  | 26 |  | Vcntl $=2.5 \mathrm{~V}$ |
| $\left(\mathrm{P}_{\mathrm{out}}=13 \mathrm{dBm}\right)$ | dB |  | 28 |  | V cntl $=2.5 \mathrm{~V}$ |
| $\left(P_{\text {out }}=-5 \mathrm{dBm}\right)$ | dB |  | 28 |  | Ventl $=2.5 \mathrm{~V}$ |
| Power Added Efficiency |  |  |  |  |  |
| $\mathrm{P}_{\text {out }}=28.0 \mathrm{dBm}$ | \% |  | 42 |  | Ventl $=2.5 \mathrm{~V}$ |
| $\mathrm{P}_{\text {out }}=16 \mathrm{dBm}$ | \% |  | 8.5 |  | Vcntl $=2.5 \mathrm{~V}$ |
| Total Supply Current | mA |  | 500 |  | $\mathrm{P}_{\text {out }}=28.0 \mathrm{dBm}, \mathrm{Vcntl}=2.5 \mathrm{~V}$ |
|  |  |  | 100 |  | $P_{\text {out }}=13 \mathrm{dBm}, \mathrm{Vcntl}=1.6 \mathrm{~V}$ |
|  |  |  | 30 |  | $P_{\text {out }}=-5 \mathrm{dBm}, \mathrm{Vcntl}=1.2 \mathrm{~V}$ |
| ACPR @ $\pm 1.25 \mathrm{MHz}$ offset | $\mathrm{dBc} / 30 \mathrm{kHz}$ |  | -43 |  | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}$ |
| ACPR @ $\pm 1.98 \mathrm{MHz}$ offset | $\mathrm{dBc} / 30 \mathrm{kHz}$ |  | -56 |  | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}$ |
| Quiescent Current | mA |  | 60 |  | $\mathrm{P}_{\text {out }} \leq 28.5 \mathrm{dBm}, \mathrm{Vcntl}=2.5 \mathrm{~V}$ |
| Input VSWR |  |  |  |  |  |
| $\left(\mathrm{P}_{\mathrm{out}}=28.5 \mathrm{dBm}\right)$ |  |  | 2.0:1 |  |  |
| ( $\mathrm{P}_{\text {out }}=16 \mathrm{dBm}$ ) |  |  | 2.5:1 |  |  |
| Noise Figure | dB |  | 4.5 |  |  |
| Noise Power @ 80 MHz offset in 1930-1990 MHz | $\mathrm{dBm} / \mathrm{Hz}$ |  | -141 |  |  |
| Stability (Spurious): Load VSWR 5:1 | dBc |  | -50 |  | All phases |
| Harmonic Suppression |  |  |  |  |  |
| 2Fo | dBc |  | -40 |  |  |
| 3Fo | dBc |  | -40 |  |  |

Typical Performance, data measured in $50 \Omega$ system, Vdd1 $=\mathrm{Vdd} 2=\mathrm{V}$ bias $=3.0 \mathrm{~V}, \mathrm{Vcntl}=2.5 \mathrm{~V}, \mathrm{~T}=25^{\circ} \mathrm{C}$ and Freq $=1880 \mathrm{MHz}$.


Figure 9. Gain vs. Pout.


Figure 12. ACPR (1.25 MHz offset) vs. Pout.


Figure 15. Gain vs. Ventl.


Figure 10. PAE vs. Pout.


Figure 13. ACPR (1.98 MHz offset) vs. Pout.


Figure 11. Idd vs. Pout.


Figure 14. Harmonic Suppression vs. Pout.

## cdma 2000 1xRTT Characterization

## System Description

CDMA2000 is the TIA's standard for third generation (3G) technology and is an evolution of the IS95 CDMA format. CDMA2000 includes 1X RTT in the singlecarrier mode and 3X RTT in the multi-carrier mode. This paper describes the CDMA2000 1X RTT approach and its performance with Agilent 4x4 CDMA PAs, ACPM-7833. CDMA2000 1X RTT, being an extension of the IS-95
standard, has a chip rate of 1.2288Mchip/s. However, in $1 \times R T T$, the reverse link transmits more than one code channel to accommodate the high data rates. The minimum configuration consists of a reverse pilot (R-Pilot) channel for synchronous detection by the Base Transceiver System (BTS) and a reverse fundamental channel (R-FCH) for voice. Additional
channels such as the reverse supplemental channels (R-SCHs) and the reverse dedicated channel (R-DCCH) are used to send data or signaling information. Channels can exist at different rates and power levels.

Table 1 shows the transmitter specification in CDMA2000 reverse link.

Table 1. Transmitter Specification in Reverse Link.

| Specification |  | Spread Rate1 |
| :---: | :---: | :---: |
| ERP at Maximum Output Power |  | Lower limit +23 dBm Upper limit +30 dBm |
| Minimum Controlled Output Power |  | $-50 \mathrm{dBm} / 1.23 \mathrm{MHz}$ |
| Waveform Quality Factor and Frequency Accuracy |  | >0.944 |
|  | SR1, Band Class 0(Cellular band) | SR1, Band Class1(PCS band) |
| Maximum RF output power offset frequency within the range | 885 kHz to 1.98 MHz Less stringent of $-42 \mathrm{dBc} / 30 \mathrm{kHz}$ or $-54 \mathrm{dBm} / 1.23 \mathrm{MHz}$ | 1.25 MHz to 1.98 MHz Less stringent of $-42 \mathrm{dBc} / 30 \mathrm{kHz}$ or $-54 \mathrm{dBm} / 1.23 \mathrm{MHz}$ |
|  | 1.98 MHz to 3.125 MHz Less stringent of $-54 \mathrm{dBc} / 30 \mathrm{kHz}$ or $-54 \mathrm{dBm} / 1.23 \mathrm{MHz}$ | 1.98 MHz to 2.25 MHz <br> Less stringent of $-50 \mathrm{dBc} / 30 \mathrm{kHz}$ or $-54 \mathrm{dBm} / 1.23 \mathrm{MHz}$ |
|  | 3.125 MHz to 5.625 MHz $-13 \mathrm{dBm} / 100 \mathrm{kHz}$ | 2.25 MHz to 6.25 MHz <br> $-13 \mathrm{dBm} / 1 \mathrm{MHz}$ |

Typical channel configurations below are based on the transmitter test condition in the reverse link.

1) "Basic" Voice only configuration

- R-PICH @ -5.3dB
- R-FCH @ - 1.5 dB 9.6 kbps

2) Voice and Data configuration

- R-PICH @ -5.3 dB
- R-FCH @ - 4.54 dB 9.6 kbps
- R-SCH1 @ -4.54 dB 9.6 kbps


## 3) Voice and Control configuration

- R-PICH @ -5.3 dB
- R-FCH @ 3.85 dB 9.6 kbps
- R-DCCH @ -3.85 dB 9.6 kbps

4) Control channel only configuration

- R-PICH @ -5.3dB
- R-DCCH @ - 1.5 dB 9.6 kbps

Combinations of these channels will increase the peak to average power ratio for higher data rates. The complementary cumulative distribution function (CCDF) measurement characterizes the peak to average power statistics of CDMA2000 reverse link. For reference, the system specifications of peak to average power
ratio of IS-95 and CDMA2000 IX RTT are 3.9 dB and 5.4 dB at $1 \%$ CCDF respectively.

Higher peak to average power ratio requires a higher margin, both in higher power gain and in improved thermal stability for PA linearity to meet the minimum system specifications.

The test results below for the ACPM-7833 show the compliance to the system linearity specifications with 4 channel configurations, representing a broad crosssection of CDMA2000 1X RTT environments.

Test result of ACPM-7833 using CDMA2000 1X RTT signal
Test condition - PA Evaluation board with Vdd1=Vdd2=Vbias $=3.4 \mathrm{~V}$, Vcntl $=2.5 \mathrm{~V}$, Frequency $=1880 \mathrm{MHz}$. Test result with each channel configuration.

| Channel | IVdd(mA) | Pin(dBm) | $\mathbf{1 . 2 5 ~ M H z}$ <br> ACPR(dBc) | $\mathbf{1 . 2 5} \mathbf{M H z}$ <br> ACPR(dBc) | $\mathbf{- 1 . 9 8 ~ M H z}$ <br> ACPR(dBc) | +1.98 MHz <br> ACPR(dBc) | Pout(dBm) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Basic | 451.0 | -0.14 | -52.6 | -51.5 | -60.2 | -60 | 28 |
| Voice+Data | 435.0 | 0.52 | -46.2 | -45.7 | -58.0 | -58.3 | 28 |
| Voice+Cntl | 439.0 | 0.50 | -45.5 | -44.9 | -60.1 | -60 | 28 |
| Cntl only | 299.0 | -2.56 | -49.1 | -48.8 | -57.7 | -57.5 | 25.5 |

EIA/TIA-98-D indicates a 2.5 dB allowed back off in power for control channel only configuration.

Peak to average power ration (Pout $=16 \mathrm{dBm})$

| CCDF(\%) | Basic | Voice + Data | Voice + CNTL | CNTL only |
| :--- | :--- | :--- | :--- | :--- |
| 10 | 2.11 | 3.37 | 3.44 | 4.00 |
| $\mathbf{1}$ | 3.74 | 4.83 | 5.21 | 5.75 |
| 0.1 | 4.68 | 5.68 | 6.24 | 6.73 |
| 0.01 | 5.15 | 6.20 | 6.76 | 7.18 |
| 0.001 | 5.36 | 6.53 | 7.11 | 7.39 |
| 0.0001 | 5.48 | 6.63 | 7.17 | 7.45 |

## Design Tips to use Ventl pin

## Power Amplifier Control Using Ventl Pin on ACPM-7833

Power amplifier control scheme in CDMA systems is one of the important and challenging aspects of CDMA-based handset design. Handset designers must balance maintaining adequate linearity while optimizing efficiency at high, medium and low output power levels. The primary method to achieve these goals is to adjust the bias of the PA as a function of output power. Theoretically, the best efficiency would be achieved when the bias of the PA is continually adjusted based on the output power requirement of the PA. However, implementing this type of circuit can be complex and costly. Therefore several different approaches have been developed to provide an acceptable tradeoff between optimum efficiency and optimum manufacturability. This application section reviews four methods of controlling the bias of a CDMA power amplifier: fixed, step, logical and dynamic.

## 1. Fixed Bias Control

Using a fixed bias point on the PA is the traditional method, and it is the simplest. For example, the recommended value of the fixed control voltage on the Ventl pin for the ACPM-7833 is 2.5 V . The Ventl pin on the PA is controlled by PA_ON pin of the baseband IC. When PA_ON is HIGH, the output RF signal of the PA is enabled, enabling the subscriber unit to transmit the required data. The switch circuit also controls the on/off state of the PA.

Below is an example of how to control the the output of the PA using PA_ON and Ventl pins.

| Power Mode | PA_ON | Vcntl | Power Range |
| :--- | :--- | :--- | :--- |
| Shut Down | LOW | OV | - |
| High Power | HIGH | 2.5 V | $\leq 28.5 \mathrm{dBm}$ |



## 2. Step Bias Control and Dynamic

 Bias Control (if controled PDM1)The PDM1 output from the baseband IC can be used to create a software-programmable voltage, to be used at the phone designer's discretion. To get high efficiency and better ACPR, the phone designers can change control voltage of the PA by adjusting PDM1 voltage according to output power of PA. A caution when using this
approach—careful consideration must be made to to avoid an abrupt discontinuity in the output signal when the step bias control voltage is applied.

The figure below is an example of how to control the PA for multiple bias points using the PA_ON and Ventl pins.

| Power Mode | PA_ON | Vcntl | Power Range |
| :--- | :--- | :--- | :--- |
| Shut Down | LOW | OV | - |
| Low Power | HIGH | 1.2 V | $\sim-5 \mathrm{dBm}$ |
| Mid Power | HIGH | 1.6 V | $-5 \mathrm{dBm} \sim 13 \mathrm{dBm}$ |
| High Power | HIGH | 2.5 V | $13 \mathrm{dBm} \sim 28.5 \mathrm{dBm}$ |



If PDM1 can be controlled then same circuit can be used for Dynamic bias control

## 3. Dynamic Bias Control Alternate Implementation

Phone designers can use TX_ADC_ADJ pin of the baseband IC to get dynamic bias control with Ventl pin of PA. TX_ADC_ADJ is a PDM output pin produced by the TX AGC subsystem and used to control the gain of the Tx signal prior to
the PA. The variable output levels from two inverting operational amplifiers, generated and compared by TX_ADC_ADJ, provide dynamic control voltages for the Vcntl of $1.0 \mathrm{~V} \sim 2.7 \mathrm{~V}$ with a 0.1 V step.

$A v=-(\mathrm{V} 1 / \mathrm{Vin})=-\mathrm{R} 3 / \mathrm{R} 2$,
V1 = -(R3/R2)Vin,
Vo $=-(R 5 / R 4) V 1=[(R 5 * R 3) /(R 4 * R 2)] * V i n$

The using of combination of two pins, PDM1 and TX_ADC_ADJ, is another method of realizing a dynamic bias control scheme. The two OP Amps control the Vcntl voltage levels with compared and integrated circuits.


## ACPR Measurement Method

Adjacent-channel power ratio (ACPR) is used to characterize the distortion of power amplifiers and other subsystems for their tendency to cause interference with neighboring radio channels or systems. The ACPR measurement often is specified as the ratio of the power spectral density (PSD) of the CDMA main channel to the PSD measured at
several offset frequencies. For the Cellular band ( $824 \sim 849 \mathrm{MHz}$ transmitter channel), the two offsets are at $\pm 885 \mathrm{kHz}$ and $\pm 1.98 \mathrm{MHz}$ and the measurement resolution bandwidth specified is 30 kHz . These offsets are at $\pm 1.25 \mathrm{MHz}$ and $\pm 1.98 \mathrm{MHz}$ for the PCS band ( 1850 ~ 1910 MHz transmitter channel).


Figure 16. CDMA Adjacent-Channel Power Ratio Measurement.

## ACPR Testing Diagram Test

PA Test Setup


Figure 17. ACPR test equipment setup.

ACPM-7833 Test Result using VSA Transmitter Tester


Figure 18. ACPR measurement using VSA Transmitter tester.

## ACPR Test Results using Spectrum Analyzer



Figure 19. Example ACPR measurement using Spectrum Analyzer.

The meaning of 16 dB
The accurate ACPR measurement using Spectrum Analyzer needs to consider the normalization factor that is dependent on the Resolution Bandwidth, RBW, settings. The above figure (measurement shown at 836 MHz for general example) shows a comparison of the different ACPR measurement results as a function of various RBW values. As the RBW is reduced, less power is captured during the measurement and consequently the channel power is recorded as a
smaller value. For example, if the main channel power is measured as 28 dBm in a 1.23 MHz bandwidth, its power spectral density is $28 \mathrm{dBm} / 1.23 \mathrm{MHz}$, which can be normalized to $11.87 \mathrm{dBm} /$ 30 kHz . The equation used to calculate the normalization factor of power spectral density is:
Normalization Factor $=$ 10log[Normalization BW/Current BW (Spectrum Analyzer RBW)]
$=10 \log \left[1.23 \times 10^{6} / 30 \times 10^{3}\right]$
$=16.13 \mathrm{~dB}$

Since the ACPR in an IS95 system is specified in a 1.23 MHz bandwidth, a channel power that is measured using a different RBW, can be normalized to reflect the channel power as if it was measured in a 1.23 MHz bandwidth. The difference in channel power measured in 30 kHz bandwidth and the channel power measured in a 1.23 MHz bandwidth is 16 dB .

## ACPM-7833 Demoboard

Operation Instructions

## 1) Module Description

The ACPM-7833 is a fully matched Power Amplifier. The sample devices are provided on a demonstration PC Board with SMA connectors for RF inputs and outputs, and a DC connector for all bias and control I/O's. Please refer to Figures 20 through 23 and the Pin configuration table for I/O descriptions and connections.


Figure 20. ACPM-7833 Evaluation Board Schematic and Layout.


Figure 21. Layer 1 - Top Metal \& Solder Mask.


Figure 22. Layer 2 - Ground.


Figure 23. Layer 3 - Bottom Metal \& Solder Mask.

PIN Configuration Table

| Top side | Back side |  |
| :--- | :--- | :--- |
| 1 | GND | 1b |
| 2 | Vdd2 (s) |  |
| 3 | Vdd1 | 2b |
| 4 | GND | 3b |
| 5 | Vdd1 (s) |  |
|  | Vdd2 | 4b |

## 2) Circuit Operation

The design of the power module (PAM) provide bias control via Ventl to achieve optimal RF performance and power control. The control pin is labeled Vcntl. Please refer to for the block diagram of this PAM.

Typical Operation Conditions (Vdd1=Vdd2=Vbias = 3.4V)

| Parameter | ACPM-7833 |
| :--- | :--- |
| Frequency Range | $1850-1910 \mathrm{MHz}$ |
| Output Power | 28.5 dBm |
| Vcntl | 2.5 V |

3) Maximum Ratings

| Vdd | 5.0 V |
| :--- | :--- |
| Drain Current | 1.5 A |
| Ventl | 3 V |
| RF input | 10 dBm |
| Temperature | -30 to $85^{\circ} \mathrm{C}$ |

Please Note: Avoid Electrostatic Discharge on all I/O's.

## 4) Heat Sinking

The demonstration PC Board provides an adequate heat sink. Maximum device dissipation should be kept below 2.5 Watts.

## 5) Testing

- Signal Source

The CDMA modulated signal for the test is generated using an Agilent ESG-D4000A (or ESGD3000A) Digital Signal Generator with the following settings:

CDMA Setup : Reverse
Spreading: On
Bits/Symbol: 1
Data: PN15
Modulation: OQPSK
Chip Rate: 1.2288 Mcps
High Crest: On
Filter: Std
Phase Polarity: Invert

- ACPR Measurement

The ACPR (and channel power) is measured using an Agilent 4406 VSA with corresponding ACPR offsets for IS-98c and JSTD-8. Averaging of 10 is used for ACPR measurements.

- DC Connection

A DC connector is provided to allow ease of connection to the I/Os. Wires can be soldered to the connector pins, or the connector can be removed and I/Os contacted via clip leads or direct soldered connections. The wiring of I/Os are listed in Figures 20 through 23 and the Pin configuration table. The Vdd
sense connections are provided to allow the use of remotesensing power supplies of compensation for PCB traces and cable resistance.

- Device Operation

1) Connect RF Input and Output for the band under test.
2) Terminate all unused RF ports into 50 Ohms.
3) Connect Vdd1, Vdd2 and Vdd3 supplies (including remote sensing labeled Vdd1 S, Vdd2 S and Vbias S on the board). Nominal voltage is 3.4 V .
4) Connect Ventl supply and set reference voltage to the voltage shown in the data packet. Note that the Vcntl pin is on the back side of the demonstration board. Please limit Vcntl to not exceed the corresponding listed "DC Biasing Condition" in the Data Packet. Note that increasing Ventl over the corresponding listed "DC Biasing Condition" can result in power decrease and current can exceed the rated limit.
5) Apply RF input power according to the values listed in "Operation Data" in Data Packet.
6) Power down in opposite sequence.


Figure 24. Power Module Block Diagram.

## IR Reflow Soldering

Figure 25 is a straight-line representation of the recommended nominal time-temperature profile from JESD22-A113-B IR reflow.


Figure 25. Time-temperature Profile for IR Reflow Soldering Process.

Table 2. IR Reflow Process Zone.

| Process Zone | $\Delta$ Temperature | $\Delta$ Temperature $/ \Delta$ Time |
| :--- | :--- | :--- |
| Preheat Zone | $25^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ | $3^{\circ} \mathrm{C} / \mathrm{s} \mathrm{MAX}$ |
| Soak Zone | $100^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ | $0.5^{\circ} \mathrm{C} / \mathrm{s} \mathrm{MAX}(120 \mathrm{~s} \mathrm{MAX})$ |
| Reflow Zone | $150^{\circ} \mathrm{C}$ to $235^{\circ} \mathrm{C}\left(240^{\circ} \mathrm{C} \mathrm{MAX}\right)$ | $4.5^{\circ} \mathrm{C} / \mathrm{s} \mathrm{TYP}$ |
|  | $235^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ | $-4.5^{\circ} \mathrm{C} / \mathrm{s} \mathrm{TYP}$ |
| Cooling Zone | $150^{\circ} \mathrm{C}$ to $25^{\circ} \mathrm{C}$ | $-6^{\circ} \mathrm{C} / \mathrm{s} \mathrm{MAX}$ |

Table 3. Classification Reflow Profiles.

|  | Convection or IR/Convection |
| :--- | :--- |
| Average ramp-up rate $\left(183^{\circ} \mathrm{C}\right.$ to peak $)$ | $3^{\circ} \mathrm{C} /$ second max. |
| Preheat temperature $125( \pm 25)^{\circ} \mathrm{C}$ | 120 seconds max. |
| Temperature maintained above $183^{\circ} \mathrm{C}$ | $60-150$ seconds |
| Time within $5^{\circ} \mathrm{C}$ of actual peak temperature | $10-20$ seconds |
| Peak temperature range | $220+5 /-0^{\circ} \mathrm{C}$ or $235+5 /-0^{\circ} \mathrm{C}$ |
| Ramp-down rate | $6^{\circ} \mathrm{C} /$ second max. |
| Time $25^{\circ} \mathrm{C}$ to peak temperature | 6 minutes max. |
| Note: |  |
| All temperatures measured refer to the package body surface. |  |

Zone 1 - Preheat Zone
The average heat up rate for surface-mount component on PCB shall be less than $3^{\circ} \mathrm{C} /$ second to allow even heating for both the component and PCB. This ramp is maintained until it reaches $100^{\circ} \mathrm{C}$ where flux activation starts.

Zone 2 - Soak Zone
The flux is being activated here to prepare for even and smooth solder joint in subsequent zone. The temperature ramp is kept gradual to minimize thermal mismatch between solder, PC Board and components. Overramp rate here can cause solder splatter due to excessive oxidation of paste.

## Zone 3 - Reflow Zone

The third process zone is the solder reflow zone. The temperature in this zone rises rapidly from $183^{\circ} \mathrm{C}$ to peak temperature of $235^{\circ} \mathrm{C}$ for the solder to trans-
form its phase from solid to liquids. The dwell time at melting point $183^{\circ} \mathrm{C}$ shall maintain at between 60 to 150 seconds. Upon the duration of $10-20$ seconds at peak temperature, it is then cooled down rapidly to allow the solder to freeze and form solid.

Extended duration above the solder melting point can potentially damage temperature sensitive components and result in excessive inter-metallic growth that causes brittle solder joint, weak and unreliable connections. It can lead to unnecessary damage to the PC Board and discoloration to component's leads.

## Zone 4 - Cooling Zone

The temperature ramp down rate is $6^{\circ} \mathrm{C} / \mathrm{sec}$ ond maximum. It is important to control the cooling rate as fast as possible in order to achieve the smaller grain size for solder and increase fatigue resistance of solder joint.

| Nominal stencil thickness | Component lead pitch |
| :--- | :--- |
| $0.102 \mathrm{~mm}(0.004 \mathrm{in})$ | Lead pitch less than $0.508 \mathrm{~mm}(0.020 \mathrm{in})$ |
| $0.152 \mathrm{~mm}(0.006 \mathrm{in})$ | 0.508 mm to $0.635 \mathrm{~mm}(0.02 \mathrm{in}$ to 0.025 in$)$ |
| $0.203 \mathrm{~mm}(0.008 \mathrm{in})$ | Lead pitch greater than $0.635 \mathrm{~mm}(0.025 \mathrm{in})$ |

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Obsoletes 5989-0403EN
November 10, 2004
Agilent Technologies
5989-1899EN

