

## Dual and Quad 12MHz, 400V/µs Op Amps

#### **FEATURES**

- 12MHz Gain-Bandwidth
- 400V/µs Slew Rate
- 1.25mA Maximum Supply Current per Amplifier
- Unity Gain Stable
- C-Load<sup>™</sup> Op Amp Drives All Capacitive Loads
- 10nV/√Hz Input Noise Voltage
- 800uV Maximum Input Offset Voltage
- 300nA Maximum Input Bias Current
- 70nA Maximum Input Offset Current
- 12V/mV Minimum DC Gain. R<sub>1</sub>=1k
- 230ns Settling Time to 0.1%, 10V Step
- 280ns Settling Time to 0.01%, 10V Step
- $\pm 12.5$ V Minimum Output Swing into  $500\Omega$
- ±3V Minimum Output Swing into 150Ω
- Specified at ±2.5V, ±5V, and ±15V

#### **APPLICATIONS**

- Wideband Amplifiers
- Buffers
- Active Filters
- Data Acquisition Systems
- Photodiode Amplifiers

### DESCRIPTION

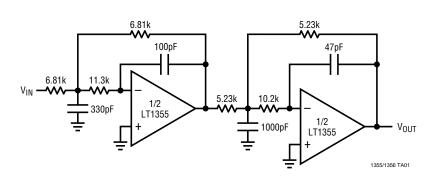
The LT1355/LT1356 are dual and quad low power high speed operational amplifiers with outstanding AC and DC performance. The amplifiers feature much lower supply current and higher slew rate than devices with comparable bandwidth. The circuit topology is a voltage feedback amplifier with matched high impedance inputs and the slewing performance of a current feedback amplifier. The high slew rate and single stage design provide excellent settling characteristics which make the circuit an ideal choice for data acquisition systems. Each output drives a  $500\Omega$  load to  $\pm 12.5 \text{V}$  with  $\pm 15 \text{V}$  supplies and a  $150\Omega$  load to  $\pm 3 \text{V}$  on  $\pm 5 \text{V}$  supplies. The amplifiers are stable with any capacitive load making them useful in buffer applications.

The LT1355/LT1356 are members of a family of fast, high performance amplifiers using this unique topology and employing Linear Technology Corporation's advanced bipolar complementary processing. For a single amplifier version of the LT1355/LT1356 see the LT1354 data sheet. For higher bandwidth devices with higher supply currents see the LT1357 through LT1365 data sheets. Bandwidths of 25MHz, 50MHz, and 70MHz are available with 2mA, 4mA, and 6mA of supply current per amplifier. Singles, duals, and guads of each amplifier are available.

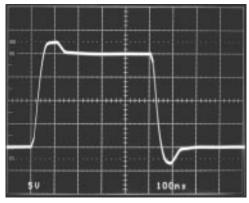
C-Load is a trademark of Linear Technology Corporation

## TYPICAL APPLICATION

100kHz, 4th Order Butterworth Filter



 $A_V = -1$  Large-Signal Response



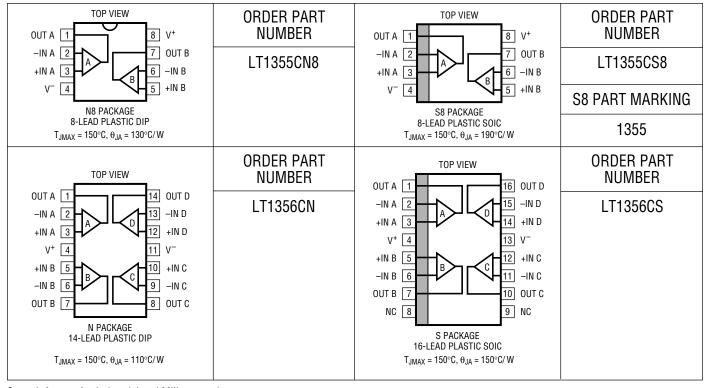
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### **ABSOLUTE MAXIMUM RATINGS**

Total Supply Voltage (V+ to V-)	36V
Differential Input Voltage	±10V
Input Voltage	±V <sub>S</sub>
Output Short-Circuit Duration (Note 1)	Indefinite
Operating Temperature Range	-40°C to 85°C

Specified Temperature Range	40°C to 85°C
Maximum Junction Temperature (See I	Below)
Plastic Package	150°C
Storage Temperature Range	. −65°C to 150°C
Lead Temperature (Soldering, 10 sec).	300°C

## PACKAGE/ORDER INFORMATION



Consult factory for Industrial and Military grade parts.

## **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
$\overline{V_{0S}}$	Input Offset Voltage		±15V		0.3	0.8	mV
			±5V		0.3	0.8	mV
			±2.5V		0.4	1.0	mV
I <sub>0S</sub>	Input Offset Current		±2.5V to ±15V		20	70	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V		80	300	nA
e <sub>n</sub>	Input Noise Voltage	f = 10kHz	±2.5V to ±15V		10		nV/√Hz
in	Input Noise Current	f = 10kHz	±2.5V to ±15V		0.6		pA/√Hz
R <sub>IN</sub>	Input Resistance	V <sub>CM</sub> = ±12V	±15V	70	160		MΩ
	Input Resistance	Differential	±15V		11		MΩ
C <sub>IN</sub>	Input Capacitance		±15V		3		pF

# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN TYP MAX	UNITS
	Input Voltage Range +		±15V	12.0 13.4	V
			±5V	2.5 3.5	V
			±2.5V	0.5 1.1	V
	Input Voltage Range -		±15V	-13.2 -12.0	V
			±5V ±2.5V		V V
CMRR	Common Made Painstian Patia	V <sub>CM</sub> = ±12V	±15V		dB
CIVIRK	Common-Mode Rejection Ratio	$V_{CM} = \pm 12V$ $V_{CM} = \pm 2.5V$	±15V ±5V	83 97 78 84	dB
		$V_{CM} = \pm 0.5V$	±2.5V	68 75	dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		92 106	dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$V_{OUT} = \pm 12V, R_L = 1k$	±15V	12 36	V/mV
.02		$V_{OUT} = \pm 10V$ , $R_L = 500\Omega$	±15V	5 15	V/mV
		$V_{OUT} = \pm 2.5V, R_L = 1k$	±5V	12 36	V/mV
		$V_{OUT} = \pm 2.5 V$ , $R_L = 500 \Omega$	±5V	5 15	V/mV
		$V_{OUT} = \pm 2.5 \text{V}, R_L = 150 \Omega$	±5V	1 4	V/mV
		$V_{OUT} = \pm 1V$ , $R_L = 500\Omega$	±2.5V	5 20	V/mV
$V_{OUT}$	Output Swing	$R_L = 1k, V_{IN} = \pm 40mV$	±15V	13.3 13.8	±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 40 \text{mV}$	±15V ±5V	12.5 13.0 3.5 4.0	±V ±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 40$ mV $R_L = 150\Omega$ , $V_{IN} = \pm 40$ mV	±5V ±5V	3.0 3.3	± V ± V
		$R_L = 500\Omega$ , $V_{IN} = \pm 40$ mV	±2.5V	1.3 1.7	± V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 12.5V$	±15V	25 30	mA
1001	Output ourrein	$V_{OUT} = \pm 12.3V$	±5V	20 25	mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	30 42	mA
SR	Slew Rate	$A_V = -2$ , (Note 2)	±15V	200 400	V/µs
			±5V	70 120	V/µs
	Full Power Bandwidth	10V Peak, (Note 3)	±15V	6.4	MHz
		3V Peak, (Note 3)	±5V	6.4	MHz
GBW	Gain-Bandwidth	$f = 200kHz, R_L = 2k$	±15V	9.0 12.0	MHz
			±5V	7.5 10.5	MHz
	Dies Tieses Fall Tieses	1 100/ 000/ 0.11/	±2.5V	9.0	MHz
t <sub>r</sub> , t <sub>f</sub>	Rise Time, Fall Time	A <sub>V</sub> = 1, 10%-90%, 0.1V	±15V ±5V	14 17	ns ns
	Overshoot	A <sub>V</sub> = 1, 0.1V	±15V	20	<u> </u>
		.,	±5V	18	%
	Propagation Delay	50% V <sub>IN</sub> to 50% V <sub>OUT</sub> , 0.1V	±15V	16	ns
			±5V	19	ns
ts	Settling Time	10V Step, 0.1%, $A_V = -1$	±15V	230	ns
		10V Step, 0.01%, $A_V = -1$	±15V	280	ns
		5V Step, 0.1%, $A_V = -1$	±5V	240	ns
		5V Step, 0.01%, A <sub>V</sub> = -1	±5V	380	ns
	Differential Gain	$f = 3.58MHz, A_V = 2, R_L = 1k$	±15V	2.2	%
			±5V	2.1	<u>%</u>
	Differential Phase	$f = 3.58MHz, A_V = 2, R_L = 1k$	±15V	3.1	Deg
		4 ( (00))	±5V	3.1	Deg
$R_0$	Output Resistance	A <sub>V</sub> = 1, f = 100kHz	±15V	0.7	Ω
	Channel Separation	$V_{OUT} = \pm 10V$ , $R_L = 500\Omega$	±15V	100 113	dB
I <sub>S</sub>	Supply Current	Each Amplifier	±15V	1.0 1.25	mA m^
		Each Amplifier	±5V	0.9 1.20	mA



# **ELECTRICAL CHARACTERISTICS** $0 ^{\circ} \text{C} \leq \text{T}_{A} \leq 70 ^{\circ} \text{C}$ , $\text{V}_{\text{CM}} = 0 \text{V}$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage		±15V ±5V ±2.5V	•		1.0 1.0 1.2	mV mV mV
	Input V <sub>OS</sub> Drift	(Note 4)	±2.5V to ±15V	•	5	8	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V	•		100	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V	•		450	nA
CMRR	Common-Mode Rejection Ratio	$V_{CM} = \pm 12V$ $V_{CM} = \pm 2.5V$ $V_{CM} = \pm 0.5V$	±15V ±5V ±2.5V	<ul><li>81</li><li>77</li><li>67</li></ul>			dB dB dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		• 90			dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$\begin{array}{c} V_{OUT} = \pm 12V, \ R_L = 1k \\ V_{OUT} = \pm 10V, \ R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \ R_L = 1k \\ V_{OUT} = \pm 2.5V, \ R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \ R_L = 150\Omega \\ V_{OUT} = \pm 1V, \ R_L = 500\Omega \end{array}$	±15V ±15V ±5V ±5V ±5V ±2.5V	<ul> <li>10.0</li> <li>3.3</li> <li>10.0</li> <li>3.3</li> <li>0.6</li> <li>3.3</li> </ul>			V/mV V/mV V/mV V/mV V/mV V/mV
V <sub>OUT</sub>	Output Swing	$\begin{array}{l} R_L = 1k,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \\ R_L = 150\Omega,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \end{array}$	±15V ±15V ±5V ±5V ±2.5V	<ul> <li>13.2</li> <li>12.0</li> <li>3.4</li> <li>2.8</li> <li>1.2</li> </ul>			±V ±V ±V ±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 12V$ $V_{OUT} = \pm 2.8V$	±15V ±5V	<ul><li>24.0</li><li>18.7</li></ul>			mA mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	• 24			mA
SR	Slew Rate	$A_V = -2$ , (Note 2)	±15V ±5V	<ul><li>150</li><li>60</li></ul>			V/μs V/μs
GBW	Gain-Bandwidth	f = 200kHz, R <sub>L</sub> = 2k	±15V ±5V	<ul><li>7.5</li><li>6.0</li></ul>			MHz MHz
	Channel Separation	$V_{OUT} = \pm 10V, R_L = 500\Omega$	±15V	• 98			dB
I <sub>S</sub>	Supply Current	Each Amplifier Each Amplifier	±15V ±5V	•		1.45 1.40	mA mA

# **ELECTRICAL CHARACTERISTICS** $-40^{\circ}C \le T_{A} \le 85^{\circ}C$ , $V_{CM}$ = 0V unless otherwise noted. (Note 5)

SYMBOL V <sub>OS</sub>	PARAMETER Input Offset Voltage	put Offset Voltage :	V <sub>SUPPLY</sub>	V <sub>SUPPLY</sub>		TYP	MAX	UNITS
			±15V ±5V	•			1.5 1.5	mV mV
			±2.5V	•			1.7	mV
	Input V <sub>OS</sub> Drift	(Note 4)	±2.5V to ±15V	•		5	8	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V	•			200	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V	•			550	nA
CMRR	Common-Mode Rejection Ratio	V <sub>CM</sub> = ±12V	±15V	•	80			dB
		$V_{CM} = \pm 2.5V$	±5V	•	76			dB
		$V_{CM} = \pm 0.5V$	±2.5V	•	66			dB
PSRR	Power Supply Rejection Ratio	V <sub>S</sub> = ±2.5V to ±15V		•	90			dB

# **ELECTRICAL CHARACTERISTICS** $-40^{\circ}C \le T_A \le 85^{\circ}C$ , $V_{CM}$ = 0V unless otherwise noted. (Note 5)

SYMBOL	PARAMETER	CONDITIONS	VSUPPLY		MIN	TYP	MAX	UNITS
A <sub>VOL</sub>	Large-Signal Voltage Gain	$\begin{array}{c} V_{OUT} = \pm 12V, \ R_L = 1k \\ V_{OUT} = \pm 10V, \ R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \ R_L = 1k \\ V_{OUT} = \pm 2.5V, \ R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \ R_L = 150\Omega \\ V_{OUT} = \pm 1V, \ R_L = 500\Omega \end{array}$	±15V ±15V ±5V ±5V ±5V ±2.5V	•	7.0 1.7 7.0 1.7 0.4 1.7			V/mV V/mV V/mV V/mV V/mV V/mV
V <sub>OUT</sub>	Output Swing	$\begin{array}{l} R_L = 1 k,  V_{IN} = \pm 40 mV \\ R_L = 500 \Omega,  V_{IN} = \pm 40 mV \\ R_L = 500 \Omega,  V_{IN} = \pm 40 mV \\ R_L = 150 \Omega,  V_{IN} = \pm 40 mV \\ R_L = 500 \Omega,  V_{IN} = \pm 40 mV \end{array}$	±15V ±15V ±5V ±5V ±2.5V	•	13.0 11.5 3.4 2.6 1.2			±V ±V ±V ±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 11.5V$ $V_{OUT} = \pm 2.6V$	±15V ±5V	•	23.0 17.3			mA mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V, V_{IN} = \pm 3V$	±15V	•	23			mA
SR	Slew Rate	$A_V = -2$ , (Note 2)	±15V ±5V	•	120 50			V/μs V/μs
GBW	Gain-Bandwidth	f = 200kHz, R <sub>L</sub> = 2k	±15V ±5V	•	7.0 5.5			MHz MHz
	Channel Separation	$V_{OUT} = \pm 10V, R_L = 500\Omega$	±15V	•	98			dB
I <sub>S</sub>	Supply Current	Each Amplifier Each Amplifier	±15V ±5V	•			1.50 1.45	mA mA

The lacktriangle denotes specifications that apply over the full operating temperature range.

**Note 1**: A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

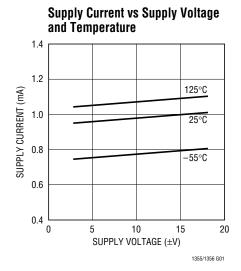
**Note 2**: Slew rate is measured between  $\pm 10V$  on the output with  $\pm 6V$  input for  $\pm 15V$  supplies and  $\pm 1V$  on the output with  $\pm 1.75V$  input for  $\pm 5V$  supplies.

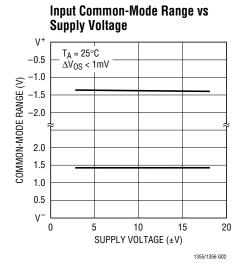
**Note 3**: Full power bandwidth is calculated from the slew rate measurement: FPBW =  $(SR)/2\pi V_P$ .

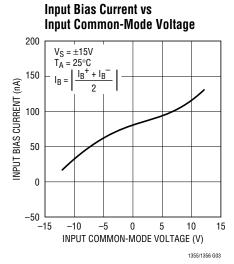
**Note 4**: This parameter is not 100% tested.

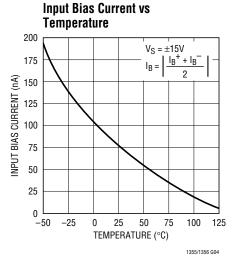
**Note 5**: The LT1355/LT1356 are not tested and are not quality-assurance sampled at  $-40^{\circ}$ C and at 85°C. These specifications are guaranteed by design, correlation, and/or inference from 0°C, 25°C, and/or 70°C tests.

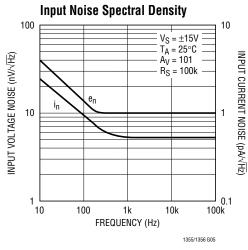
### TYPICAL PERFORMANCE CHARACTERISTICS

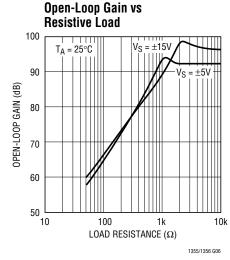


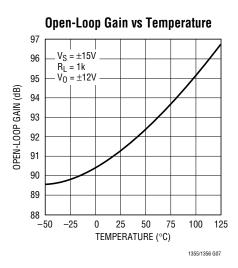


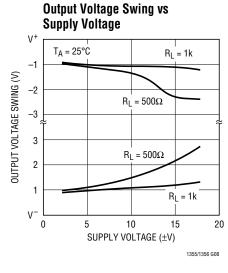


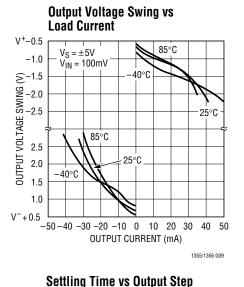


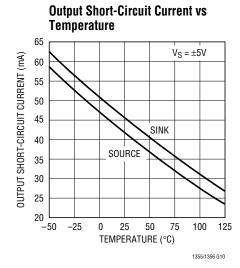


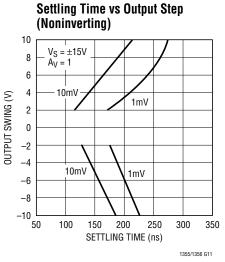


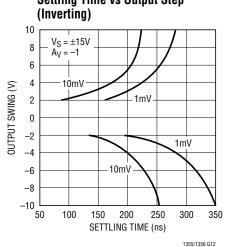


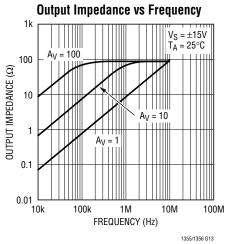


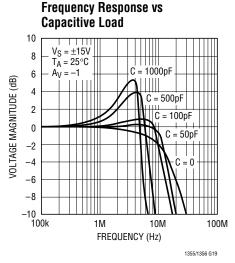


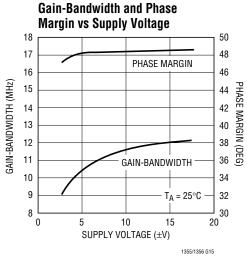


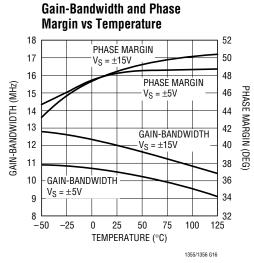


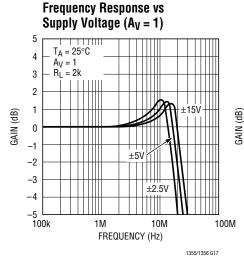


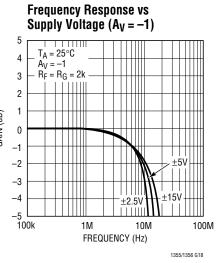


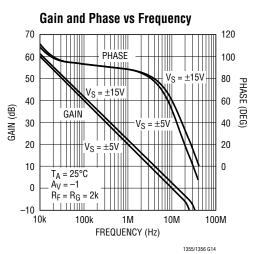


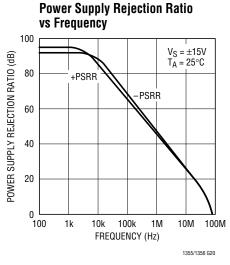


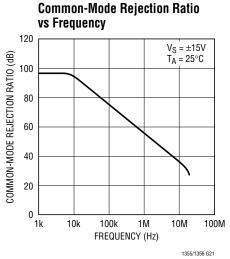


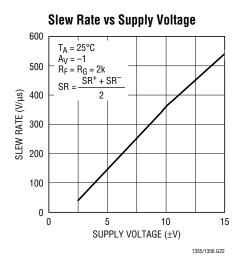


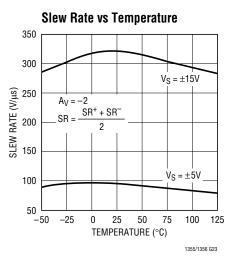


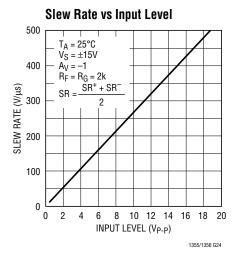


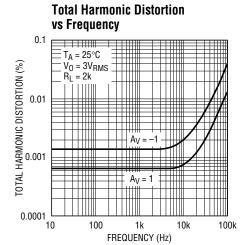




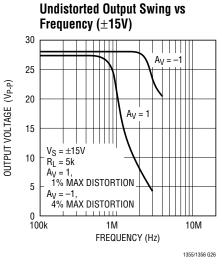


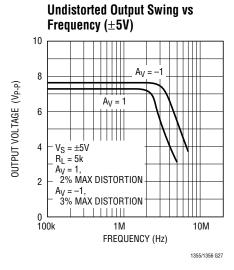


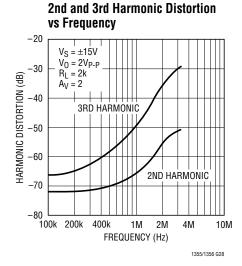


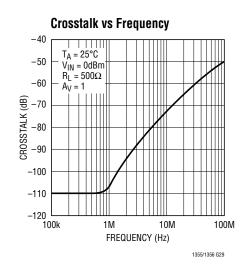


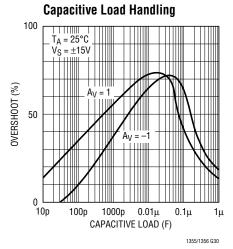
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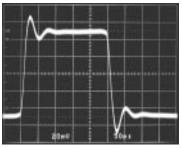






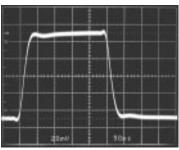


Small-Signal Transient  $(A_V = 1)$ 



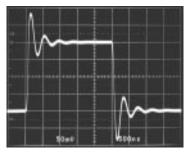
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**Small-Signal Transient**  $(A_V = -1)$ 



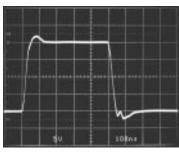
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**Small-Signal Transient**  $(A_V = -1, C_L = 1000pF)$ 



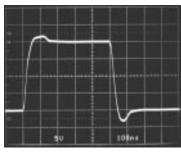
1355/1356 G33

Large-Signal Transient  $(A_V = 1)$ 



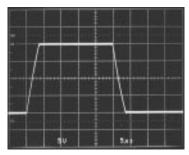
1355/1356 G34

Large-Signal Transient  $(A_V = -1)$ 



1355/1356 G35

**Large-Signal Transient**  $(A_V = 1, C_L = 10,000pF)$ 



1355/1356 G36

## APPLICATIONS INFORMATION

### **Layout and Passive Components**

The LT1355/LT1356 amplifiers are easy to use and tolerant of less than ideal layouts. For maximum performance (for example, fast 0.01% settling) use a ground plane. short lead lengths, and RF-quality bypass capacitors  $(0.01\mu F \text{ to } 0.1\mu F)$ . For high drive current applications use low ESR bypass capacitors (1µF to 10µF tantalum).

The parallel combination of the feedback resistor and gain setting resistor on the inverting input combine with the input capacitance to form a pole which can cause peaking or oscillations. If feedback resistors greater than  $5k\Omega$  are used, a parallel capacitor of value

$$C_F > R_G \times C_{IN}/R_F$$

should be used to cancel the input pole and optimize dynamic performance. For unity-gain applications where a large feedback resistor is used. C<sub>F</sub> should be greater than or equal to C<sub>IN</sub>.

### **Capacitive Loading**

The LT1355/LT1356 are stable with any capacitive load. As the capacitive load increases, both the bandwidth and phase margin decrease so there will be peaking in the frequency domain and in the transient response. Coaxial cable can be driven directly, but for best pulse fidelity a resistor of value equal to the characteristic impedance of the cable (i.e.,  $75\Omega$ ) should be placed in series with the output. The other end of the cable should be terminated with the same value resistor to ground.

#### APPLICATIONS INFORMATION

#### **Input Considerations**

Each of the LT1355/LT1356 amplifier inputs is the base of an NPN and PNP transistor whose base currents are of opposite polarity and provide first-order bias current cancellation. Because of variation in the matching of NPN and PNP beta, the polarity of the input current can be positive or negative. The offset current does not depend on beta matching and is well controlled. The use of balanced source resistance at each input is recommended for applications where DC accuracy must be maximized. The inputs can withstand differential input voltages of up to 10V without damage and need no clamping or source resistance for protection.

#### **Circuit Operation**

The LT1355/LT1356 circuit topology is a true voltage feedback amplifier that has the slewing behavior of a current feedback amplifier. The operation of the circuit can be understood by referring to the simplified schematic. The inputs are buffered by complementary NPN and PNP emitter followers which drive an  $800\Omega$  resistor. The input voltage appears across the resistor generating currents which are mirrored into the high impedance node. Complementary followers form an output stage which buffers the gain node from the load. The bandwidth is set by the input resistor and the capacitance on the high impedance node. The slew rate is determined by the current available to charge the gain node capacitance. This current is the differential input voltage divided by R1. so the slew rate is proportional to the input. Highest slew rates are therefore seen in the lowest gain configurations. For example, a 10V output step in a gain of 10 has only a 1V input step, whereas the same output step in unity gain has a 10 times greater input step. The curve of Slew Rate vs Input Level illustrates this relationship. The LT1355/ LT1356 are tested for slew rate in a gain of -2 so higher slew rates can be expected in gains of 1 and -1, and lower slew rates in higher gain configurations.

The RC network across the output stage is bootstrapped when the amplifier is driving a light or moderate load and has no effect under normal operation. When driving a capacitive load (or a low value resistive load) the network is incompletely bootstrapped and adds to the compensation at the high impedance node. The added capacitance slows down the amplifier which improves the phase margin by moving the unity-gain frequency away from the pole formed by the output impedance and the capacitive load. The zero created by the RC combination adds phase to ensure that even for very large load capacitances, the total phase lag can never exceed 180 degrees (zero phase margin) and the amplifier remains stable.

#### **Power Dissipation**

The LT1355/LT1356 combine high speed and large output drive in small packages. Because of the wide supply voltage range, it is possible to exceed the maximum junction temperature under certain conditions. Maximum junction temperature  $(T_J)$  is calculated from the ambient temperature  $(T_A)$  and power dissipation  $(P_D)$  as follows:

LT1355CN8:  $T_J = T_A + (P_D \times 130^{\circ}\text{C/W})$ LT1355CS8:  $T_J = T_A + (P_D \times 190^{\circ}\text{C/W})$ LT1356CN:  $T_J = T_A + (P_D \times 110^{\circ}\text{C/W})$ LT1356CS:  $T_J = T_A + (P_D \times 150^{\circ}\text{C/W})$ 

Worst case power dissipation occurs at the maximum supply current and when the output voltage is at 1/2 of either supply voltage (or the maximum swing if less than 1/2 supply voltage). For each amplifier  $P_{DMAX}$  is:

$$P_{DMAX} = (V^+ - V^-)(I_{SMAX}) + (V^+/2)^2/R_L$$

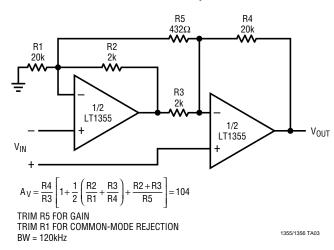
Example: LT1356 in S16 at 70°C,  $V_S = \pm 15V$ ,  $R_L = 1k$ 

$$P_{DMAX} = (30V)(1.45mA) + (7.5V)^2/1kW = 99.8mW$$

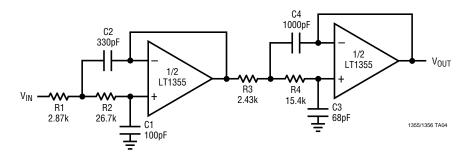
$$T_{JMAX} = 70^{\circ}C + (4 \times 99.8 \text{mW})(150^{\circ}C/W) = 130^{\circ}C$$

## TYPICAL APPLICATIONS

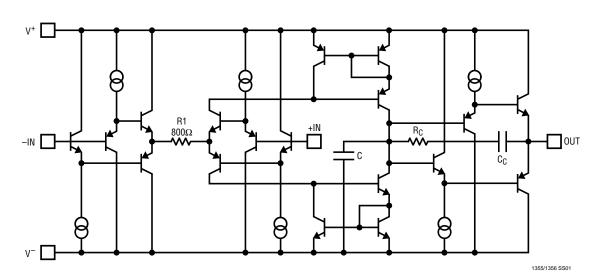
#### **Instrumentation Amplifier**



# 100kHz, 4th Order Butterworth Filter (Sallen-Key)



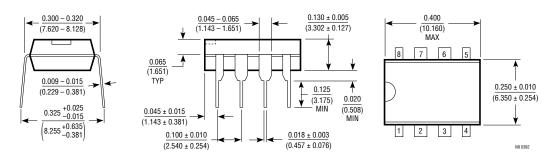
## SIMPLIFIED SCHEMATIC



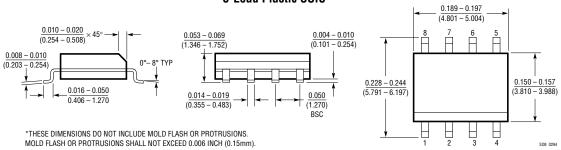
#### PACKAGE DESCRIPTION

Dimension in inches (millimeters) unless otherwise noted.

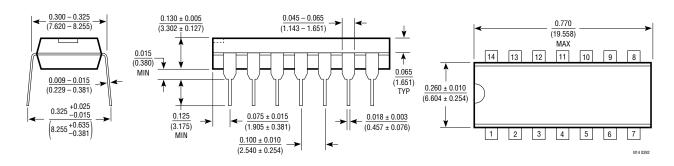
#### N8 Package 8-Lead Plastic DIP



#### S8 Package 8-Lead Plastic SOIC



#### N Package 14-Lead Plastic DIP



#### S Package 16-Lead Plastic SOIC

