

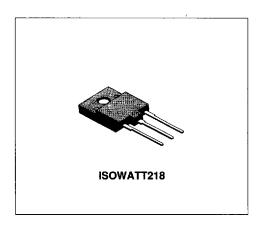
BUH417

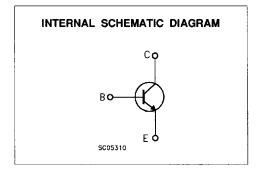
CRT HORIZONTAL DEFLECTION HIGH VOLTAGE NPN FASTSWITCHING TRANSISTOR

- HIGH BREAKDOWN VOLTAGE CAPABILITY
- FULLY INSULATED PACKAGE FOR EASY MOUNTING
- LOW SATURATION VOLTAGE
- HIGH SWITCHING SPEED
- COMPLETE CHARACTERIZATION OF POWER LOSSES AND SWITCHING TIMES AS A FUNCTION OF NEGATIVE BASE CUR-RENT FOR OPTIMUM DRIVE

APPLICATIONS:

- HORIZONTAL DEFLECTION STAGE IN STANDARD AND HIGH RESOLUTION DIS-PLAYS FOR TV's AND MONITORS
- SWITCHING POWER SUPPLY FOR TV's AND MONITORS





ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Value	Unit	
V _{СВО}	Collector-Base Voltage (I _E = 0)	1700	V	
Vceo	Collector-Emitter Voltage (I _B = 0)	700	V	
V _{EBO}	Emitter-Base Voltage (I _C = 0)	10	V	
lc	Collector Current	7	A	
Icm	Collector Peak Current (tp < 5 ms)	12	A	
l _B	Base Current	4	A	
l _{BM}	Base Peak Current (tp < 5 ms)	7	Α	
Ptot	Total Dissipation at T _c = 25 °C	55	W	
T _{stg}	Storage Temperature	-65 to 150	°C	
Tj	Max. Operating Junction Temperature	150	°C	

THERMAL DATA

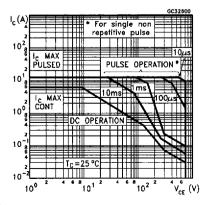
R _{thj-case}	Thermal Resistance Junction-case	Max	2.27	°C/W

ELECTRICAL CHARACTERISTICS (T_{case} = 25 °C unless otherwise specified)

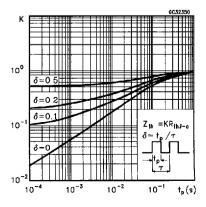
Symbol	Parameter	Test Conditions	Min.	Тур.	Max.	Unit
Ices	Collector Cut-off Current (VBE = 0)	V _{CE} = 1700 V V _{CE} = 1700 V T _J = 125 °C			1 2	mA mA
I _{EBO}	Emitter Cut-off Current (I _C = 0)	V _{EB} = 5 V			100	μА
V _{CEO(sus)}	Collector-Emitter Sustaining Voltage	Ic = 100 mA	700			٧
V_{EBO}	Emitter-Base Voltage (I _C = 0)	I _E = 10 mA	10			٧
V _{CE(sat)} *	Collector-Emitter Saturation Voltage	I _C = 4 A I _B = 1 A			1.5	٧
V _{BE(sat)} *	Base-Emitter Saturation Voltage	Ic = 4 A I _B = 1 A			1.3	٧
h _{FE} *	DC Current Gain	Ic = 4 A V _{CE} = 5 V Ic = 4 A V _{CE} = 5 V T _J = 100 °C	6 4			
t _s t _f	RESISTIVE LOAD Storage Time Fall Time	V _{CC} = 400 V I _C = 4 A I _{B1} = 1 A I _{B2} = 2 A		2.1 140	3.2 210	μs ns
t _s t _f	INDUCTIVE LOAD Storage Time Fall Time	$\begin{aligned} &I_{C} = 4 \text{ A} & f = 15625 \text{ Hz} \\ &I_{B1} = 1 \text{ A} &I_{B2} = 2 \text{ A} \\ &V_{ceflyback} = 1050 \text{ sin} \bigg(\frac{\pi}{10} 10^6 \bigg) t & V \end{aligned}$		4.3 370		μs ns
ts t _f	INDUCTIVE LOAD Storage Time Fall Time	$\begin{split} I_{C} &= 4 \text{ A} & f = 31250 \text{ Hz} \\ I_{B1} &= 1 \text{ A} & I_{B2} = 2 \text{ A} \\ V_{ceflyback} &= 1200 \text{ sin} \bigg(\frac{\pi}{5} 10^6 \bigg) t V \end{split}$		4.3 330		μs ns

^{*} Pulsed: Pulse duration = 300 µs, duty cycle 1.5 %

Safe Operating Areas



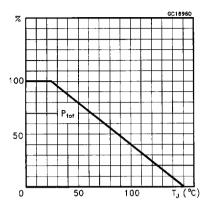
Thermal Impedance



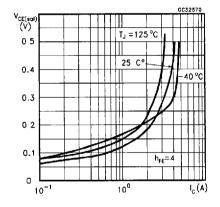
2/5

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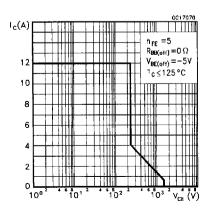
Derating Curves



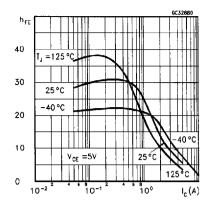
Collector-Emitter Saturation Voltage



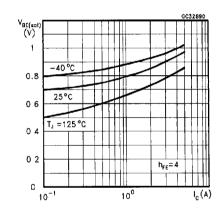
Reverse Biased SOA



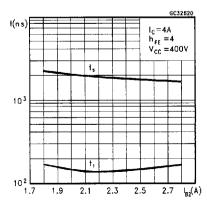
DC Current Gain



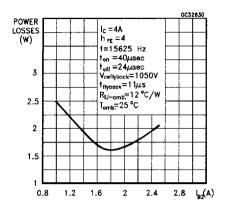
Base-Emitter Saturation Voltage



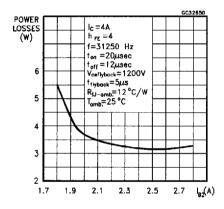
Switching Time Resistive Load



Power Losses at 16 KHz



Power Losses at 32 KHz

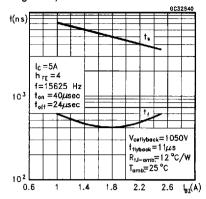


BASE DRIVE INFORMATION

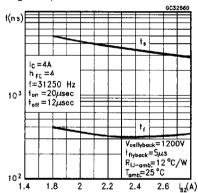
A fundamental parameter of high voltage power transistors like those used in the horizontal deflection stage is their junction temperature Tj, which, in turn, depends on the power dissipation. This parameter turns out to influence the system reliability under normal operation. Based on that, SGS-THOMSON has introduced a new dynamic, application-oriented characterization differing from the traditional data given in most datasheets.

In order to saturate the power switch and reduce conduction losses, adequate direct base current I_{B1} has to be provided for the lowest gain h_{FE} at $T_j = 100\,^{\circ}\text{C}$ (line scan phase). On the other hand, negative base current I_{B2} must be provided for

Switching Time Inductive Load at 16 KHz (see figure 2)



Switching Time Inductive Load at 32 KHz (see figure 2)



the transistor to be turned off (retrace phase). Most of the dissipation, especially in the deflection application, occurs at switch-off so it is essential to determine the value of $I_{\rm B2}$ which minimizes power losses, fall time $t_{\rm f}$ and, consequently, $T_{\rm j}.$ A new set of curves have been defined to give total power losses, $t_{\rm s}$ and $t_{\rm f}$ as a function of $I_{\rm B2}$ at both 16 KHz and 32 KHz scanning frequencies for choosing the optimum negative drive. The test circuit is illustrated in fig. 1.

Inductance L1 serves to control the slope of the negative base current l_{B2} in order that excess carriers in the collector recombine when base current is still present, thus avoiding any tailing phenomenon in the collector current. This effect

is, in any case, markedly reduced intrinsically by adopting the hollow emitter technology.

The values of L and C are calculated from the following equations:

$$\frac{1}{2} L (I_C)^2 = \frac{1}{2} C (V_{CEfly})^2$$

RBSOA INFORMATION

During turn-off with an inductive load, the power transistor has to withstand high voltages and high currents simultaneously with negative base-to-emitter voltage V_{BEoff}. Very often it has to reach a working area above V_{CEO}, remaining there all the time needed for the collector current I_C to fall to zero. The safe operation for the power transistor under these conditions is specified by RBSOA (Reverse Bias Safe Operating Area) which repre-

$$\omega = 2 \pi f = \frac{1}{\sqrt{L C}}$$

Where I_C= operating collector current, V_{CEfly}= flyback voltage, f= frequency of oscillation during retrace.

sents the permissible I_C-V_{CE} locus within which proper operation is guaranteed. RBSOA is strongly dependent on the circuit topology and is valid only under specified drive conditions. High voltage Multiepitaxial Fastswitching transistors of the BUH series have been optimized to give improved RBSOA to suit off-line switch mode power supplies applications.

Figure 1: Test Circuits for Dynamic Characterization.

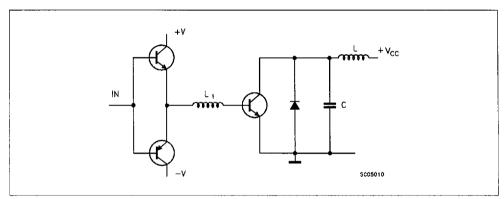


Figure 2: Switching Waveforms in a Deflection Circuit

