

**Radiation Hardened, Dual, High Speed  
Low Power, Video Closed Loop Buffer**

The HS-1212RH is a dual closed loop buffer featuring user programmable gain and high speed performance. Manufactured on Intersil's proprietary complementary bipolar UHF-1 (DI bonded wafer) process, this device offers wide -3dB bandwidth of 340MHz, very fast slew rate, excellent gain flatness and high output current. These devices are QML approved and are processed and screened in full compliance with MIL-PRF-38535.

A unique feature of the pinout allows the user to select a voltage gain of +1, -1, or +2, without the use of any external components. Gain selection is accomplished via connections to the inputs, as described in the "Application Information" section. The result is a more flexible product, fewer part types in inventory, and more efficient use of board space.

Compatibility with existing op amp pinouts provides flexibility to upgrade low gain amplifiers, while decreasing component count. Unlike most buffers, the standard pinout provides an upgrade path should a higher closed loop gain be needed at a future date.

**Specifications for Rad Hard QML devices are controlled by the Defense Supply Center in Columbus (DSCC). The SMD numbers listed here must be used when ordering.**

**Detailed Electrical Specifications for these devices are contained in SMD 5962-96831. A "hot-link" is provided on our homepage for downloading.**  
[www.intersil.com/spacedefense/space.asp](http://www.intersil.com/spacedefense/space.asp)

**Ordering Information**

ORDERING NUMBER	INTERNAL MKT. NUMBER	TEMP. RANGE (°C)
5962F9683101VPA	HS7-1212RH-Q	-55 to 125
5962F9683101VPC	HS7B-1212RH-Q	-55 to 125

**Features**

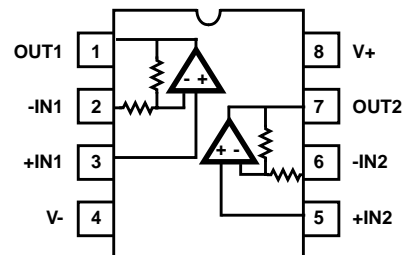
- Electrically Screened to SMD # 5962-96831
- QML Qualified per MIL-PRF-38535 Requirements
- MIL-PRF-38535 Class V Compliant
- User Programmable For Closed-Loop Gains of +1, -1 or +2 Without Use of External Resistors
- Standard Operational Amplifier Pinout
- Low Supply Current . . . . . 5.9mA/Op Amp (Typ)
- Excellent Gain Accuracy . . . . . 0.99V/V (Typ)
- Wide -3dB Bandwidth. . . . . 340MHz (Typ)
- Fast Slew Rate . . . . . 1155V/μs (Typ)
- High Input Impedance . . . . . 1MΩ (Typ)
- Excellent Gain Flatness (to 50MHz). . . . . ±0.02dB (Typ)
- Fast Overdrive Recovery . . . . . <10ns (Typ)
- Total Gamma Dose. . . . . 300kRAD(Si)
- Latch Up. . . . . None (DI Technology)

**Applications**

- Flash A/D Driver
- Video Switching and Routing
- Pulse and Video Amplifiers
- Wideband Amplifiers
- RF/IF Signal Processing
- Imaging Systems

**Pinout**

**HS-1212RH (CERDIP) GDIP1-T8  
OR  
HS-1212RH (SBDIP) CDIP2-T8  
TOP VIEW**



**Application Information**

**HS-1212RH Advantages**

The HS-1212RH features a novel design which allows the user to select from three closed loop gains, without any external components. The result is a more flexible product, fewer part types in inventory, and more efficient use of board space. Implementing a dual, gain of 2, cable driver with this IC eliminates the four gain setting resistors, which frees up board space for termination resistors.

Like most newer high performance amplifiers, the HS-1212RH is a current feedback amplifier (CFA). CFAs offer high bandwidth and slew rate at low supply currents, but can be difficult to use because of their sensitivity to feedback capacitance and parasitics on the inverting input (summing node). The HS-1212RH eliminates these concerns by bringing the gain setting resistors on-chip. This yields the optimum placement and value of the feedback resistor, while minimizing feedback and summing node parasitics. Because there is no access to the summing node, the PCB parasitics do not impact performance at gains of +2 or -1 (see “Unity Gain Considerations” for discussion of parasitic impact on unity gain performance).

The HS-1212RH's closed loop gain implementation provides better gain accuracy, lower offset and output impedance, and better distortion compared with open loop buffers.

**Closed Loop Gain Selection**

This “buffer” operates in closed loop gains of -1, +1, or +2, with gain selection accomplished via connections to the inputs. Applying the input signal to +IN and floating -IN selects a gain of +1 (see next section for layout caveats), while grounding -IN selects a gain of +2. A gain of -1 is obtained by applying the input signal to -IN with +IN grounded through a 50Ω resistor.

The table below summarizes these connections:

GAIN (ACL)	CONNECTIONS	
	+INPUT	-INPUT
-1	50Ω to GND	Input
+1	Input	NC (Floating)
+2	Input	GND

**Unity Gain Considerations**

Unity gain selection is accomplished by floating the -Input of the HS-1212RH. Anything that tends to short the -Input to GND, such as stray capacitance at high frequencies, will cause the amplifier gain to increase toward a gain of +2. The result is excessive high frequency peaking, and possible instability. Even the minimal amount of capacitance associated with attaching the -Input lead to the PCB results in approximately 6dB of gain peaking. At a minimum this requires due care to ensure the minimum capacitance at the -Input connection.

Table 1 lists five alternate methods for configuring the HS-1212RH as a unity gain buffer, and the corresponding performance. The implementations vary in complexity and involve performance trade-offs. The easiest approach to implement is simply shorting the two input pins together, and applying the input signal to this common node. The amplifier bandwidth decreases from 430MHz to 280MHz, but excellent gain flatness is the benefit. A drawback to this approach is that the amplifier input noise voltage and input offset voltage terms see a gain of +2, resulting in higher noise and output offset voltages. Alternately, a 100pF capacitor between the inputs shorts them only at high frequencies, which prevents the increased output offset voltage but delivers less gain flatness.

Another straightforward approach is to add a 620Ω resistor in series with the amplifier's positive input. This resistor and the HS-1212RH input capacitance form a low pass filter which rolls off the signal bandwidth before gain peaking occurs. This configuration was employed to obtain the data sheet AC and transient parameters for a gain of +1.

**Pulse Overshoot**

The HS-1212RH utilizes a quasi-complementary output stage to achieve high output current while minimizing quiescent supply current. In this approach, a composite device replaces the traditional PNP pulldown transistor. The composite device switches modes after crossing 0V, resulting in added distortion for signals swinging below ground, and an increased overshoot on the negative portion of the output waveform (see Figure 6, Figure 9, and Figure 12). This overshoot isn't present for small bipolar signals (see Figure 4, Figure 7, and Figure 10) or large positive signals (see Figure 5, Figure 8 and Figure 11).

**PC Board Layout**

This amplifier's frequency response depends greatly on the care taken in designing the PC board (PCB). **The use of low inductance components such as chip resistors and chip capacitors is strongly recommended, while a solid ground plane is a must!**

Attention should be given to decoupling the power supplies. A large value (10μF) tantalum in parallel with a small value (0.1μF) chip capacitor works well in most cases.

**TABLE 1. UNITY GAIN PERFORMANCE FOR VARIOUS IMPLEMENTATIONS**

APPROACH	PEAKING (dB)	BW (MHz)	±0.1dB GAIN FLATNESS (MHz)
Remove -IN Pin	4.5	430	21
+R <sub>S</sub> = 620Ω	0	220	27
+R <sub>S</sub> = 620Ω and Remove -IN Pin	0.5	215	15
Short +IN to -IN (e.g., Pins 2 and 3)	0.6	280	70
100pF Capacitor Between +IN and -IN	0.7	290	40

Terminated microstrip signal lines are recommended at the input and output of the device. Capacitance directly on the output must be minimized, or isolated as discussed in the next section.

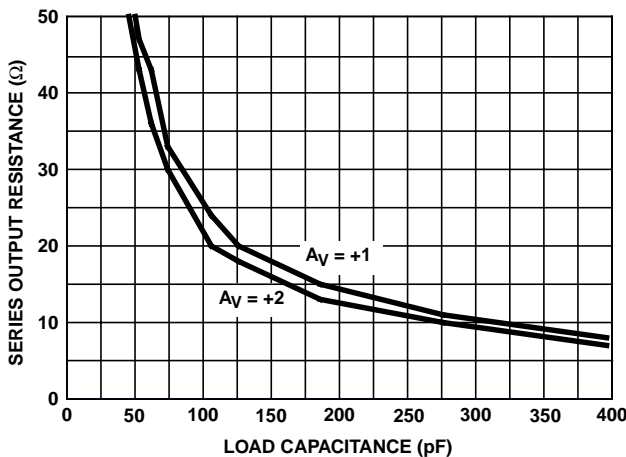
An example of a good high frequency layout is the Evaluation Board shown in Figure 3.

### Driving Capacitive Loads

Capacitive loads, such as an A/D input, or an improperly terminated transmission line will degrade the amplifier's phase margin resulting in frequency response peaking and possible oscillations. In most cases, the oscillation can be avoided by placing a resistor (R<sub>S</sub>) in series with the output prior to the capacitance.

Figure 1 details starting points for the selection of this resistor. The points on the curve indicate the R<sub>S</sub> and C<sub>L</sub> combinations for the optimum bandwidth, stability, and settling time, but experimental fine tuning is recommended. Picking a point above or to the right of the curve yields an overdamped response, while points below or left of the curve indicate areas of underdamped performance.

R<sub>S</sub> and C<sub>L</sub> form a low pass network at the output, thus limiting system bandwidth well below the amplifier bandwidth of 350MHz. By decreasing R<sub>S</sub> as C<sub>L</sub> increases (as illustrated in the curves), the maximum bandwidth is obtained without sacrificing stability. In spite of this, bandwidth decreases as the load capacitance increases.



**FIGURE 1. RECOMMENDED SERIES RESISTOR vs LOAD CAPACITANCE**

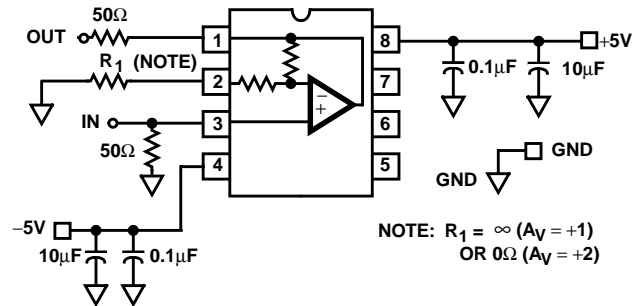
### Evaluation Board

The performance of the HS-1212RH may be evaluated using the HA5023 Evaluation Board, slightly modified as follows:

1. Remove the two feedback resistors, and leave the connections open.
2. a. For A<sub>V</sub> = +1 evaluation, remove the gain setting resistors (R<sub>1</sub>), and leave pins 2 and 6 floating.  
 b. For A<sub>V</sub> = +2, replace the gain setting resistors (R<sub>1</sub>) with 0Ω resistors to GND.

The modified schematic for amplifier 1, and the board layout are shown in Figures 2 and 3.

To order evaluation boards (part number HA5023EVAL), please contact your local sales office.



**FIGURE 2. MODIFIED EVALUATION BOARD SCHEMATIC**

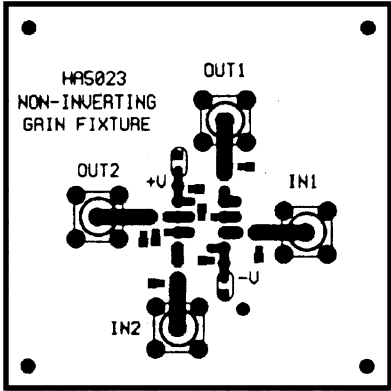


FIGURE 3A. TOP LAYOUT

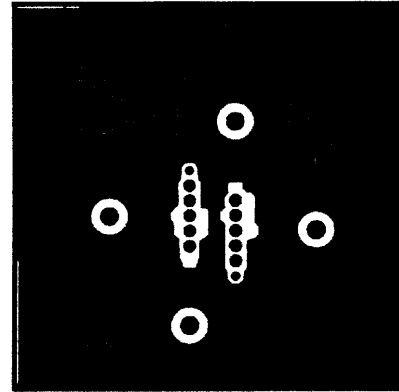


FIGURE 3B. BOTTOM LAYOUT

FIGURE 3. EVALUATION BOARD LAYOUT

**Typical Performance Curves**  $V_{SUPPLY} = \pm 5V$ ,  $T_A = 25^\circ C$ ,  $R_L = 100\Omega$ , Unless Otherwise Specified

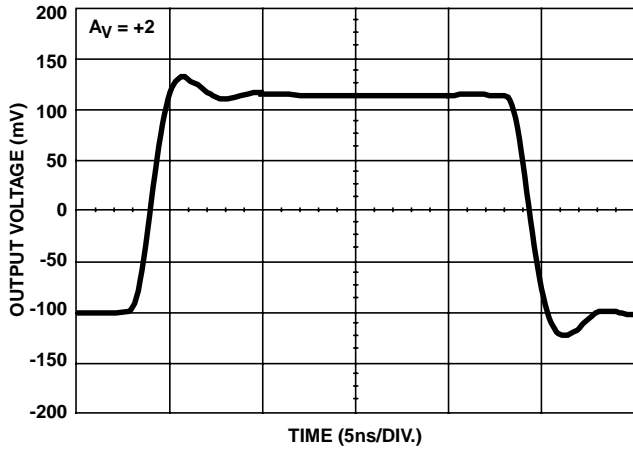


FIGURE 4. SMALL SIGNAL PULSE RESPONSE

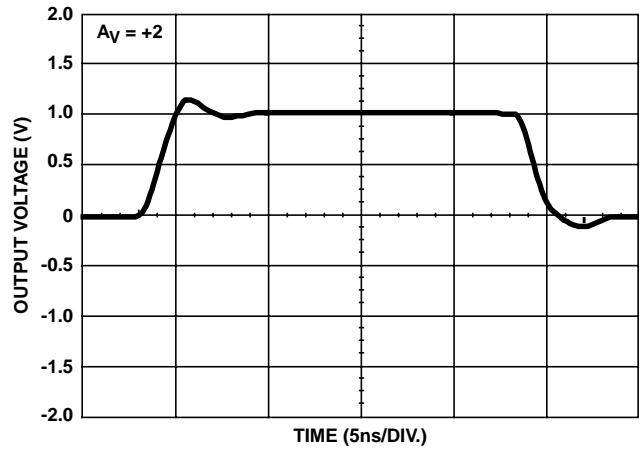


FIGURE 5. LARGE SIGNAL POSITIVE PULSE RESPONSE

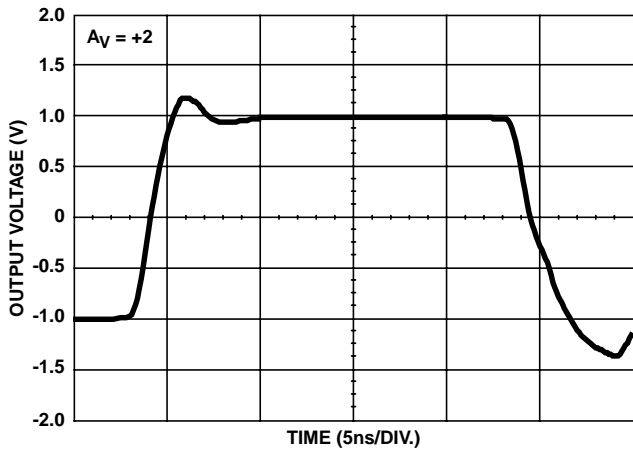


FIGURE 6. LARGE SIGNAL BIPOLAR PULSE RESPONSE

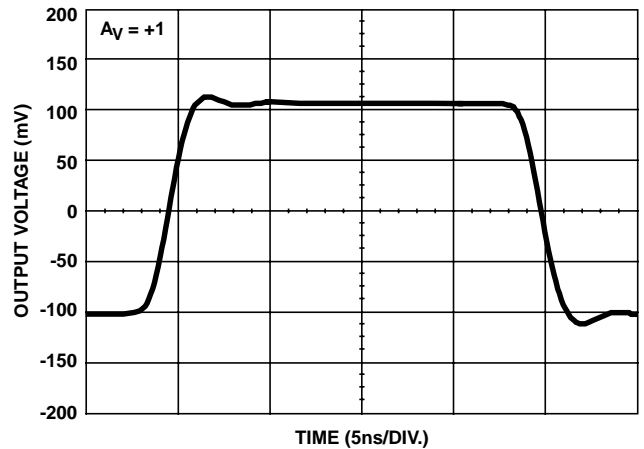


FIGURE 7. SMALL SIGNAL PULSE RESPONSE

**Typical Performance Curves**  $V_{SUPPLY} = \pm 5V$ ,  $T_A = 25^\circ C$ ,  $R_L = 100\Omega$ , Unless Otherwise Specified (Continued)

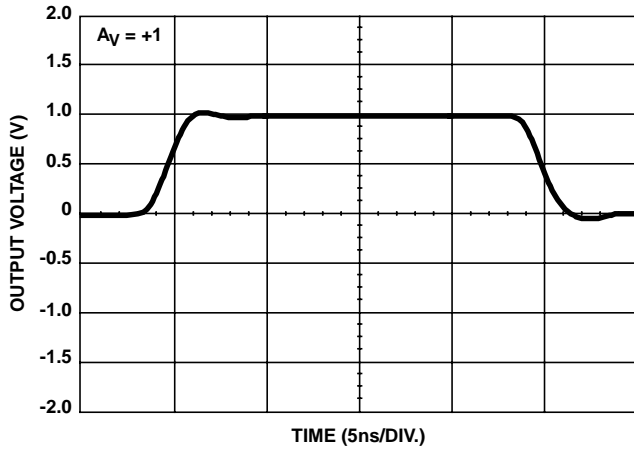


FIGURE 8. LARGE SIGNAL POSITIVE PULSE RESPONSE

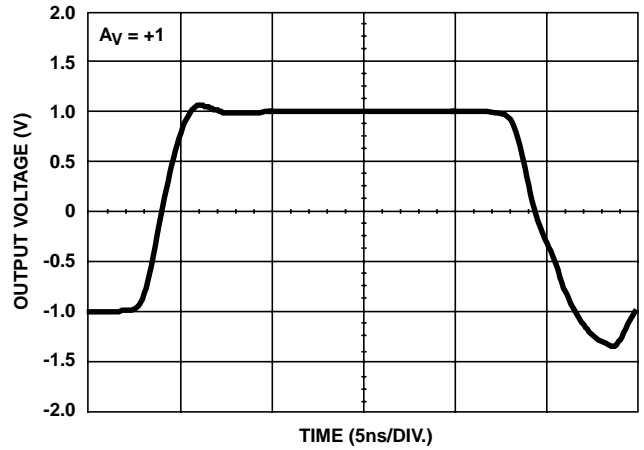


FIGURE 9. LARGE SIGNAL BIPOLAR PULSE RESPONSE

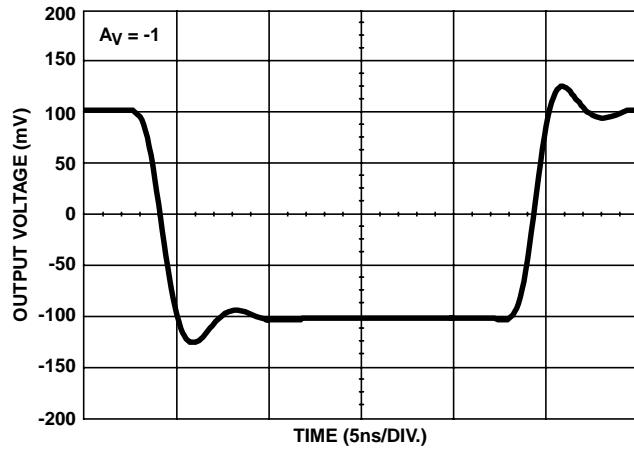


FIGURE 10. SMALL SIGNAL PULSE RESPONSE

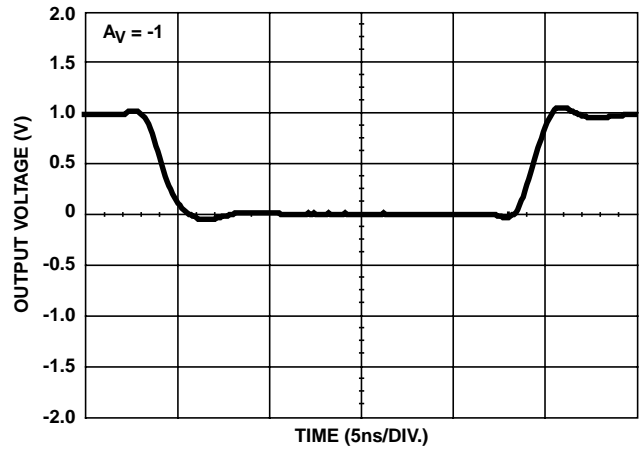


FIGURE 11. LARGE SIGNAL POSITIVE PULSE RESPONSE

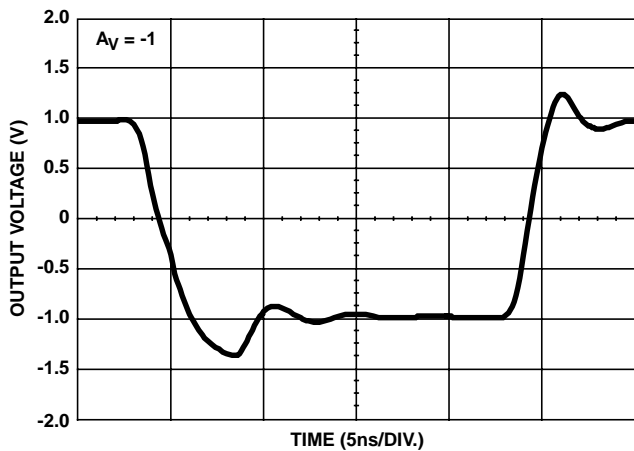


FIGURE 12. LARGE SIGNAL BIPOLAR PULSE RESPONSE

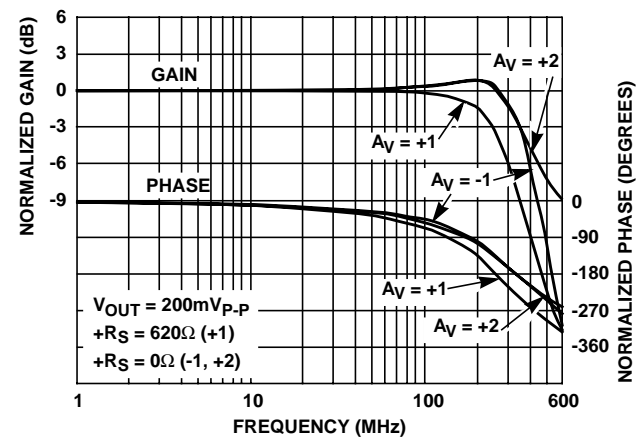


FIGURE 13. FREQUENCY RESPONSE

**Typical Performance Curves**  $V_{SUPPLY} = \pm 5V$ ,  $T_A = 25^\circ C$ ,  $R_L = 100\Omega$ , Unless Otherwise Specified (Continued)

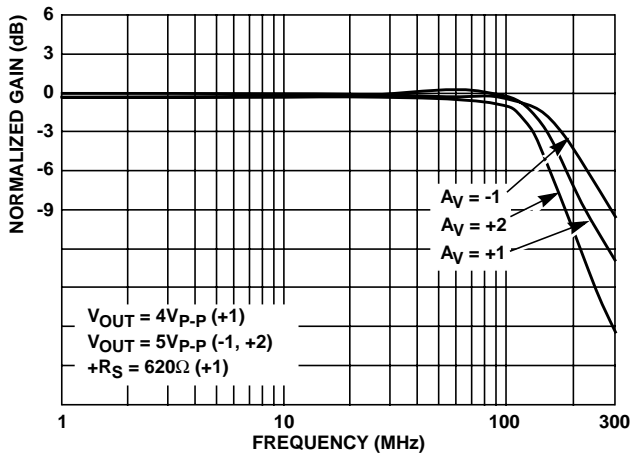


FIGURE 14. FULL POWER BANDWIDTH

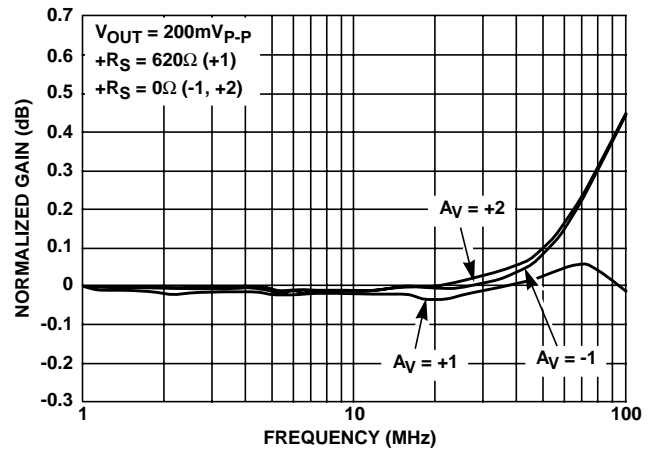


FIGURE 15. GAIN FLATNESS

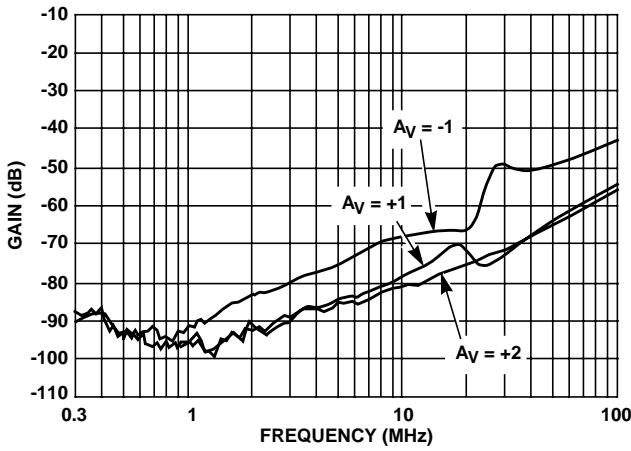


FIGURE 16. REVERSE ISOLATION

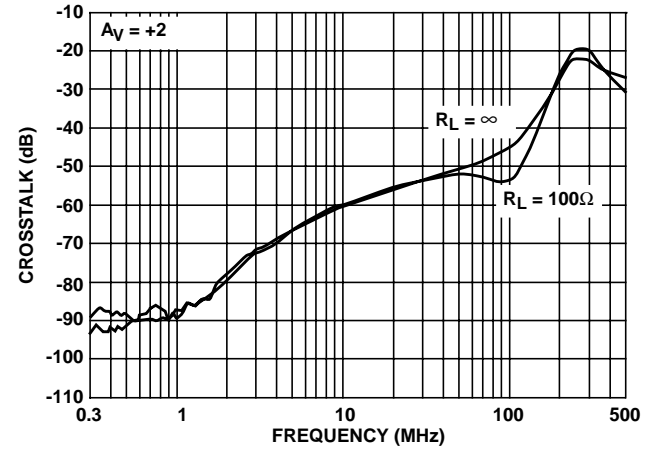


FIGURE 17. ALL HOSTILE CROSSTALK

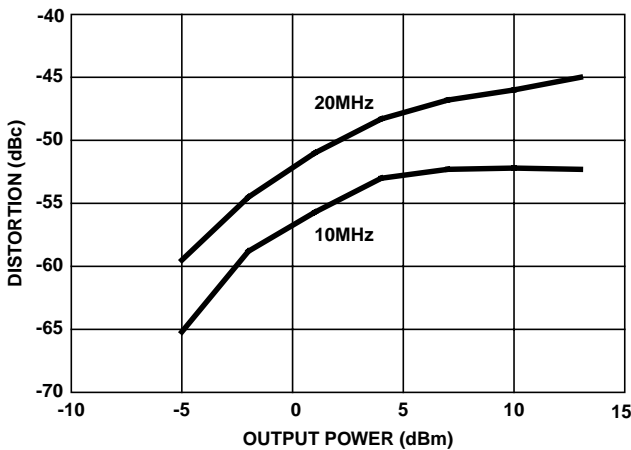


FIGURE 18. 2nd HARMONIC DISTORTION vs  $P_{OUT}$

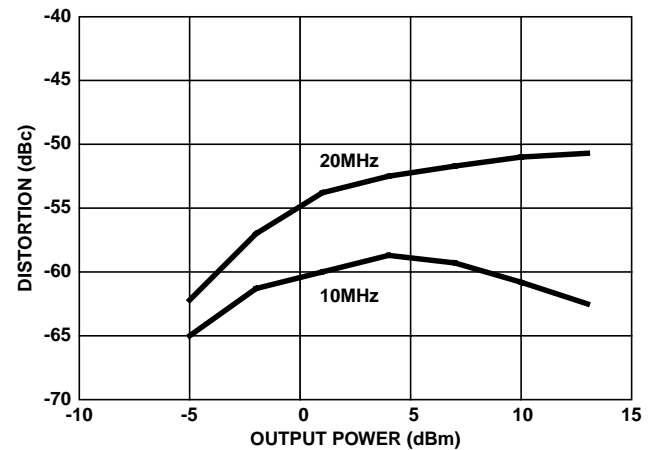


FIGURE 19. 3rd HARMONIC DISTORTION vs  $P_{OUT}$

**Typical Performance Curves**  $V_{SUPPLY} = \pm 5V$ ,  $T_A = 25^\circ C$ ,  $R_L = 100\Omega$ , Unless Otherwise Specified (Continued)

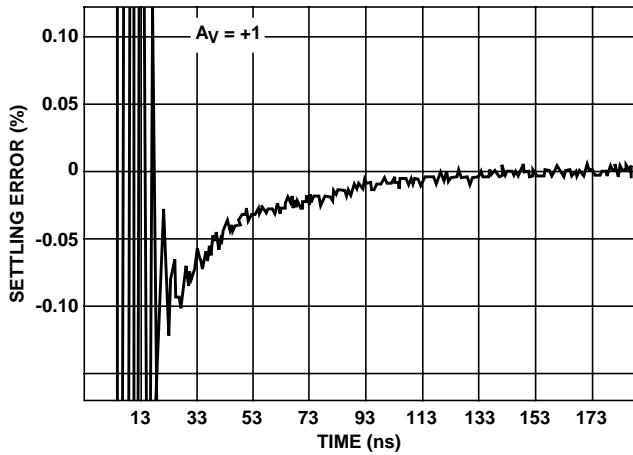


FIGURE 20. SETTLING RESPONSE

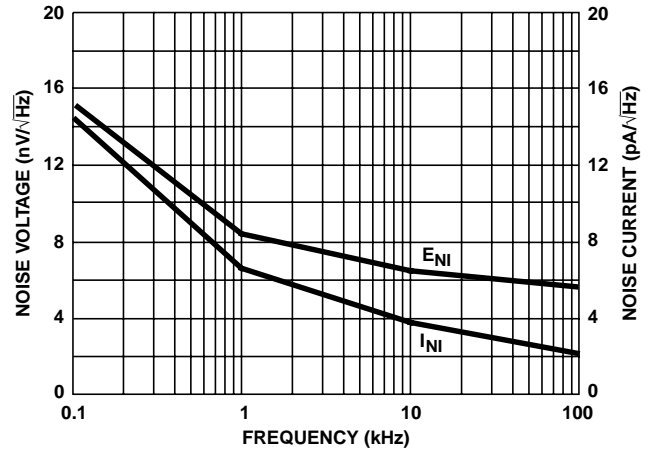


FIGURE 21. INPUT NOISE CHARACTERISTICS

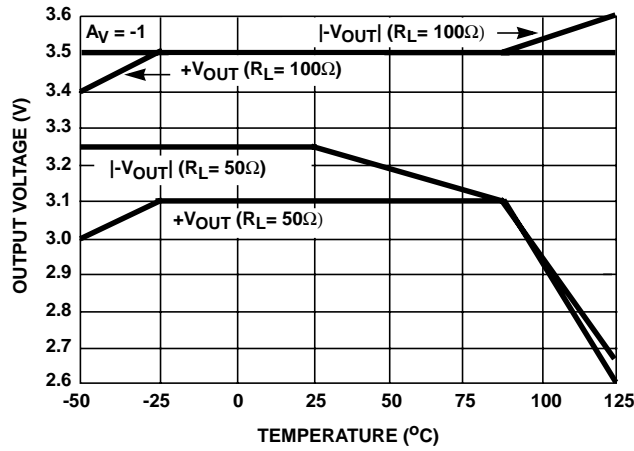
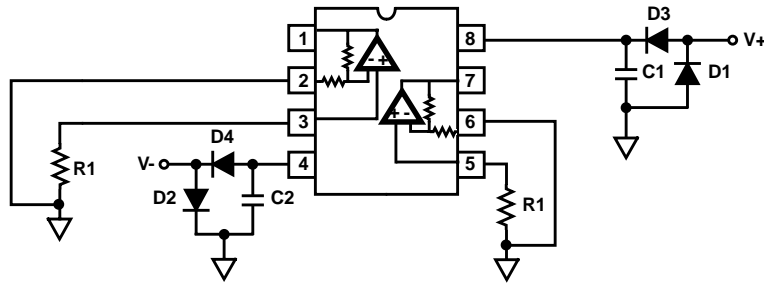


FIGURE 22. OUTPUT VOLTAGE vs TEMPERATURE

**Burn-In Circuit**

HS-1212RH CERDIP

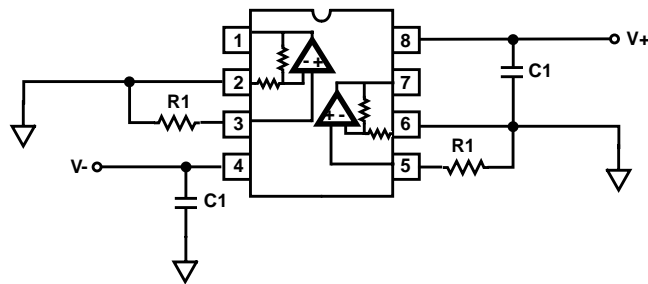


NOTES:

1. R1 = 1kΩ, ±5% (Per Socket).
2. C1 = C2 = 0.01μF (Per Socket) or 0.1μF (Per Row) Minimum.
3. D1 = D2 = 1N4002 or Equivalent (Per Board).
4. D3 = D4 = 1N4002 or Equivalent (Per Socket).
5.  $|(-V)| + |(+V)| = 11V \pm 1.0V$ .
6.  $10mA < |I_{CC}, I_{EE}| < 16mA$ .
7.  $-50mV < V_{OUT} < +50mV$ .

**Irradiation Circuit**

HS-1212RH CERDIP



NOTES:

8. R1 = 1kΩ, ±5%
9. C1 = 0.01μF
10. V+ = +5.0V ±0.5V
11. V- = -5.0V ±0.5V



# HS-1212RH

## Die Characteristics

### DIE DIMENSIONS:

69 mils x 92 mils x 19 mils  
1750 $\mu$ m x 2330 $\mu$ m x 483 $\mu$ m

### INTERFACE MATERIALS:

#### Glassivation:

Type: Nitride  
Thickness: 4k $\text{\AA}$   $\pm$ 0.5k $\text{\AA}$

#### Top Metallization:

Type: Metal 1: AlCu(2%)/TiW  
Thickness: Metal 1: 8k $\text{\AA}$   $\pm$ 0.4k $\text{\AA}$   
Type: Metal 2: AlCu(2%)  
Thickness: Metal 2: 16k $\text{\AA}$   $\pm$ 0.8k $\text{\AA}$

#### Substrate:

UHF-1X, Bonded Wafer, DI

#### Backside Finish:

Silicon

### ASSEMBLY RELATED INFORMATION:

#### Substrate Potential (Powered Up):

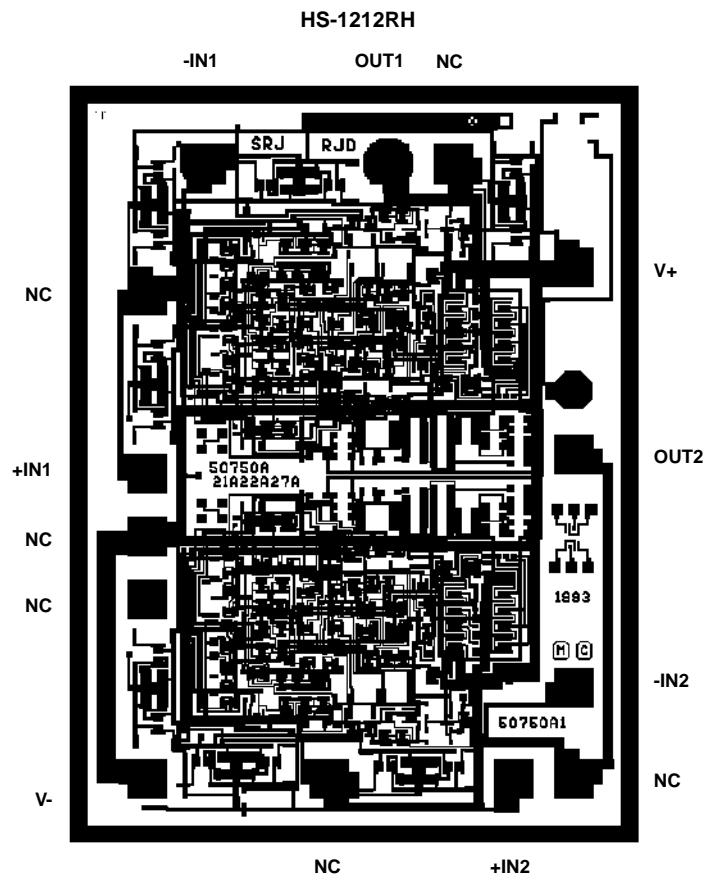
Floating (Recommend Connection to V-)

### ADDITIONAL INFORMATION:

#### Transistor Count:

180

## Metallization Mask Layout



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