

# TLV431

## 1.24V Cost effective shunt regulator

### Description

The TLV431 is a three terminal adjustable shunt regulator offering excellent temperature stability and output current handling capability up to 20mA. The output voltage may be set to any chosen voltage between 1.24 and 18 volts by selection of two external divider resistors.

The TLV431 can be used as a replacement for zener diodes in many applications requiring an improvement in zener performance.

The TLV431 is available in 2 grades with initial tolerances of 1% and 0.5% for the A and B grades respectively.

### Features

- Low Voltage Operation .....  $V_{REF} = 1.24V$
- Temperature range -40 to 125°C
- Reference Voltage Tolerance at 25°C
  - 0.5%.....TLV431B
  - 1%.....TLV431A
- Typical temperature drift
  - 4 mV (0°C to 70°C)
  - 6 mV (-40°C to 85°C)
  - 11mV (-40°C to 125°C)
- 80µA Minimum cathode current
- 0.25Ω Typical Output Impedance
- Adjustable Output Voltage .....  $V_{REF}$  to 18V

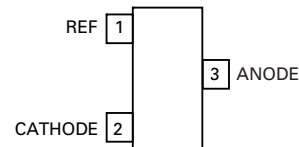
### Applications

- Opto-coupler linearisation
- Linear regulators
- Improved Zener
- Variable reference

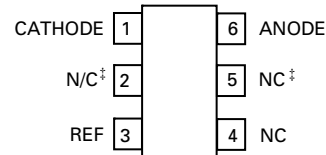
### Order Information

TOL	Order code	Pack	Part mark	Status	Reel Size (inches)	Tape width (mm)	Quantity per reel
1%	TLV431AE5TA	SOT23-5	V1A	Active	7	8	3000
	TLV431AFTA	SOT23	V1A	Active	7	8	3000
	TLV431AH6TA	SC70-6	V1A	Active	7	8	3000
0.5%	TLV431BE5TA	SOT23-5	V1B	Active	7	8	3000
	TLV431BFTA	SOT23	V1B	Active	7	8	3000
	TLV431BH6TA	SC70-6	V1B	Active	7	8	3000

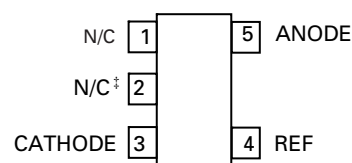
TLV431\_F (SOT23)



TLV431\_H6 (SC70-6)



TLV431\_E5 (SOT23-5)



‡ Connected internally to substrate; should be left floating or connected to anode

## Absolute Maximum Ratings

Cathode Voltage ( $V_{KA}$ ) .....	20V
Continuous Cathode Current ( $I_{KA}$ ) .....	-20 to 20mA
Reference input current range ( $I_{REF}$ ).....	-0.050 mA to 3mA
Operating Junction Temperature.....	-40 to 150°C
Storage Temperature .....	-55 to 150°C

Operation above the absolute maximum rating may cause device failure. Operation at the absolute maximum ratings, for extended periods, may reduce device reliability.

Unless otherwise stated voltages specified are relative to the ANODE pin.

## Package Thermal Data

Package	$\theta_{JA}$	$P_{DIS}$ $T_A = 25^\circ C, T_J = 150^\circ C$
SOT23	380°C/W	330 mW
SOT23-5	250°C/W	500 mW
SC70-6	380°C/W	330mW

## Recommended Operating Conditions

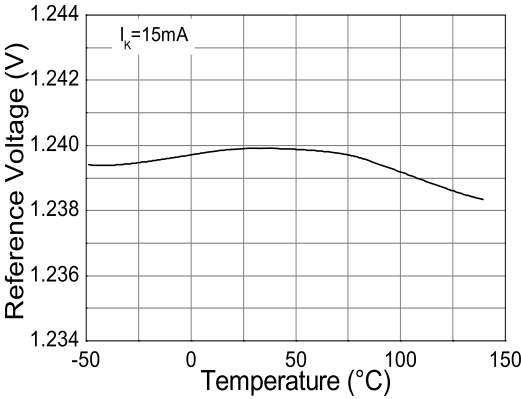
		Min	Max	Units
$V_{KA}$	Cathode Voltage	$V_{REF}$	18	V
$I_{KA}$	Cathode Current	0.1	15	mA
$T_A$	Operating Ambient temperature range	-40	125	°C

## Electrical Characteristics

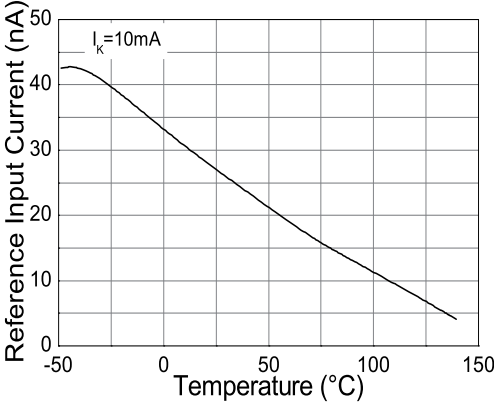
Electrical characteristics over recommended operating conditions,  $I_{KA} = 10\text{mA}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise stated.

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_{REF}$	Reference voltage	$V_{KA} = V_{REF}$ $T_A = 25^\circ\text{C}$	TLV431A	1.228	1.24	1.252	V
			TLV431B	1.234	1.24	1.246	
		$V_{KA} = V_{REF}$ $T_A = 0 \text{ to } 70^\circ\text{C}$	TLV431A	1.221		1.259	
			TLV431B	1.227		1.253	
		$V_{KA} = V_{REF}$ $T_A = -40 \text{ to } 85^\circ\text{C}$	TLV431A	1.215		1.265	
			TLV431B	1.224		1.259	
$V_{KA} = V_{REF}$ $T_A = -40 \text{ to } 125^\circ\text{C}$	TLV431A	1.209		1.271			
	TLV431B	1.221		1.265			
$V_{REF(\text{dev})}$	Deviation of reference voltage over full temperature range	$V_{KA} = V_{REF}$	$T_A = 0 \text{ to } 70^\circ\text{C}$		4	12	mV
			$T_A = -40 \text{ to } 85^\circ\text{C}$		6	20	
			$T_A = -40 \text{ to } 125^\circ\text{C}$		11	31	
$\frac{\Delta V_{REF}}{\Delta V_{KA}}$	Ratio of change in reference voltage to the change in cathode voltage	$V_{KA}$ from $V_{REF}$ to	6V		-1.5	-2.7	mV/V
			18V		-1.5	-2.7	
$I_{REF}$	Reference Input Current	$R_1 = 10\text{k}\Omega$ $R_2 = \text{OC}$		0.15	0.5	$\mu\text{A}$	
$I_{REF(\text{dev})}$	$I_{REF}$ deviation over full temperature range	$R_1 = 10\text{k}\Omega$ , $R_2 = \text{OC}$	$T_A = 0 \text{ to } 70^\circ\text{C}$		0.05	0.3	$\mu\text{A}$
			$T_A = -40 \text{ to } 85^\circ\text{C}$		0.1	0.4	
			$T_A = -40 \text{ to } 125^\circ\text{C}$		0.15	0.5	
$I_{K\text{MIN}}$	Minimum Cathode current for regulation	$V_{KA} = V_{REF}$	$T_A = 0 \text{ to } 70^\circ\text{C}$		55	80	$\mu\text{A}$
			$T_A = -40 \text{ to } 85^\circ\text{C}$		55	80	
			$T_A = -40 \text{ to } 125^\circ\text{C}$		55	100	
$I_{K(\text{OFF})}$	Off state current	$V_{KA} = 18\text{V}$ $V_{REF} = 0\text{V}$		0.001	0.1	$\mu\text{A}$	
$Z_{KA}$	Dynamic Output Impedance	$V_{KA} = V_{REF}$ $f = < 1\text{kHz}$ $I_K = 0.1 \text{ to } 15\text{mA}$		0.25	0.4	$\Omega$	

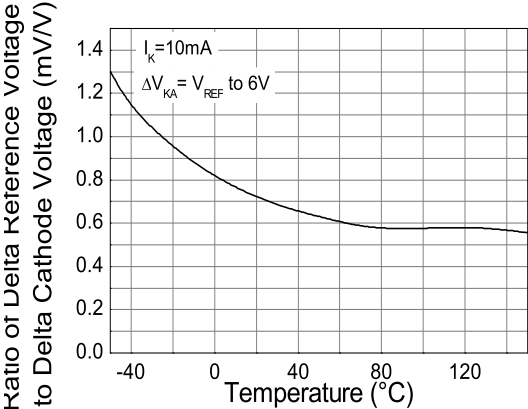
Typical Characteristics



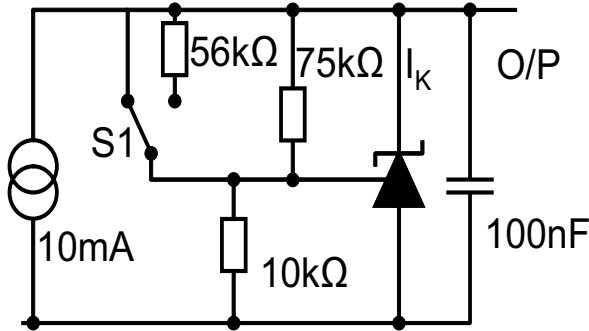
Reference Voltage vs Temperature



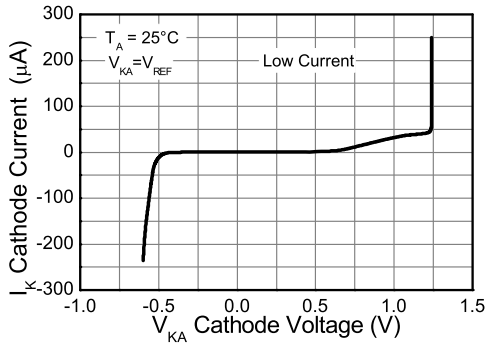
Reference Input Current vs Temperature



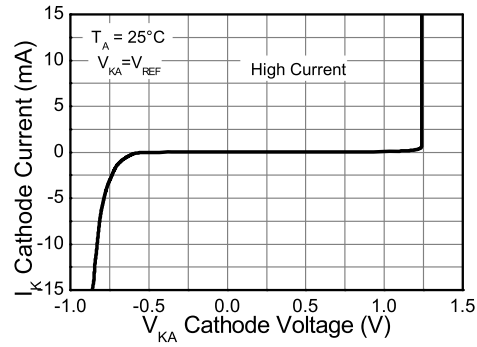
Ratio of Delta Reference Voltage to Delta Cathode Voltage vs Temperature



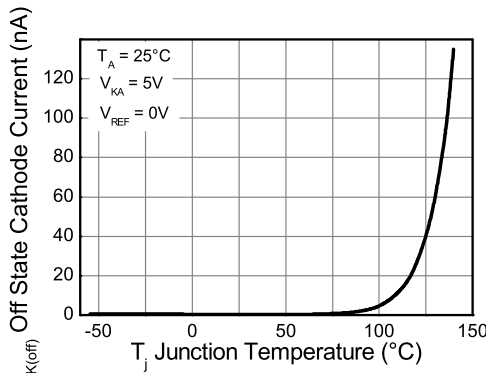
## Typical Characteristics



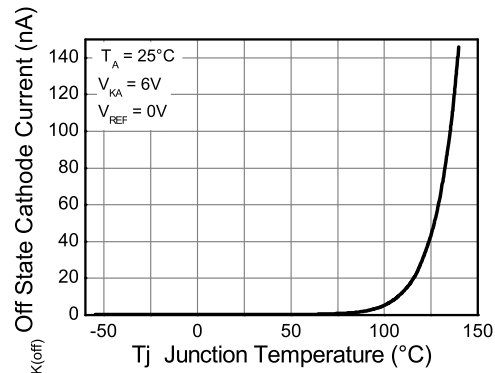
**Cathode Current vs Voltage**



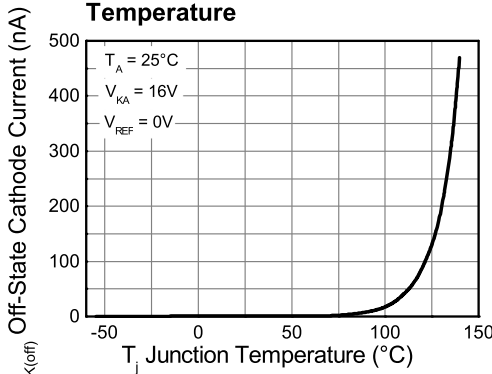
**Cathode Current vs Voltage**



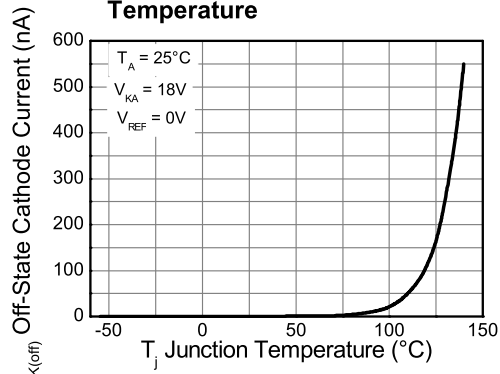
**Off-State Current vs Junction Temperature**



**Off-State Current vs Junction Temperature**

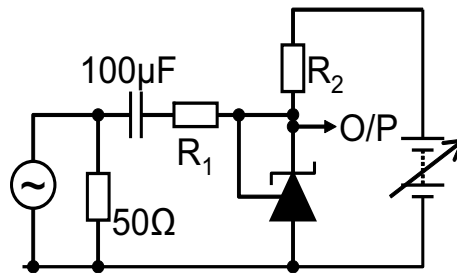
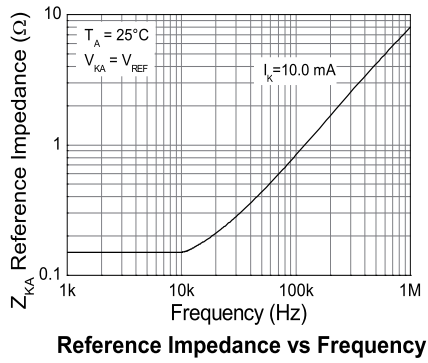
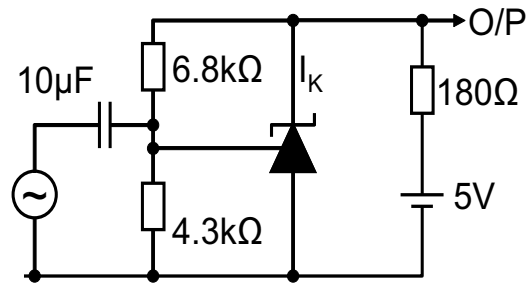
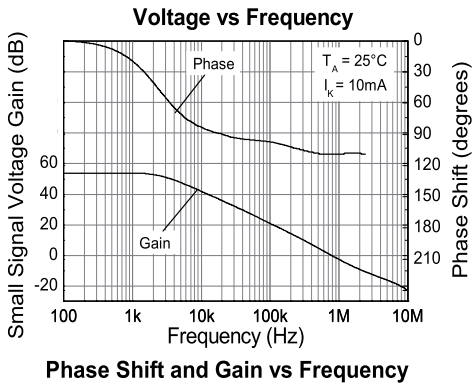
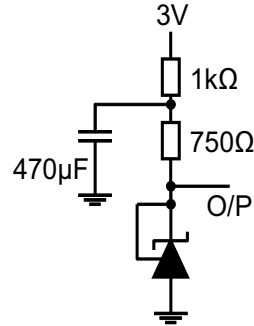
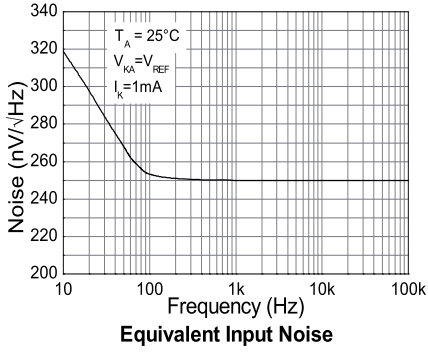


**Off-State Current vs Junction Temperature**



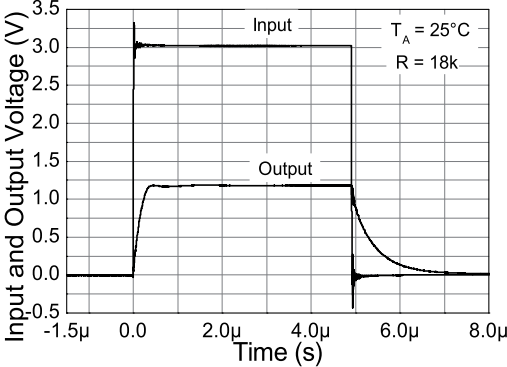
**Off-state Current vs Junction Temperature**

## Typical Characteristics

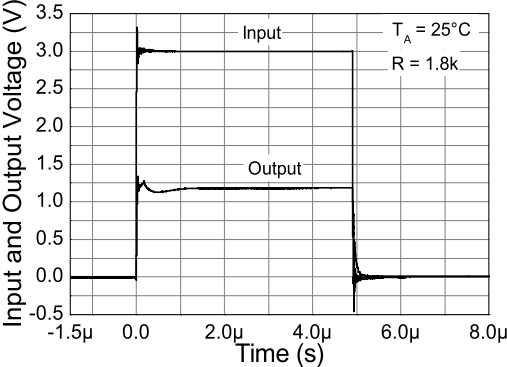
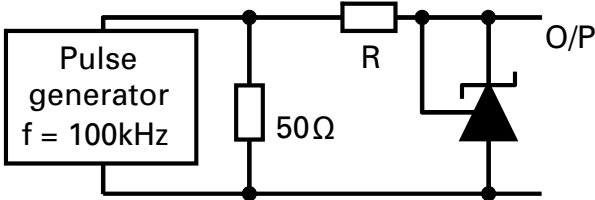


$I_K$	0.1mA	1-15mA
R1	1kΩ	100Ω
R2	1kΩ	100Ω

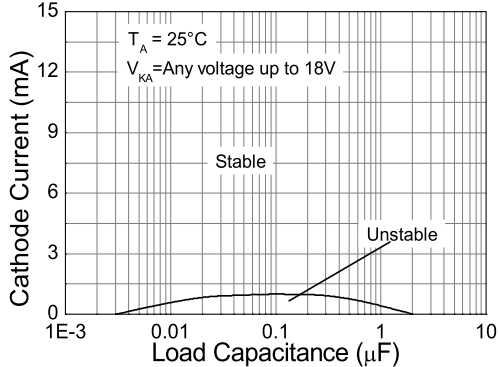
Typical Characteristics



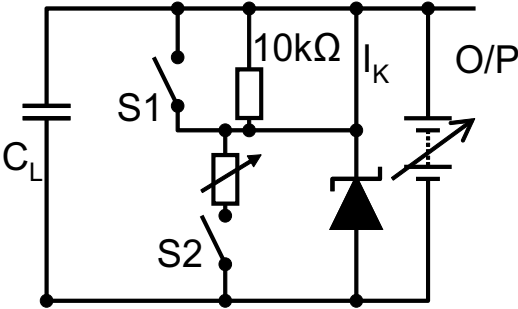
Pulse Response



Pulse Response

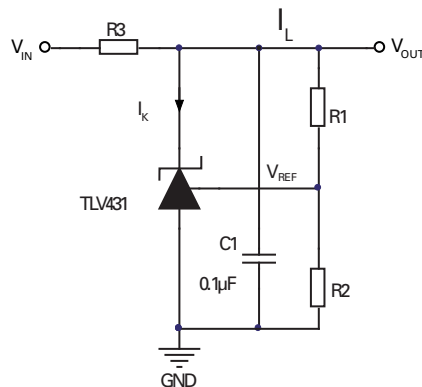


Stability Boundary Condition



## Application information

In a conventional shunt regulator application (*Figure 1*), an external series resistor ( $R_3$ ) is connected between the supply voltage and the TLV431.  $R_3$  determines the current that flows through the load ( $I_L$ ) and the TLV431 ( $I_K$ ). The TLV431 will adjust how much current it sinks or “shunts” to maintain a voltage equal to  $V_{REF}$  across its feedback pin. Since load current and supply voltage may vary,  $R_3$  should be small enough to supply at least the minimum acceptable  $I_{KMIN}$  to the TLV431 even when the supply voltage is at its minimum and the load current is at its maximum value. When the supply voltage is at its maximum and  $I_L$  is at its minimum,  $R_3$  should be large enough so that the current flowing through the TLV431 is less than 15 mA.  $R_3$  is determined by the supply voltage, ( $V_{IN}$ ), the load and operating current, ( $I_L$  and  $I_K$ ), and the TLV431’s reverse breakdown voltage,  $V_{KA}$ .



$$R_3 = \frac{V_S - V_{KA}}{I_L + I_K}$$

where

$$V_{KA} = V_{REF} \times \left( 1 + \frac{R_1}{R_2} \right)$$

and  $V_{KA} = V_{OUT}$

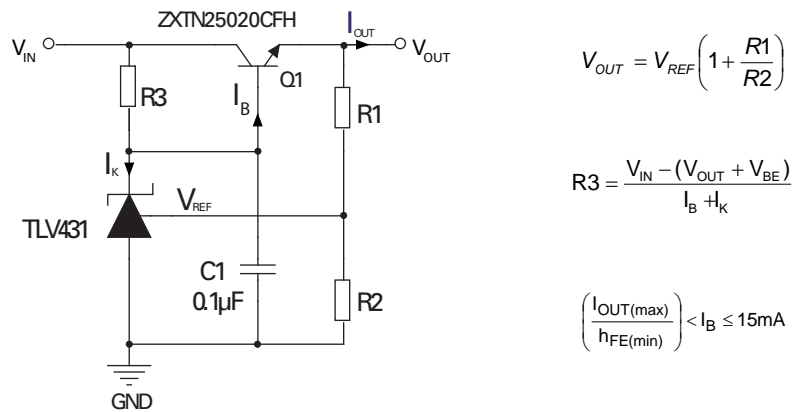
**Figure 1. Basic shunt regulator**

The values of  $R_1$  and  $R_2$  should be large enough so that the current flowing through them is much smaller than the current through  $R_3$  yet not too large that the voltage drop across them caused  $I_{REF}$  affects the reference accuracy.

The most frequent application of the TLV431 is in isolated low output voltage power supplies where the regulated output is galvanically isolated from the controller. As shown in figure 2 the TLV431 drives current,  $I_F$ , through the opto-coupler’s LED which in turn drives the isolated transistor which is connected to the controller on the primary side of the power supply. This completes the feedback path through the isolation barrier and ensures that a stable isolated supply is maintained. Assuming a forward drop of 1.4V across the opto-coupler diode allows output voltages as low as 2.7V to be regulated.

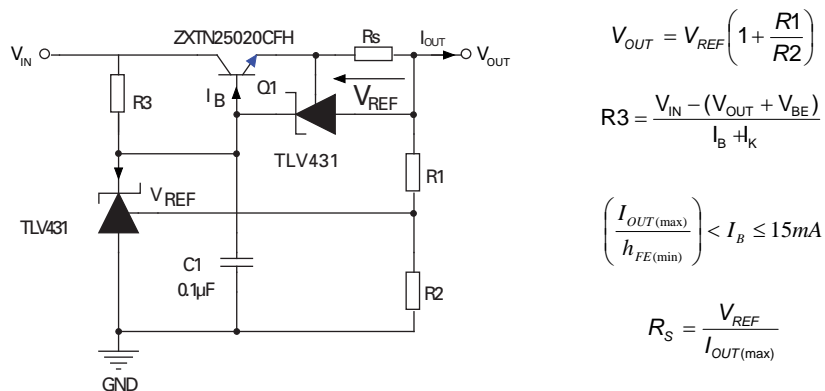






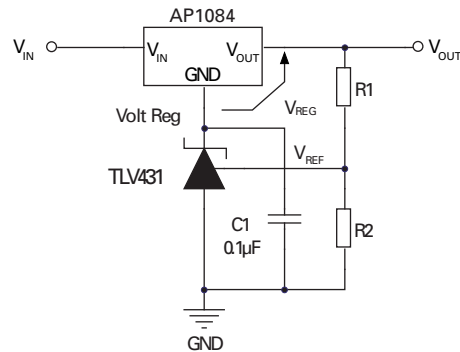
**Figure 4. Basic series regulator**

A very effective and simple series regulator can be implemented as shown in Figure 4 above. This may be preferable if the load requires more current than can be provided by the TLV431 alone and there is a need to conserve power when the load is not being powered. This circuit also uses one component less than the shunt circuit shown in Figure 2 above.



**Figure 5. Series regulator with current limit**

Figure 5 adds current limit to the series regulator in Figure 4 using a second TLV431. For currents below the limit, the circuit works normally supplying the required load current at the design voltage. However should attempts be made to exceed the design current set by the second TLV431, the device begins to shunt current away from the base of Q1. This begins to reduce the output voltage and thus ensuring that the output current is clamped at the design value. Subject only to Q1's ability to withstand the resulting power dissipation, the circuit can withstand either a brief or indefinite short circuit.



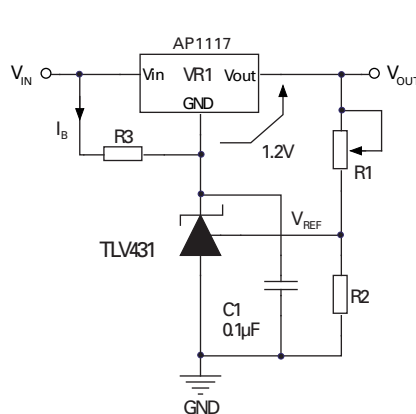
$$V_{OUT} = V_{REF} \left( 1 + \frac{R1}{R2} \right)$$

$$V_{OUT} \geq (V_{REG} + V_{REF})$$

(All features of the regulator such as short circuit protection, thermal shutdown, etc, are maintained.)

**Figure 6. Increasing output voltage of a fixed linear regulator**

One of the useful applications of the TLV431 is in using it to improve the accuracy and/or extend the range and flexibility of fixed voltage regulators. In the circuit in Figure 6 above, both the output voltage and its accuracy are entirely determined by the TLV431, R1 and R2. However the rest of the features of the regulator (up to 5A output current, output current limiting and thermal shutdown) are all still available.



$$V_{OUT} = V_{REF} \left( 1 + \frac{R1}{R2} \right)$$

$$V_{OUT} \geq (V_{REG} + V_{REF})$$

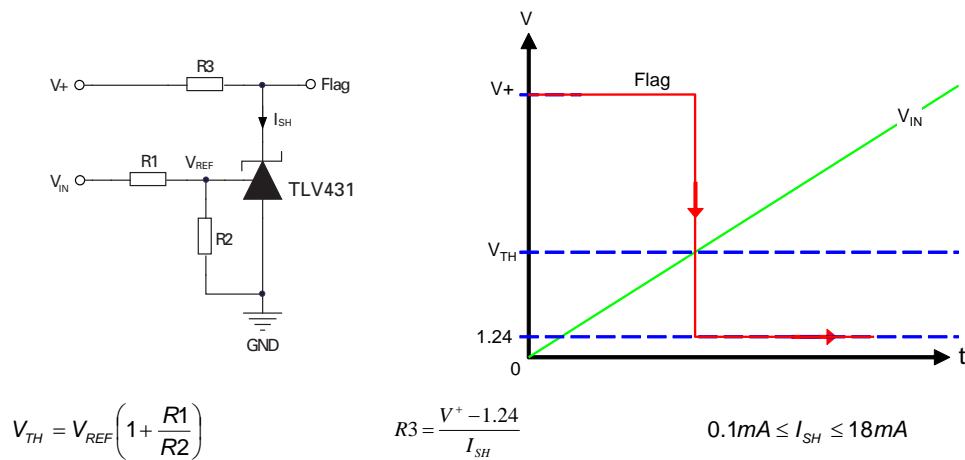
$$R3 = \frac{V_{IN} - (V_{OUT} - V_{REF})}{I_B}$$

$$0.1mA \leq I_B \leq 15mA$$

(All features of the regulator such as short circuit protection, thermal shutdown, etc, are maintained.)

**Figure 7. Adjustable linear voltage regulator**

Figure 7 is similar to Figure 6 with adjustability added. Note the addition of R3. This is only required for the AP1117 due to the fact that its ground or adjustment pin can only supply a few micro-Amps of current at best. R3 is therefore needed to provide sufficient bias current for the TLV431.

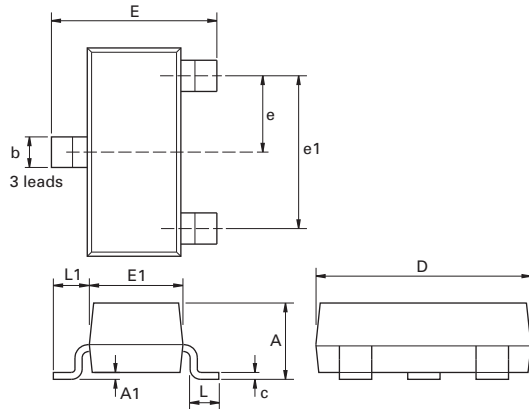


**Figure 8. Using the TLV431 as a level detector**

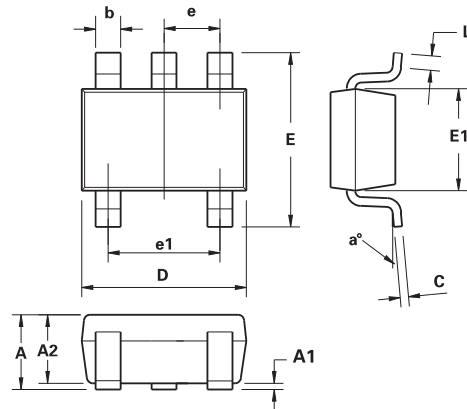
In its open loop state, the TLV431 is analogous to a line-powered comparator with its non-inverting input internally connected to a 1.24V reference voltage. This means the remaining inverting input can be used for comparator functions.

Figure 8 above shows the TLV431 being used as a level comparator. Its output (Flag) is normally high and goes low when the input reaches or exceeds the threshold ( $V_{TH}$ ) determined by R1 and R2.

## Package Outline - SOT23



## SOT23-5



### Dimension Table SOT23

Dim.	Millimeters		Inches		Dim.	Millimeters		Inches	
	Min.	Max.	Min.	Max.		Min.	Max.	Min.	Max.
A	-	1.12	-	0.044	e1	1.90 NOM		0.075 NOM	
A1	0.01	0.10	0.0004	0.004	E	2.10	2.64	0.083	0.104
b	0.30	0.50	0.012	0.020	E1	1.20	1.40	0.047	0.055
c	0.085	0.20	0.003	0.008	L	0.25	0.60	0.0098	0.0236
D	2.80	3.04	0.110	0.120	L1	0.45	0.62	0.018	0.024
e	0.95 NOM		0.037 NOM		-	-	-	-	-

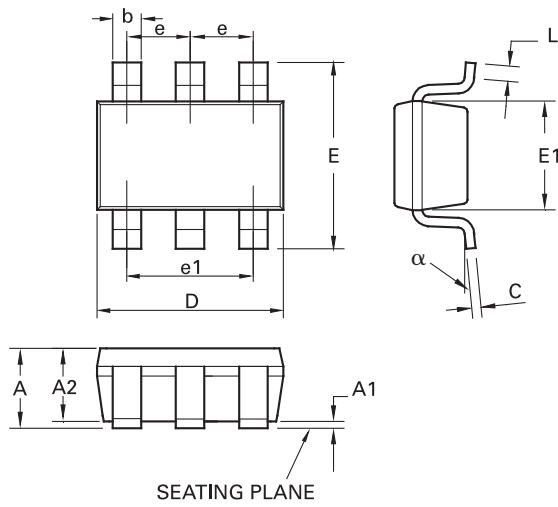
**Note:** Controlling dimensions are in millimeters. Approximate dimensions are provided in inches

### Dimension table - SOT23-5

Dim.	Millimeters		Inches		Dim.	Millimeters		Inches	
	Min.	Max.	Min.	Max.		Min.	Max.	Min.	Max.
A	0.9	1.45	0.0354	0.0570	E	2.20	3.20	0.0866	0.1181
A1	0.00	0.15	0.00	0.0059	E1	1.30	1.80	0.0511	0.0708
A2	0.90	1.3	0.0354	0.0511	e	0.95 REF		0.0374	
b	0.20	0.50	0.0078	0.0196	e1	1.90 REF		0.0748	
C	0.09	0.26	0.0035	0.0102	L	0.10	0.60	0.0039	0.0236
D	2.70	3.10	0.1062	0.1220	a°	0	30	0	30

**Note:** Controlling dimensions are in millimeters. Approximate dimensions are provided in inches

## Package outline - SC70-6



Dim.	Millimeters		Inches		Dim.	Millimeters		Inches	
	Min.	Max.	Min.	Max.		Min.	Max.	Min.	Max.
A	0.80	1.10	0.0315	0.0433	E	2.10 BSC		0.0826 BSC	
A1	0	0.10	0	0.0039	E1	1.25 BSC		0.0492 BSC	
A2	0.80	1.00	0.0315	0.0394	e	0.65 BSC		0.0255 BSC	
b	0.15	0.30	0.006	0.0118	e1	1.30 BSC		0.0511 BSC	
C	0.08	0.25	0.0031	0.0098	L	0.26	0.46	0.0102	0.0181
D	2.00 BSC		0.0787 BSC		a°	0	8	0	8

**Note:** Controlling dimensions are in millimeters. Approximate dimensions are provided in inches

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"Not recommended for new designs"	Device is still in production to support existing designs and production
"Obsolete"	Production has been discontinued

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