

### General Description

The AAT2806 is a dual charge pump designed to support both the white LED backlight and flash applications for systems operating with lithium-ion/polymer batteries. The backlight charge pump is capable of driving up to four LEDs at a total of 80mA. The current sinks may be operated individually or in parallel for driving higher current LEDs. To maximize power efficiency, the charge pump operates in 1X, 1.5X, or 2X mode, where the mode of operation is automatically selected by comparing the forward voltage of each LED with the input voltage. AnalogicTech's S<sup>2</sup>Cwire™ (Simple Serial Control™) serial digital input is used to enable, disable, and set current for each LED with an eight-level logarithmic scale plus four low-current settings down to 50μA for optimized efficiency, with a typical operating quiescent current of less than 50μA.

The flash charge pump is a charge pump doubler with a regulated output voltage. It is designed to deliver 120mA of continuous current and up to 250mA of pulsed current. It has an independent enable pin for improved power savings.

The AAT2806 has thermal protection and built-in soft-start circuitry. A low-current shutdown feature disconnects the load from V<sub>IN</sub> and reduces quiescent current to less than 1μA.

The AAT2806 is available in a Pb-free, space-saving, thermally-enhanced TDFN44-16 package and is rated over the -40°C to +85°C temperature range.

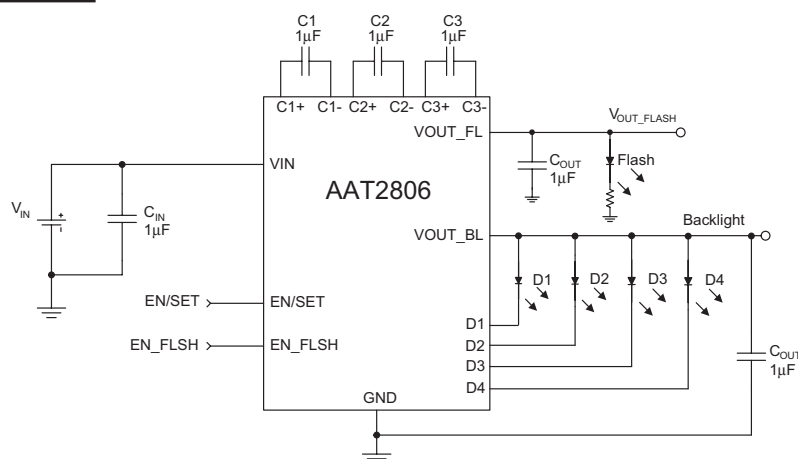
### Features

- V<sub>IN</sub> Range: 2.7V to 5.5V
- Dual Charge Pump to Support Backlight and Flash LEDs
- Backlight Charge Pump:
  - Regulated Current
  - Four Current Sink Inputs
  - S<sup>2</sup>Cwire Brightness Control
  - Tri-Mode Charge Pump
  - Maximum 20mA of Current Per Input
  - Low I<sub>Q</sub> (50μA) in Light Load Mode
- Flash Charge Pump:
  - Regulated Output Voltage
  - Up to 250mA of Pulsed Current
- Independent Backlight/Flash Control
- Low Noise 1MHz Constant Frequency Operation
- Automatic Soft Start
- No Inductors
- Available in TDFN44-16 Package

### Applications

- Color (RGB) Lighting
- White LED Backlighting
- White LED Photo Flash

### Typical Application

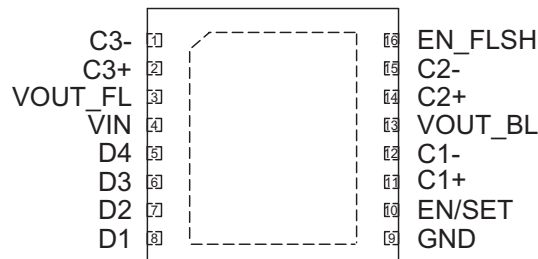


### Pin Descriptions

Pin #	Symbol	Function
1	C3-	Flying capacitor 3 negative terminal.
2	C3+	Flying capacitor 3 positive terminal. Connect a 1 $\mu$ F capacitor between C3+ and C3-.
3	VOUT_FL	Regulated output voltage for the flash LED. Requires 1 $\mu$ F capacitor connected between this pin and ground.
4	VIN	Input power supply. Requires 1 $\mu$ F capacitor connected between this pin and ground.
5	D4	Current sink input 4.
6	D3	Current sink input 3.
7	D2	Current sink input 2.
8	D1	Current sink input 1.
9	GND	Ground.
10	EN/SET	S <sup>2</sup> Cwire serial interface control pin. It is used to enable/disable the backlight charge pump and to control the brightness of the white LEDs.
11	C1+	Flying capacitor 1 positive terminal. Connect a 1 $\mu$ F capacitor between C1+ and C1-.
12	C1-	Flying capacitor 1 negative terminal.
13	VOUT_BL	Regulated output voltage for the white LEDs. Requires 1 $\mu$ F capacitor connected between this pin and ground.
14	C2+	Flying capacitor 2 positive terminal. Connect a 1 $\mu$ F capacitor between C2+ and C2-.
15	C2-	Flying capacitor 2 negative terminal.
16	EN_FLSH	Enable/disable pin for the flash charge pump.
EP		Exposed paddle (bottom); connect to GND directly beneath package.

### Pin Configuration

**TDFN44-16  
(Top View)**



### Absolute Maximum Ratings<sup>1</sup>

Symbol	Description	Value	Units
$V_{IN}$	Input Voltage	-0.3 to 6.0	V
$V_{EN/SET}; EN\_FL$	EN/SET; EN_FL to GND Voltage	-0.3 to $V_{IN} + 0.3$	V
$T_{LEAD}$	Maximum Soldering Temperature (at leads, 10 sec)	300	°C

### Thermal Information<sup>2</sup>

Symbol	Description	Value	Units
$P_D$	Maximum Power Dissipation <sup>3</sup>	2.0	W
$\theta_{JA}$	Maximum Thermal Resistance	50	°C/W

1. Stresses above those listed in Absolute Maximum Ratings may cause permanent damage to the device. Functional operation at conditions other than the operating conditions specified is not implied. Only one Absolute Maximum Rating should be applied at any one time.
2. Mounted on an FR4 board.
3. Derate 6.25mW/°C above 25°C.

### Electrical Characteristics<sup>1</sup>

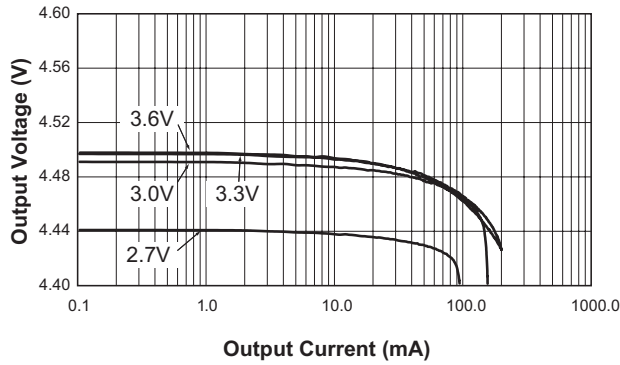
$V_{IN} = 3.6V$ ;  $C_{IN} = C_{OUT} = C_1 = C_2 = C_3 = 1.0\mu F$ ;  $T_A = -40^\circ C$  to  $+85^\circ C$ , unless otherwise noted.  
Typical values are  $T_A = 25^\circ C$ .

Symbol	Description	Conditions	Min	Typ	Max	Units
<b>Input Power Supply</b>						
$V_{IN}$	Operation Range		2.7		5.5	V
$I_{CC}$	Operating Current	1X Mode, $3.0 \leq V_{IN} \leq 5.5$ , Active, No Load Current; EN_FLSH = GND, EN/SET = $V_{IN}$		0.3	1	mA
		1.5X Mode, $3.0 \leq V_{IN} \leq 5.5$ , Active, No Load Current; EN_FLSH = GND, EN/SET = $V_{IN}$		1.0	3.0	
		2X Mode, $3.0 \leq V_{IN} \leq 5.5$ , Active, No Load Current; EN_FLSH = GND, EN/SET = $V_{IN}$		2.0	3.7	
		EN_FLSH = GND, 50 $\mu A$ Output Setting, 1X Mode		50		$\mu A$
		$3.0 \leq V_{IN} \leq 5.5$ , No Load Current; EN_FLSH = $V_{IN}$ , EN/SET = GND		2.0	4.5	mA
$I_{SHDN}$	Shutdown Current	EN_FLSH = EN/SET = 0			1.0	$\mu A$
$I_{DX}$	Input Current Accuracy <sup>2,3</sup>	$I_{SET} = 20mA$ and $I_{SET} = 4.1mA$ ; $T_A = 25^\circ C$	-10		10	%
$I_{(D-Match)}$	Current Matching Between Any Two Current Sink Inputs <sup>2,4</sup>	VD1:D4 = 3.6V, $V_{IN} = 3.5V$		0.5		%
$R_{SINK}$	Sink Switch Impedance (each) <sup>2</sup>			7		$\Omega$
$V_{OUT\_FL}$	Flash Charge Pump Output Voltage <sup>5</sup>	$3.0V < V_{IN} < 5V$ , $I_{OUT} = 100mA$ ; EN_FLSH = $V_{IN}$	4.32	4.5	4.68	V
		$3.0V < V_{IN} < 5V$ , $I_{OUT} = 150mA$ ; EN_FLSH = $V_{IN}$	4.3	4.5	4.7	
$I_{OUT\_FL}$	Maximum Continuous $I_{OUT}$ <sup>5</sup> Maximum Pulsed $I_{OUT}$ <sup>5</sup>	$V_{IN} = 3.6V$ ; $V_{OUT} = 4.5V$ ; EN_FLSH = $V_{IN}$	120			mA
		$V_{IN} = 3.6V$ ; $V_{OUT} = 4.5V$ ; $I_{PULSED} < 500ms$	250			
$T_{SS}$	Soft-Start Time			100		$\mu s$
$F_{CLK}$	Clock Frequency			1.0		MHz
$V_{EN(L)}$	Enable Threshold Low				0.4	V
$V_{EN(H)}$	Enable Threshold High		1.4			V
$T_{EN/SET\_LO}$	EN/SET Low Time		0.3		75	$\mu s$
$T_{EN/SET\_HL\_MIN}$	Minimum EN/SET High Time			50		ns
$T_{EN/SET\_HL\_MAX}$	Maximum EN/SET High Time				75	$\mu s$
$T_{OFF}$	EN/SET Off Timeout				500	$\mu s$
$T_{LAT}$	EN/SET Latch Timeout				500	$\mu s$
$I_I$	Enable and EN/SET Input Leakage		-1.0		1.0	$\mu A$

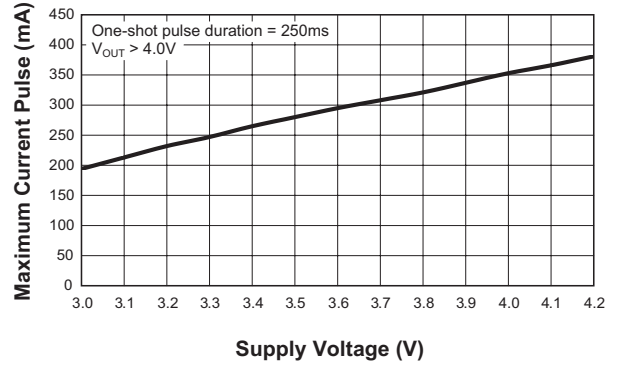
1. The AAT2806 is guaranteed to meet performance specifications over the  $-40^\circ C$  to  $+85^\circ C$  operating temperature range and is assured by design, characterization, and correlation with statistical process controls.
2. Specification applies only to the tri-mode charge pump.
3. Determined by the average of all active channels.
4. Current matching is defined as the deviation of any sink current from the average of all active channels.
5. Specification applies only to the charge pump doubler.

### Typical Characteristics—Flash Driver Charge Pump Section

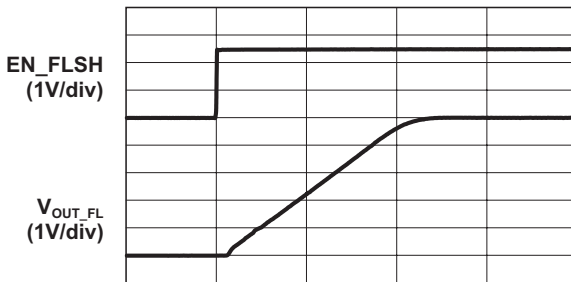
**Output Voltage vs. Output Current**  
( $V_{OUT\_FL} = 4.5V$ ;  $EN\_FL = V_{IN}$ ;  $EN/SET = GND$ )



**Maximum Current Pulse vs. Supply Voltage**  
( $V_{OUT\_FL} = 4.5V$ ;  $EN\_FL = V_{IN}$ ;  $EN/SET = GND$ )

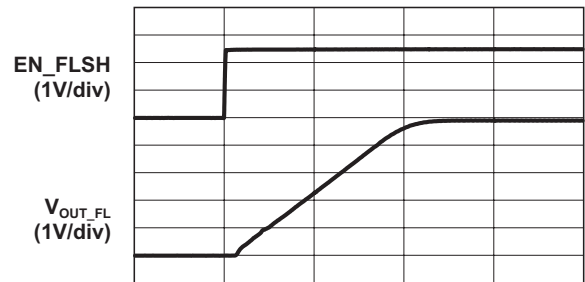


**Start-Up Time**  
(50mA Load)



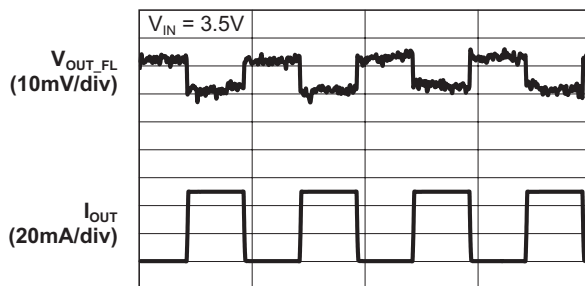
Time (100µs/div)

**Start-Up Time**  
(100mA Load)



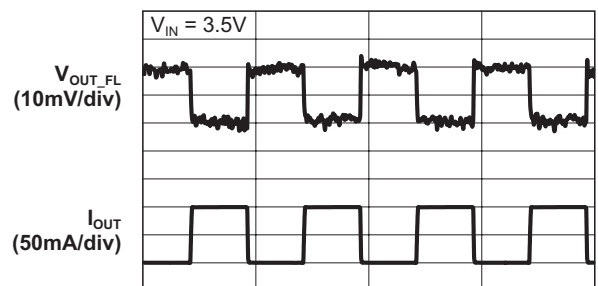
Time (100µs/div)

**Load Response vs. Time**  
(50mA Load)



Time (5ms/div)

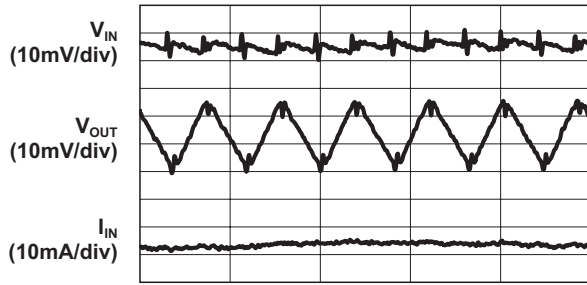
**Load Response vs. Time**  
(100mA Load)



Time (5ms/div)

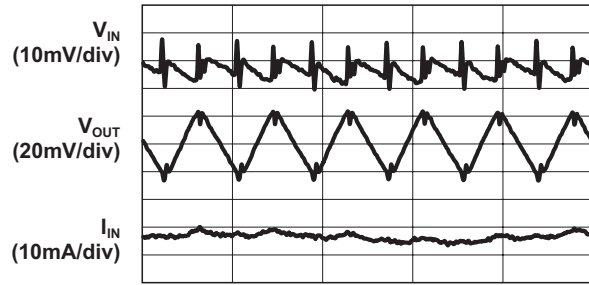
### Typical Characteristics–Flash Driver Charge Pump Section

**Output Ripple Voltage vs. Time**  
( $I_{OUT} = 50\text{mA}$  @  $V_{IN} = 3.5\text{V}$ )



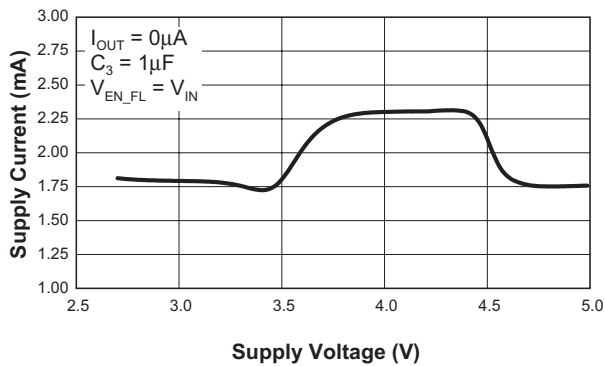
Time (500ns/div)

**Output Ripple Voltage vs. Time**  
( $I_{OUT} = 100\text{mA}$  @  $V_{IN} = 3.5\text{V}$ )

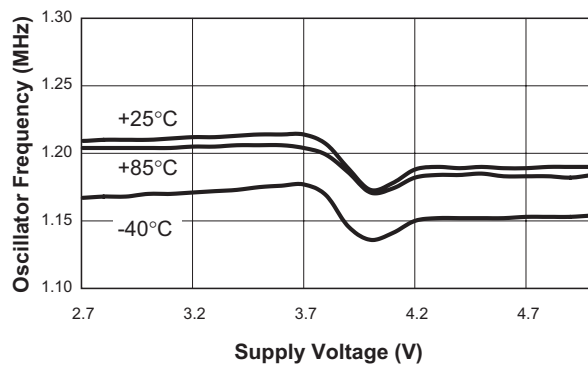


Time (500ns/div)

**Supply Current vs. Supply Voltage**

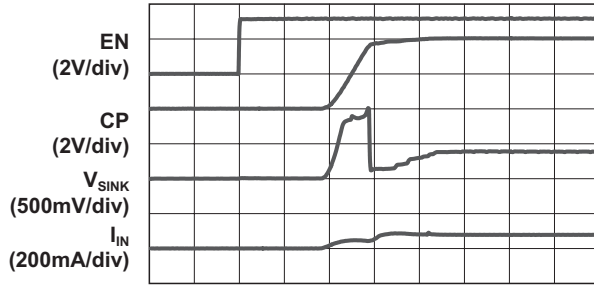


**Oscillator Frequency vs. Supply Voltage**



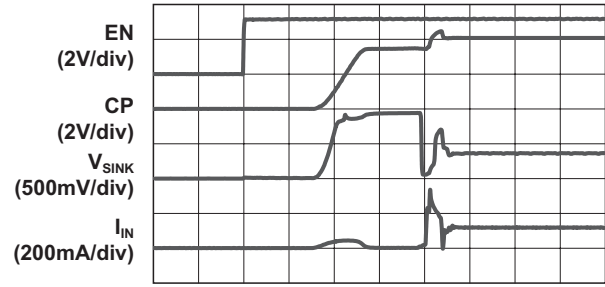
### Typical Characteristics—White LED Backlight Driver Section

Turn-On to 1X Mode  
( $V_{IN} = 4.2V$ ; 20mA Load)



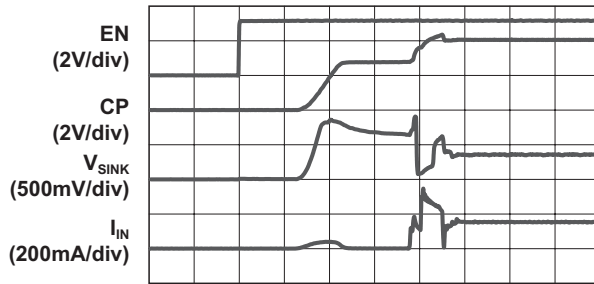
Time (100µs/div)

Turn-On to 1.5X Mode  
( $V_{IN} = 3.5V$ ; 20mA Load)



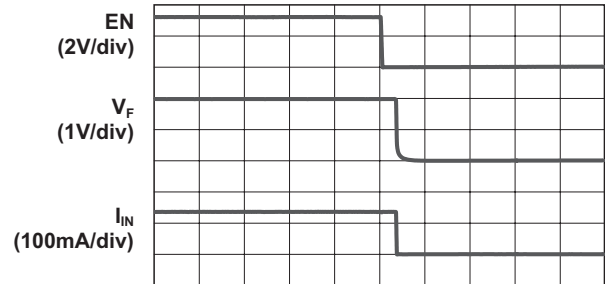
Time (100µs/div)

Turn-On to 2X Mode  
( $V_{IN} = 2.8V$ ; 20mA Load)



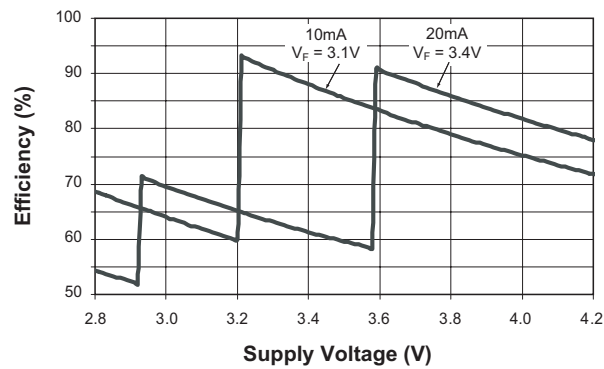
Time (100µs/div)

Turn-Off from 1.5X Mode  
( $V_{IN} = 3.5V$ ; 20mA Load)

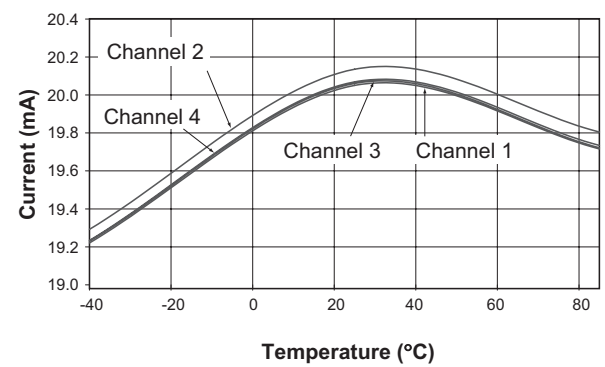


Time (500µs/div)

Efficiency vs. Supply Voltage

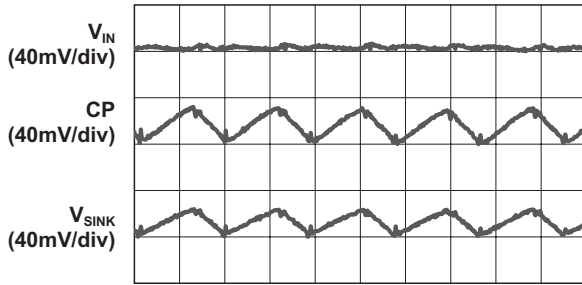


Current Matching vs. Temperature



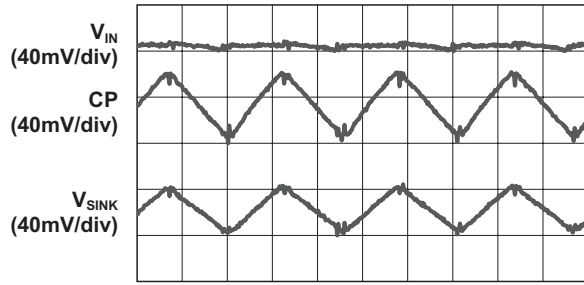
### Typical Characteristics—White LED Backlight Driver Section

**Load Characteristics**  
( $V_{IN} = 3.7V$ ; 1.5X Mode; 14mA Load)



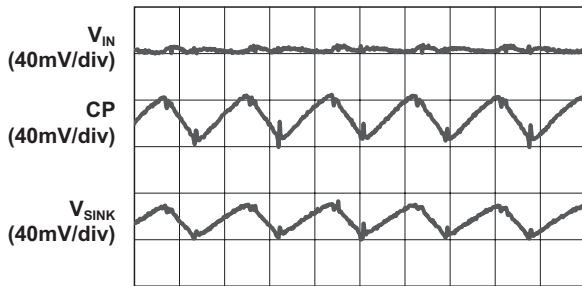
Time (500ns/div)

**Load Characteristics**  
( $V_{IN} = 2.7V$ ; 2X Mode; 14mA Load)



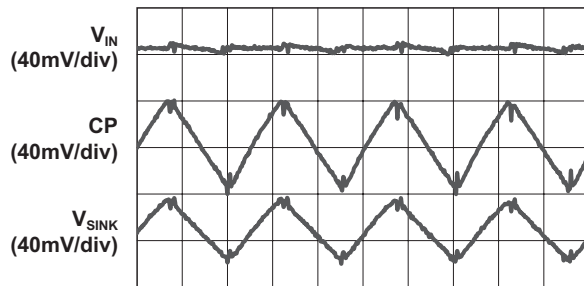
Time (500ns/div)

**Load Characteristics**  
( $V_{IN} = 3.9V$ ; 1.5X Mode; 20mA Load)



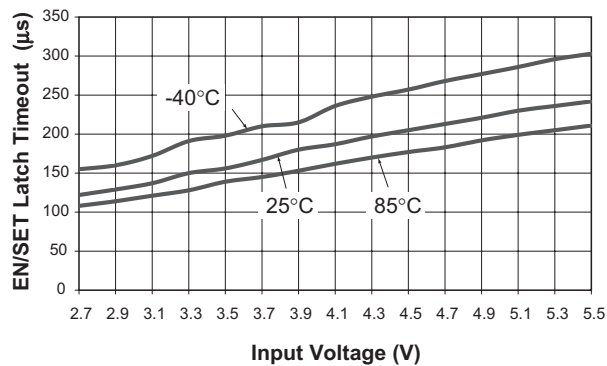
Time (500ns/div)

**Load Characteristics**  
( $V_{IN} = 2.9V$ ; 2X Mode; 20mA Load)

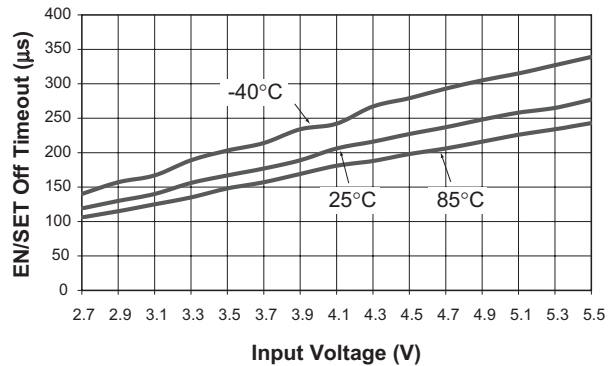


Time (500ns/div)

**EN/SET Latch Timeout vs. Input Voltage**



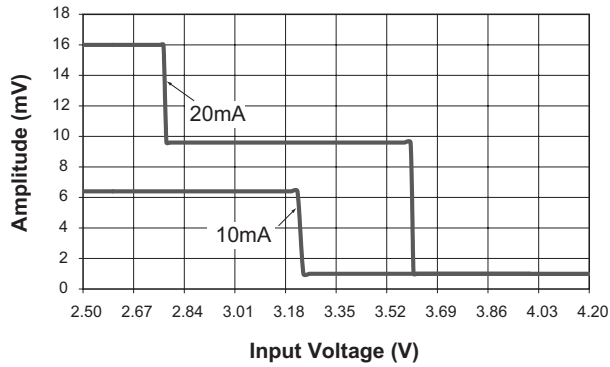
**EN/SET Off Timeout vs. Input Voltage**



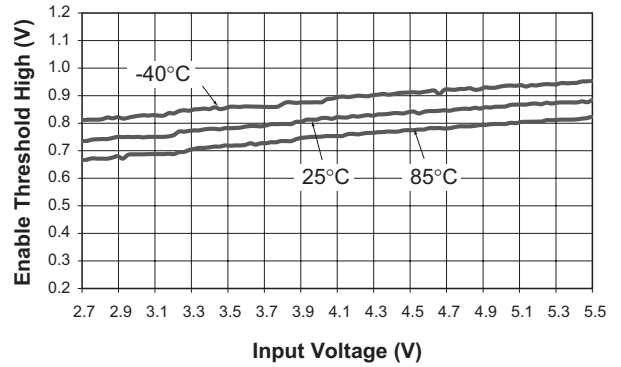


### Typical Characteristics—White LED Backlight Driver Section

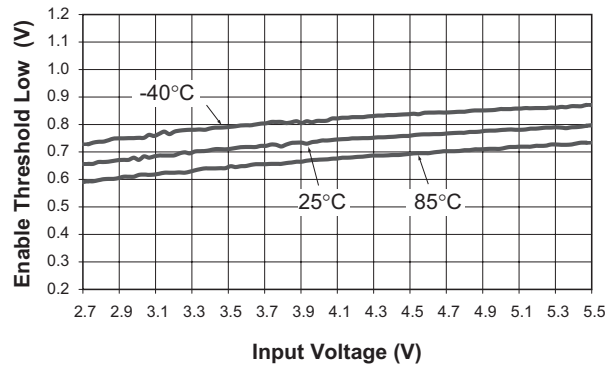
Input Ripple vs. Input Voltage



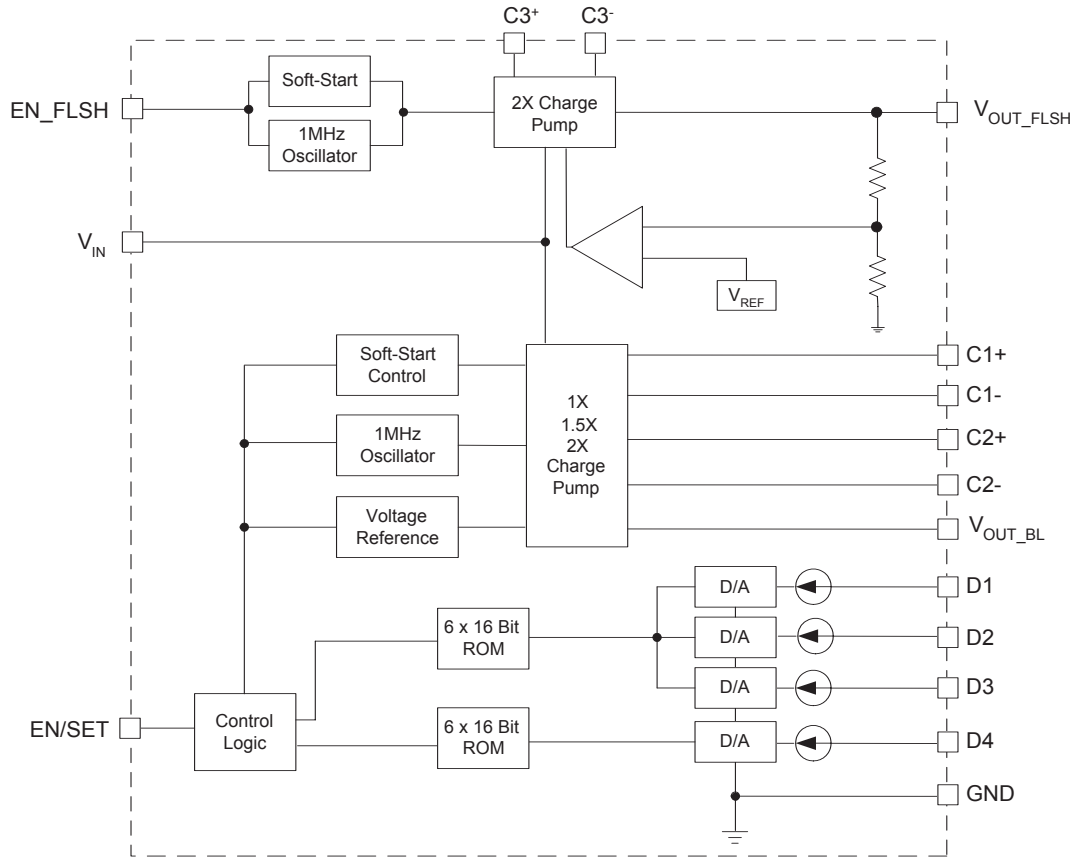
Enable Threshold High vs. Input Voltage



Enable Threshold Low vs. Input Voltage



### Functional Block Diagram



### Functional Description

The AAT2806 is a dual charge pump designed for flash and white LED applications. The backlight charge pump is a tri-mode load switch (1X) and high efficiency (1.5X or 2X) charge pump device. To maximize power conversion efficiency, an internal sensing circuit monitors the voltage required on each constant current sink input and sets the load switch and charge pump modes based on the input battery voltage and the current sink input voltage. As the battery voltage discharges over time, the white LED charge pump is enabled when any of the four current sink

inputs near dropout. The charge pump initially starts in 1.5X mode. If the charge pump output drops enough for any current source output to become close to dropout, the charge pump will automatically transition to 2X mode. The four constant current sink inputs D1 to D4 can drive four individual LEDs with a maximum current of 20mA per LED. The unused sink inputs must be connected to  $V_{OUT\_BL}$ ; otherwise, the part will operate only in 2X charge pump mode. The S<sup>2</sup>Cwire serial interface enables and sets the constant current sink magnitudes. S<sup>2</sup>Cwire addressing allows the LED main channels D1 to D3 to be controlled independently from the LED sub-channel D4.

The flash charge pump is a charge pump doubler with regulated output voltage. It is designed to deliver 120mA of continuous current and 250mA of pulsed current.

The AAT2806 requires six external components: three 1µF ceramic capacitors for the charge pump flying capacitors ( $C_1$ ,  $C_2$ , and  $C_3$ ), one 1µF ceramic input capacitor ( $C_{IN}$ ), one 0.33µF to 1µF ceramic capacitor for the backlight charge pump output capacitor ( $C_{OUT}$ ), and one 1µF ceramic capacitor for the flash charge pump output capacitor ( $C_{OUT}$ ).

### Constant Current Output Level Settings

The constant current level for the LED channels is set via the S<sup>2</sup>Cwire serial interface (see Table 1). Because the inputs D1 to D4 are true independent constant current sinks, the voltage observed on any single given input will be determined by the difference between  $V_{OUT}$  and the actual forward voltage ( $V_F$ ) of the LED being driven.

Since the constant current levels are programmable, no PWM (pulse width modulation) or additional control circuitry is needed to control LED brightness. This feature greatly reduces the burden on a microcontroller or system IC to manage LED or display brightness, allowing the user to "set it and forget it." With its high-speed serial interface (>1MHz data rate), the LED current drive can be changed successively to brighten or dim LEDs, in smooth transitions (e.g., to fade-out) or in abrupt steps, giving the user complete programmability and real-time control of LED brightness.

The AAT2806 offers an additional Low Current mode with reduced quiescent current (Data 13 to 16). This mode is especially useful for low-current applications where a continuous, low-current state is maintained. The reduction in quiescent current significantly reduces the impact due to maintaining a continuous backlighting state.

Data	$I_{OUT}$ (mA)	
	D1-D3	Sub-Group D4
1	20	20
2	14	14
3	10	10
4	7	7
5	20	0
6	14	0
7	10	0
8	7	0
9	0	20
10	0	14
11	0	10
12	0	7
13	0.05	0.05
14	0.5	0.5
15	1	1
16	2	2

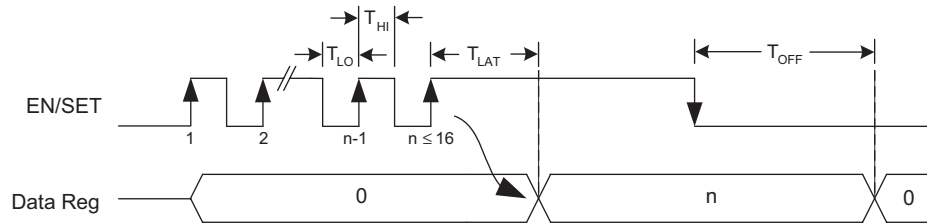
**Table 1: Constant Current Programming Levels.**

### S<sup>2</sup>Cwire Serial Interface

The current sink input magnitude on the backlight charge pump is controlled by AnalogicTech's S<sup>2</sup>Cwire serial digital input. The interface relies on the number of rising edges of the EN/SET pin to address and load the registers. S<sup>2</sup>Cwire latches data or address after the EN/SET pin has been held high for time  $T_{LAT}$ . The interface records rising edges of the EN/SET pin and decodes them into 16 different states, as indicated in Table 1. There are four brightness levels for the main or sub-display group with the possibility of individually turning ON or OFF each group. To further optimize power efficiency, the device also offers four low-current levels for dim LED operation (Data 13 to 16). During this low-current mode, the internal supply current reduces to only 50µA typical.

The counter can be clocked at speeds up to 1MHz, such that intermediate states are not visible. The first rising edge of EN/SET enables the IC and initially sets the output LED current to 20mA. Once the final clock cycle is input for the desired brightness level, the EN/SET pin is held high to maintain the device output current at the programmed level. The device is disabled 500µs ( $T_{OFF}$ ) after the EN/SET pin transitions to a logic low state.

### S<sup>2</sup>Cwire Serial Interface Timing Diagram



### Disabled Current Sinks

The backlight charge pump is equipped with an auto-disable feature to protect against an LED failure condition. Current sink inputs that are not used should be disabled. To disable and properly terminate unused current sink inputs, they must be tied to  $V_{OUT}$ . If left unconnected or terminated to ground, the part will be forced to operate in 2X charge pump mode.

Properly terminating unused current sink inputs is important to prevent the charge pump modes from activating prematurely. When properly terminated, only a small sense current flows for each disabled channel. The sense current for each disabled channel is less than 10 $\mu$ A.

### Applications Information

#### LED Selection

The AAT2806 is specifically intended for driving white LEDs. However, the device design will allow the AAT2806 to drive most types of LEDs with forward voltage specifications ranging from 2.0V to 4.3V. LED applications may include main display backlighting, camera photo-flash applications, color (RGB) LEDs, infrared (IR) diodes for remotes, and other loads benefiting from a controlled output current generated from a varying input voltage. Since the D1 to D4 input current sinks are matched with negligible voltage dependence, the LED brightness will be matched regardless of the specific LED forward voltage ( $V_F$ ) levels.

In some instances (e.g., in high-luminous-output applications such as photo-flash), it may be necessary to drive high- $V_F$  type LEDs. The low-dropout current-sinks in the AAT2806 make it capable of driving LEDs with forward voltages as high as 4.3V at full current from an input supply as low as 3.0V. Outputs can be paralleled to drive high-current LEDs without complication.

#### Device Switching Noise Performance

The AAT2806 operates at a fixed frequency of approximately 1MHz to control noise and limit harmonics that can interfere with the RF operation of cellular telephone handsets or other communication devices. Back-injected noise appearing on the input pin of the charge pump is 20mV peak-to-peak, typically ten times less than inductor-based DC/DC boost converter white LED backlight solutions. The AAT2806 soft-start feature prevents noise transient effects associated with inrush currents during start-up of the charge pump circuit.

#### Capacitor Selection

Careful selection of the six external capacitors  $C_{IN}$ ,  $C_1$ ,  $C_2$ ,  $C_3$ , and  $C_{OUT}$  (for backlight and flash) is important because they will affect turn-on time, output ripple, and transient performance. Optimum performance will be obtained when low equivalent series resistance (ESR) ceramic capacitors are used. In general, low ESR may be defined as less than 100m $\Omega$ . A value of 1 $\mu$ F for all six capacitors is a good starting point when choosing capacitors.

### Capacitor Characteristics

Ceramic composition capacitors are highly recommended over all other types of capacitors for use with the AAT2806. Ceramic capacitors offer many advantages over their tantalum and aluminum electrolytic counterparts. A ceramic capacitor typically has very low ESR, is lowest cost, has a smaller PCB footprint, and is non-polarized. Low ESR ceramic capacitors help maximize charge pump transient response. Since ceramic capacitors are non-polarized, they are not prone to incorrect connection damage.

### Equivalent Series Resistance

ESR is an important characteristic to consider when selecting a capacitor. ESR is a resistance internal to a capacitor that is caused by the leads, internal connections, size or area, material composition, and ambient temperature. Capacitor ESR is typically measured in milliohms for ceramic capacitors and can range to more than several ohms for tantalum or aluminum electrolytic capacitors.

### Ceramic Capacitor Materials

Ceramic capacitors less than 0.1 $\mu$ F are typically made from NPO or C0G materials. NPO and C0G materials generally have tight tolerance and are very stable over temperature. Larger capacitor values are usually composed of X7R, X5R, Z5U, or Y5V dielectric materials. Large ceramic capacitors (i.e., greater than 2.2 $\mu$ F) are often available in low-cost Y5V and Z5U dielectrics, but capacitors greater than 1 $\mu$ F are not typically required for AAT2806 applications.

Capacitor area is another contributor to ESR. Capacitors that are physically large will have a lower ESR when compared to an equivalent material smaller capacitor. These larger devices can improve circuit transient response when compared to an equal value capacitor in a smaller package size.

### Thermal Protection

The AAT2806 has a thermal protection circuit that will shut down the two charge pumps if the die temperature rises above the thermal limit.

### Charge Pump Power Efficiency

**Backlight Charge Pump:** The charge pump efficiency discussion in the following sections only accounts for the efficiency of the charge pump section itself. Due to the unique circuit architecture, it is very difficult to measure efficiency in terms of a percent value comparing input power over output power. Since the outputs are pure constant current sinks and typically drive individual loads, it is difficult to measure the output voltage for a given output (D1 to D4) to derive an overall output power measurement. For any given application, white LED forward voltage levels can differ, yet the output drive current will be maintained as a constant.

This makes quantifying output power a difficult task when taken in the context of comparing to other white LED driver circuit topologies. A better way to quantify total device efficiency is to observe the total input power to the device for a given LED current drive level. The best white LED driver for a given application should be based on trade-offs of size, external components count, reliability, operating range, and total energy usage...*not just "% efficiency."*

Efficiency of the AAT2806 may be quantified under very specific conditions and is dependent upon the input voltage versus the output voltage seen across the loads applied to outputs D1 through D4 for a given constant current setting. Depending on the combination of  $V_{IN}$  and voltages sensed at the current sinks, the device will operate in load switch mode. When any one of the voltages sensed at the current sinks nears dropout, the device will operate in 1.5X or 2X charge pump mode. Each of these modes will yield different efficiency values. Refer to the following two sections for explanations for each operational mode.

**Load Switch Mode Efficiency:** The load switch mode is operational at all times and functions alone to enhance device power conversion efficiency when  $V_{IN}$  is greater than the voltage across the load. When in load switch mode, the voltage conversion efficiency is defined as output power divided by input power:

$$\eta = \frac{P_{OUT}}{P_{IN}}$$

The expression to define the ideal efficiency ( $\eta$ ) can be rewritten as:

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{V_{OUT} \times I_{OUT}}{V_{IN} \times I_{OUT}} = \frac{V_{OUT}}{V_{IN}}$$

-or-

$$\eta(\%) = 100 \left( \frac{V_{OUT}}{V_{IN}} \right)$$

**Charge Pump Mode Efficiency:** Fractional charge pumps will boost the input supply voltage in the event where  $V_{IN}$  is less than the voltage required on the constant current source outputs. The efficiency ( $\eta$ ) can be simply defined as a linear voltage regulator with an effective output voltage that is equal to one and a half or two times the input voltage. Efficiency ( $\eta$ ) for an ideal 1.5X charge pump can typically be expressed as the output power divided by the input power:

$$\eta = \frac{P_{OUT}}{P_{IN}}$$

In addition, with an ideal 1.5X charge pump, the output current may be expressed as 2/3 of the input current. The expression to define the ideal efficiency ( $\eta$ ) can be rewritten as:

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{V_{OUT} \times I_{OUT}}{V_{IN} \times 1.5I_{OUT}} = \frac{V_{OUT}}{1.5V_{IN}}$$

-or-

$$\eta(\%) = 100 \left( \frac{V_{OUT}}{1.5V_{IN}} \right)$$

For a charge pump with an output of 5V and a nominal input of 3.5V, the theoretical efficiency is 95%. Due to internal switching losses and IC quiescent current consumption, the actual efficiency can be measured at 93%. These figures are in close agreement for output load conditions from 1mA to 100mA. Efficiency will decrease as load current drops below 0.05mA or when the level of  $V_{IN}$  approaches  $V_{OUT}$ .

**Flash Charge Pump:** The flash charge pump is a regulated output voltage doubling charge pump. The efficiency is defined as a linear voltage regulator with an effective output voltage that is equal to two times the input voltage. The expression to define the ideal efficiency can be written as:

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{V_{OUT} \times I_{OUT}}{V_{IN} \times 2.0I_{OUT}} = \frac{V_{OUT}}{2.0V_{IN}}$$

-or-

$$\eta(\%) = 100 \left( \frac{V_{OUT}}{2.0V_{IN}} \right)$$

For a charge pump with an output of 5V and a nominal input of 3V, the theoretical efficiency is 83.3%. Due to internal switching losses and IC quiescent current consumption, the actual efficiency can be measured at approximately 82%. Efficiency will decrease as the level of  $V_{IN}$  approaches that of the regulated  $V_{OUT}$ . Refer to the device typical characteristics curves for expected actual efficiency based on either input voltage or load current.

### Ordering Information

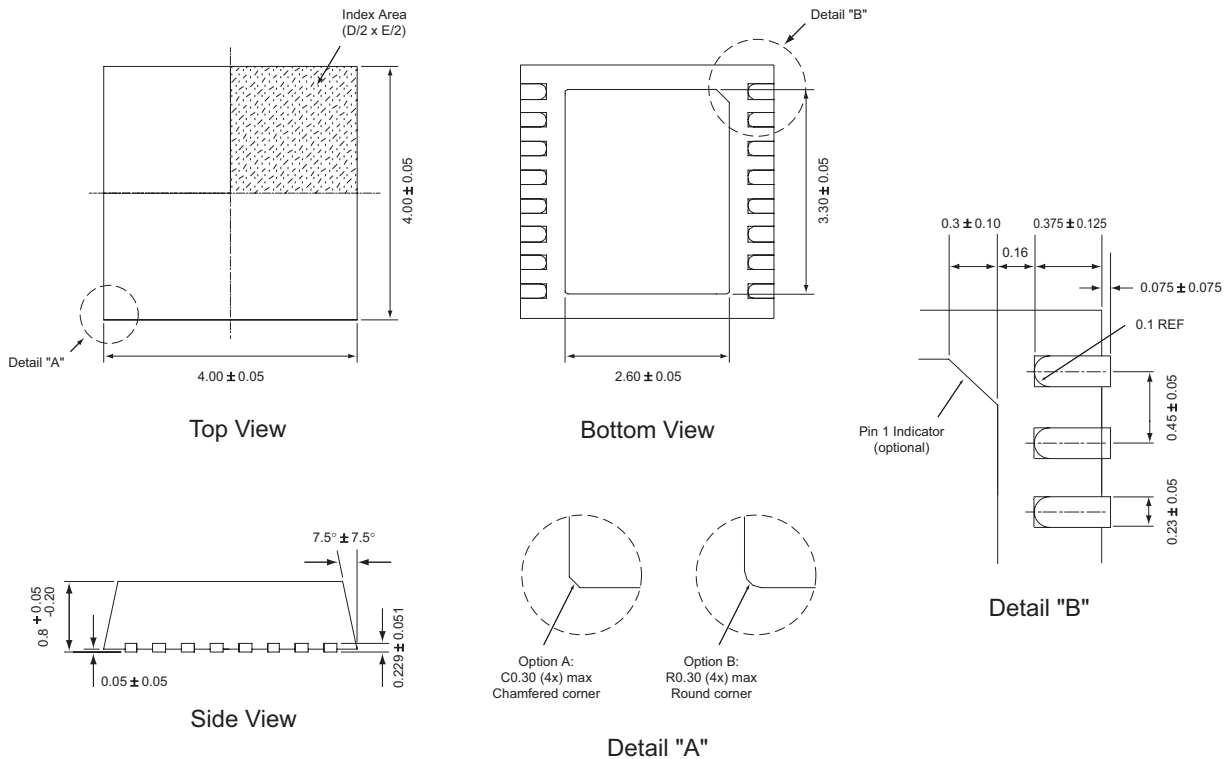
Package	Marking <sup>1</sup>	Part Number (Tape and Reel) <sup>2</sup>
TDFN44-16	NPXYY	<b>AAT2806IXN-4.5-T1</b>



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### Package Information

#### TDFN44-16



All dimensions in millimeters.

1. XYY = assembly and date code.  
2. Sample stock is generally held on part numbers listed in **BOLD**.

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**Advanced Analogic Technologies, Inc.**  
**830 E. Arques Avenue, Sunnyvale, CA 94085**  
**Phone (408) 737-4600**  
**Fax (408) 737-4611**

