# Design Idea DI-63 TinySwitch-II 4.8 W CV/CC Charger with Output Cable-Drop Compensation 

| Application | Device | Power Output | Input Voltage | Output Voltage | Topology |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Charger | TNY266P | 4.8 W | $85-265 \mathrm{VAC}$ | $6 \mathrm{~V}, 800 \mathrm{~mA} \pm 7 \%$ | Flyback |

## Design Highlights

- Universal input, no-load consumption < 300 mW
- Meets CISPR-22 Class B EMI without a Y capacitor
- Extremely simple circuit, requires only 32 components!
- Circuit has output cable voltage drop compensation
- Ultra-low Leakage current: $<5 \mu \mathrm{~A}$ at 265 VAC input


## Operation

Fusible resistor RF1 provides short-circuit fault protection and limits start-up inrush current. Inductors L1 and L2 and capacitors C 1 and C 2 form a low-cost pi $(\pi)$ filter that attenuates conducted EMI.

Transformer (T1) has two shield windings (1-3 and 1-open) which reduce the generation of EMI noise. Winding phasing and D7 orientation let no secondary winding current flow when the MOSFET in U1 is ON, so primary winding current stores energy in the core of T1. When the MOSFET in U1 turns OFF, the energy stored in T1 drives current out of the secondary
winding, forward biasing D7, charging C7 and developing/ maintaining the output voltage across C 7 . The $\mathrm{V}_{\mathrm{BE}}$ of Q 1 and the $\mathrm{V}_{\mathrm{Z}}$ of VR1 determine the CV set point. The voltage across R4, R5 and the U2-LED determine the CC set point.

Resistors R7, R10 and diode D6 compensate for output-cable voltage-drop. The CV portion of the output VI curve is flat, at the end of the cable, because a current sense resistor (R10) equal to the $D C$ resistance of the output cable is in the voltage feedback loop. Diode D6 implements temperature compensation for the cable drop.

The combination of TinySwitch-II frequency jitter, the output diode snubber (R6 and C5), the T1 shield windings and careful primary clamp circuit component selection enable compliance with CISPR-22, Class B conducted EMI limits, without a Y-1 Safety capacitor. Eliminating the Y capacitor gives this circuit very low $(<5 \mu \mathrm{~A}) \mathrm{AC}$ leakage current.

This circuit is suitable for portable electronics chargers.


Figure 1. TinySwitch-II Based Charger/Adapter Circuit Diagram.

## Key Design Points

- Secondary feedback bias current and output tolerances are minimized by using a low current part for VR1
- Primary clamp losses are minimized by keeping the voltage reflected across the transformer $\left(\mathrm{V}_{\mathrm{OR}}\right)$ low
- Picking wire sizes that fill each winding layer produce transformers with the lowest leakage inductance
- Putting the floating shield winding between the primary and secondary windings reduces EMI noise
- A high gain opto-coupler (CTR $=200-400)$ keeps the CC portion of the output curve more vertical
- R10 should equal the output cable resistance value


Figure 2. No-Load Input Power vs. Line Voltage.


Figure 3. 6.0 VDC, 800 mA CV/CC Curve.

| TRANSFORMER PARAMETERS |  |
| :---: | :--- |
| Core Material | EE16, TDK PC40, or equivalent <br> $A_{\mathrm{L}}$ of $127.5 \mathrm{nH} / \mathrm{T}^{2}$ |
| Bobbin | EE16, 10 pin |
| Winding Order <br> (pin numbers) | Core shield (1-3), tape <br> Primary (1-2), tape <br> Shield (1-floating), tape <br> Secondary (10-9), tape |
| Primary Inductance | $1.25 \mathrm{mH} \pm 10 \%$ |
| Primary Resonant Frequency | 500 kHz (minimum) |
| Leakage Inductance | 35 HH (maximum) |

Table 1. Transformer Construction Information.

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