

## GENERAL-PURPOSE HIGH-FREQUENCY WIDEBAND AMPLIFIERS

### $\mu$ PC1675G, $\mu$ PC1676G, $\mu$ PC1688G

#### 1. GENERAL

The  $\mu$ PC1675G,  $\mu$ PC1676G and  $\mu$ PC1688G are silicon monolithic ICs developed as general-purpose high-frequency wideband amplifiers.

These ICs are based on the  $\mu$ PC1651G packaged in a 4-pin disc mold. The present ICs are each packaged in a 4-pin mini-mold suitable for surface mounting on higher density print board. (the  $\mu$ PC1651G has been discontinued).

The features of these amplifier ICs are:

- <1> The 4-pin mini-mold package as shown in Figure 1 substantially reduces the mounting area.
- <2> The ICs are supplied on an embossed tape conforming to EIAJ's "Taping Dimensions of Electronic Components (RC-1009)". This embossed tape is 8 mm wide, and suits automatic mounting.
- <3> The following three models are available, classified by power gain.
  - $\mu$ PC1675G:  $G_P = 12$  dB TYP.,  $NF = 5.5$  dB TYP. (@  $f = 500$  MHz)
  - $\mu$ PC1676G:  $G_P = 22$  dB TYP.,  $NF = 4.5$  dB TYP. (@  $f = 500$  MHz)
  - $\mu$ PC1688G:  $G_P = 21$  dB TYP.,  $NF = 4.0$  dB TYP. (@  $f = 500$  MHz)
- <4> All the models can operate at high frequency and in wide band.
 

$\mu$ PC1675G: 1900 MHz TYP. $\mu$ PC1676G: 1200 MHz TYP. $\mu$ PC1688G: 1100 MHz TYP.	}	frequency point of -3 dB gain from flat gain
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- <5> Input/output matched to  $Z_o = 50 \Omega$ .
- <6> Single power source ( $V_{CC} = 5$  V TYP.)

Figure 1. Package (unit: mm)

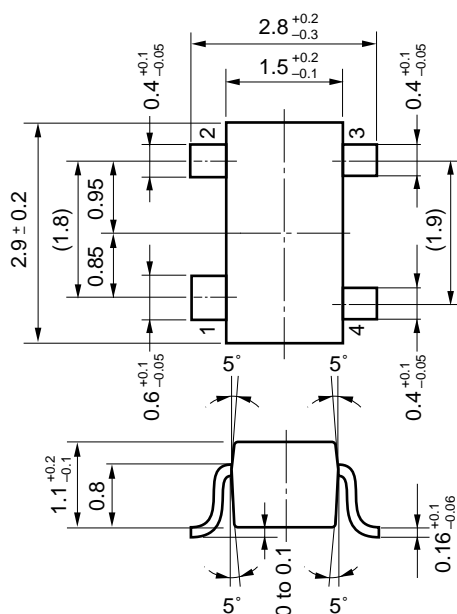
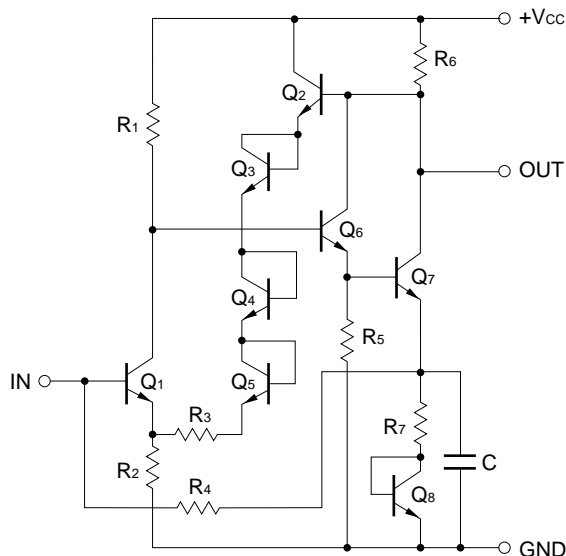


Figure 2. Internal Equivalent Circuit



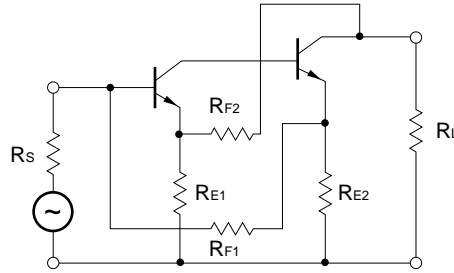
## 2. CIRCUIT CONFIGURATION

Figure 2 shows the internal equivalent circuit of the  $\mu\text{PC1675G}/\mu\text{PC1676G}/\mu\text{PC1688G}$ .

The equivalent circuits of all the models are the same, and gain is set by changing  $R_2$ ,  $R_3$ ,  $R_4$ , and  $R_7$ . Like the  $\mu\text{PC1651G}$ , each circuit is designed as multiple negative feedback amplification from the output block to the base and emitter of  $Q_1$ . MOS capacitance  $C$  is connected to the emitter of  $Q_7$  to peak the frequency characteristics.

The basic circuit is the single-end multiple negative feedback amplification type shown in Figure 3. This circuit configuration has the following features:

**Figure 3. Circuit Configuration**



- <1> Excellent frequency-gain characteristics.
- <2> The input/output impedance and gain can be determined by the feedback resistance.
- <3> Excellent noise characteristics because the resistance at the emitter of transistor in the input stage is lower than that of the differential circuits.
- <4> Excellent impedance matching with external circuits as compared with differential circuits, improving the output efficiency and decreasing the noise.

As the first approximation, the input/output impedances  $R_i$  and  $R_o$ , and gain  $S_{21}$  of the circuit in Figure 3 can be generally determined by the following equation.

$$R_i = \frac{(R_{F2} + R_{E2}) R_{E1} \cdot R}{R_{E1} \cdot R + R_{E2} (R_{F1} + R_{E1} + R)} \quad \dots\dots\dots (1)$$

$$R_o = \frac{(R_{F1} + R_{E1}) R_{E2} \cdot R}{R_{E1} (R_{E2} + R_{F2} + R) + R_{E2} \cdot R} \quad \dots\dots\dots (2)$$

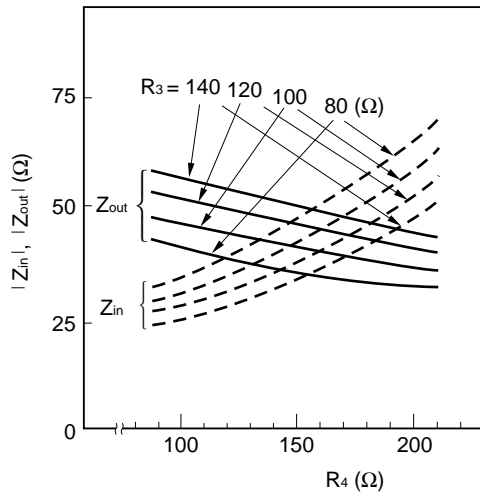
$$S_{21} = \frac{R_{F1} + R_{E1}}{R_{E1}} \quad \dots\dots\dots (3) \quad (\text{where } R_S = R_L = R)$$

By following modification on Figure 3, multiple negative feedback amplifier is realized as monolithic IC shown in Figure 2.

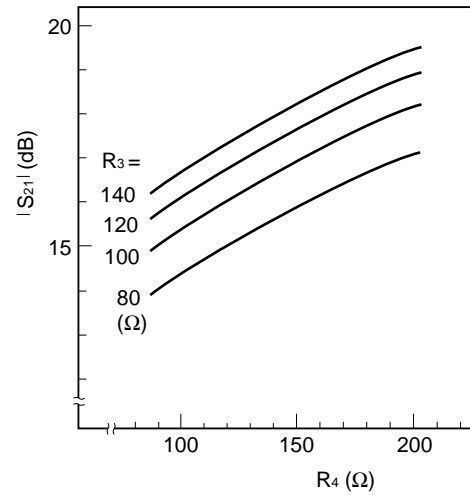
- <1> To increase the feedback loop gain, the final stage  $Q_6$  and  $Q_7$  are connected in a Darlington configuration.  $Q_6$  is connected to  $R_5$  to optimize the bias current.
- <2> As for feedback to the emitter of  $Q_1$  from the collectors of  $Q_6$  and  $Q_7$ , the impedance and voltage are adjusted by the emitter-follower configuration of  $Q_2$  and the diodes of  $Q_3$  through  $Q_5$ .
- <3>  $Q_8$  diode rises up  $Q_7$  emitter potential to supply bias current to  $Q_1$  base through feedback path.

Simulation results of input/output impedance and gain vs.  $R_3$ ,  $R_4$  feedback resistance are shown below (the result of this simulation is slightly different from the calculation using equation 1 through 3 because the circuit configuration is more complicated than Figure 3.  $R_3$  is equivalent to  $R_{F2}$  in Figure 3, and  $R_4$  is equivalent to  $R_{F1}$ ).

**Figure 4. Input/Output Impedance vs. Feedback Resistor**



**Figure 5. Forward Transmission Gain vs. Negative Feedback Resistor**



As shown in Figures 4 and 5, the input/output impedance and gain can be easily controlled by feedback resistors  $R_3$  and  $R_4$ .

Respectively, the input/output impedance is set to  $50 \Omega$  for wideband operation, and  $R_3$  and  $R_4$  to  $120 \Omega$  and  $200 \Omega$  to obtain a sufficient gain.

### 3. CHARACTERISTICS

This chapter compares the measured characteristics of  $\mu\text{PC1675G}$  and  $\mu\text{PC1676G}$  as representative IC. The absolute maximum ratings and electrical characteristics are shown in Table 1 and 2. (Test circuit is shown in Figure 20.)

**Table 1. Absolute Maximum Ratings ( $T_A = +25\text{ }^\circ\text{C}$ )**

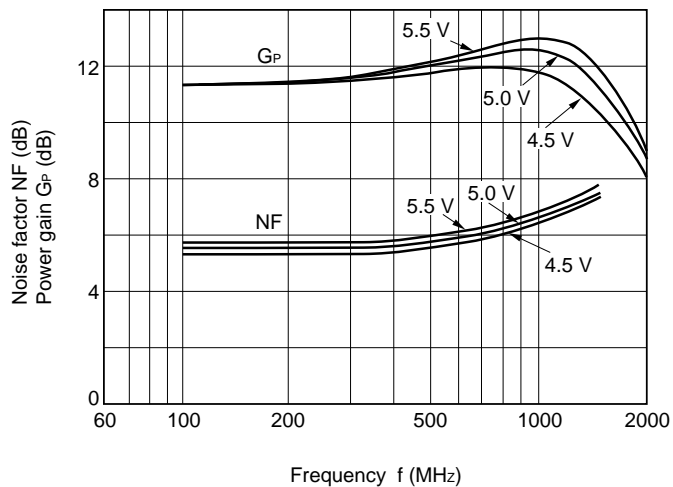
Parameter	Symbol	Rating	Unit
Supply voltage	$V_{CC}$	6	V
Total dissipation	$P_T$	200	mW
Operating temperature range	$T_{opt}$	-40 to +85	$^\circ\text{C}$
Storage temperature range	$T_{stg}$	-55 to +150	$^\circ\text{C}$

**Table 2. Electrical Characteristics ( $V_{CC} = 5\text{ V}$ ,  $T_A = +25\text{ }^\circ\text{C}$ )**

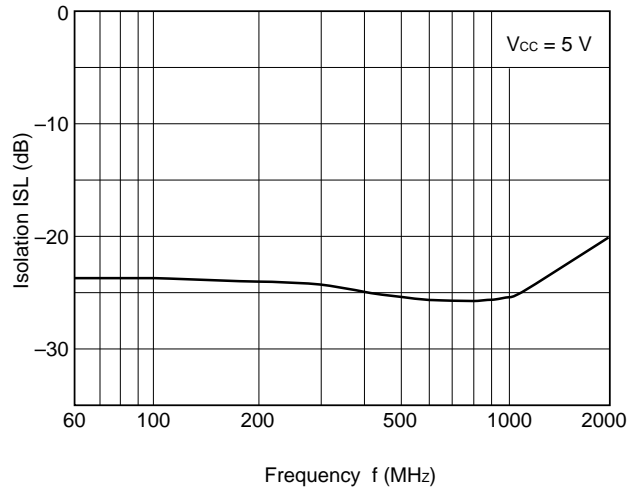
Parameter	Symbol	Condition	Specifications						Unit
			μPC1675G			μPC1676G			
			MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	
Supply current	I <sub>CC</sub>	Without signal	12	17	22	14	19	24	mA
Power gain	G <sub>P</sub>	f = 500 MHz	10	12	14	19	22	24	dB
Noise factor	NF	f = 500 MHz	–	5.5	7.0	–	4.5	6.0	dB
Upper-limit operating frequency	f <sub>u</sub>	–3 dB from gain flat	1600	1900	–	1000	1200	–	MHz
Isolation	ISL	f = 500 MHz	21	25	–	24	28	–	dB
Input return loss	RL <sub>in</sub>	f = 500 MHz	9	12	–	9	12	–	dB
Output return loss	RL <sub>out</sub>	f = 500 MHz	8	11	–	6	9	–	dB
Output power	P <sub>O</sub>	f = 500 MHz, P <sub>in</sub> = 0 dBm	2	4	–	3	5	–	dBm

Figures 6 through 11 and Figures 12 through 17 show the characteristic curves including the voltage characteristics and temperature characteristics of the  $\mu\text{PC1675G}$  and  $\mu\text{PC1676G}$ . Figure 18 shows the impedance characteristics (Smith chart).

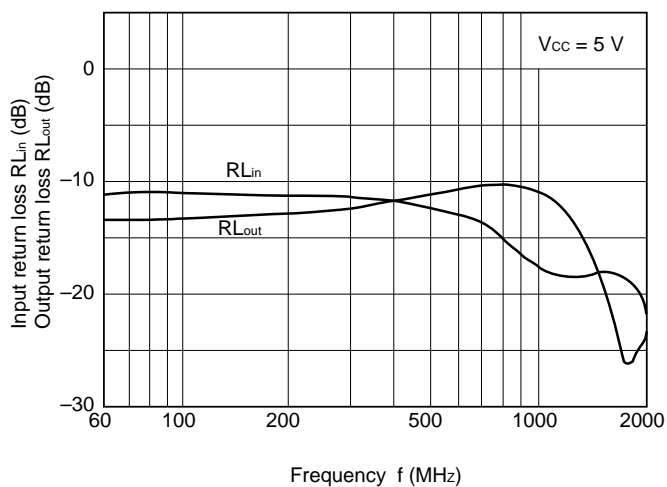
**Figure 6.  $G_P$ , NF vs.  $f$  Characteristics of  $\mu$ PC1675G**



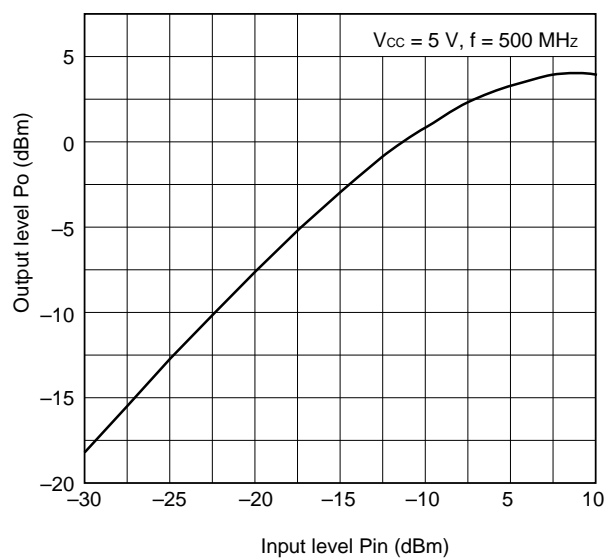
**Figure 7. Isolation vs.  $f$  Characteristics of  $\mu$ PC1675G**



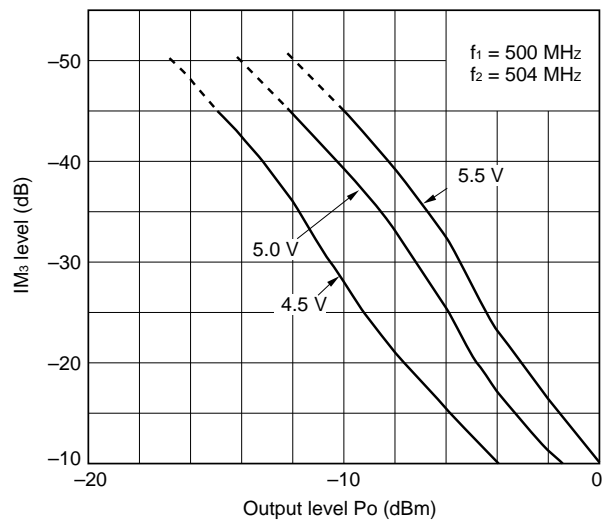
**Figure 8. Return Loss vs.  $f$  Characteristics of  $\mu$ PC1675G**



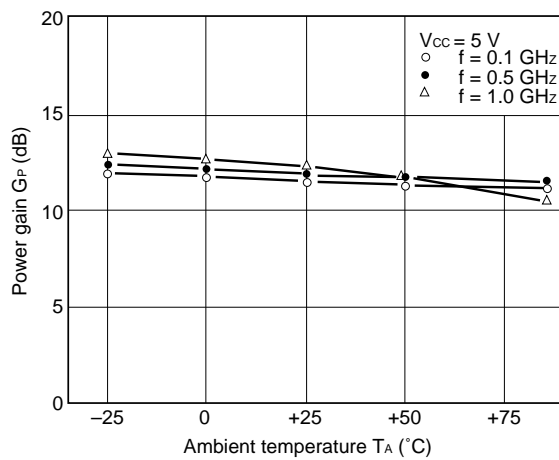
**Figure 9. Input/Output Characteristics of  $\mu$ PC1675G**



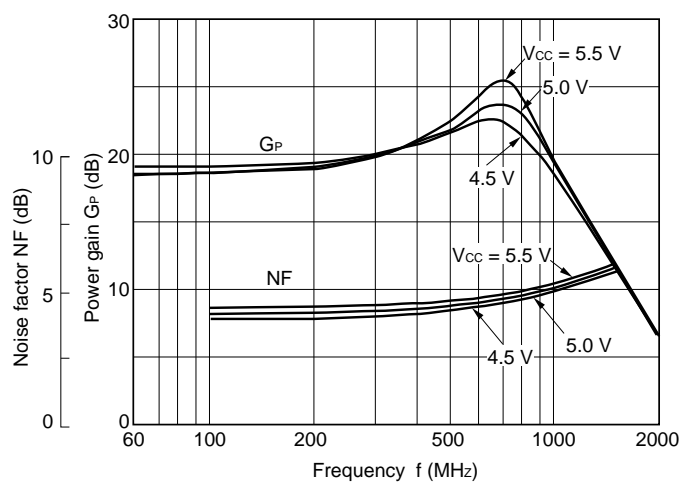
**Figure 10.  $IM_3$  Characteristics of  $\mu PC1675G$**



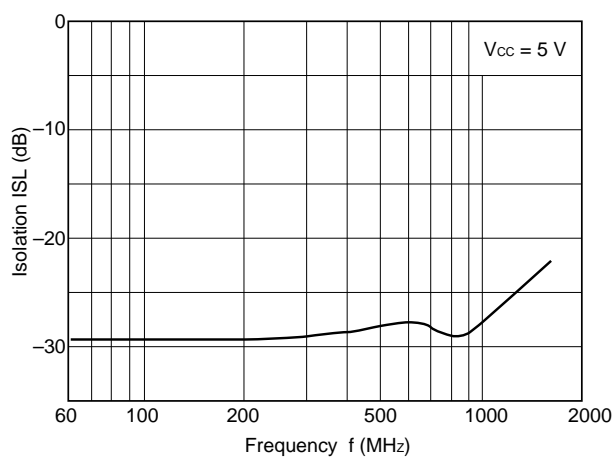
**Figure 11.  $G_P$  vs. Temperature Characteristics of  $\mu PC1675G$**



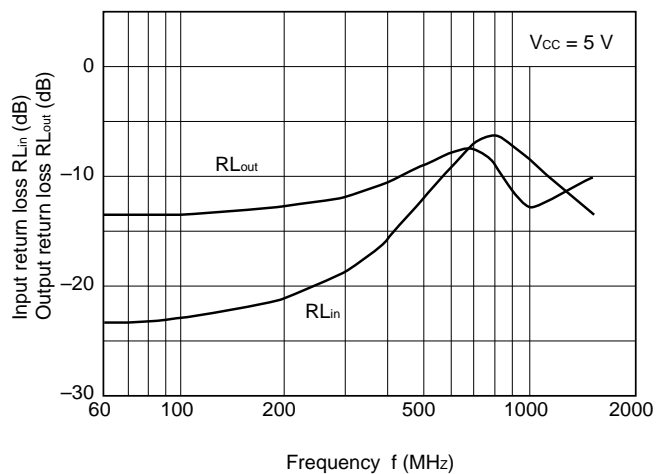
**Figure 12.  $G_P$ , NF vs.  $f$  Characteristics of  $\mu PC1676G$**



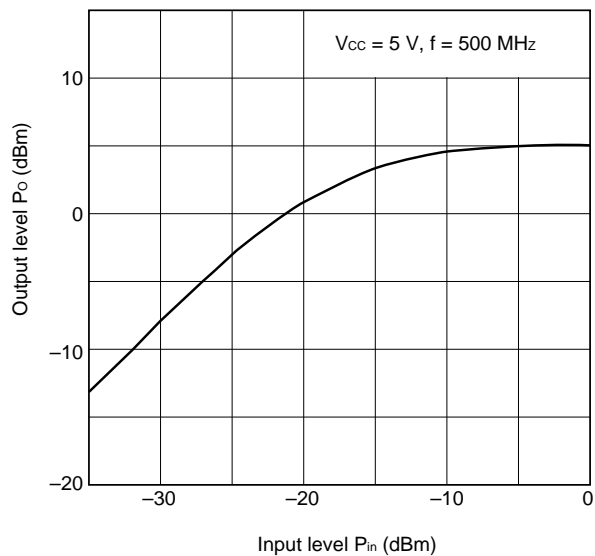
**Figure 13. Isolation vs.  $f$  Characteristics of  $\mu PC1676G$**



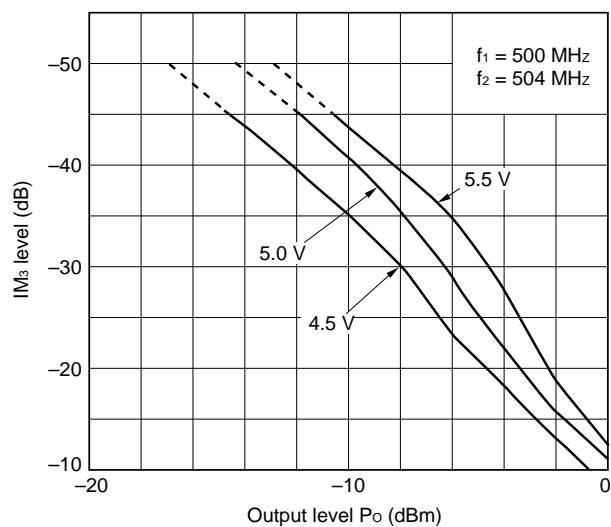
**Figure 14. Return Loss vs. f Characteristics of  $\mu$ PC1676G**



**Figure 15. Input/Output Characteristics of  $\mu$ PC1676G**



**Figure 16. IM<sub>3</sub> Characteristics of  $\mu$ PC1676G**



**Figure 17. G<sub>P</sub> Temperature Characteristics of  $\mu$ PC1676G**

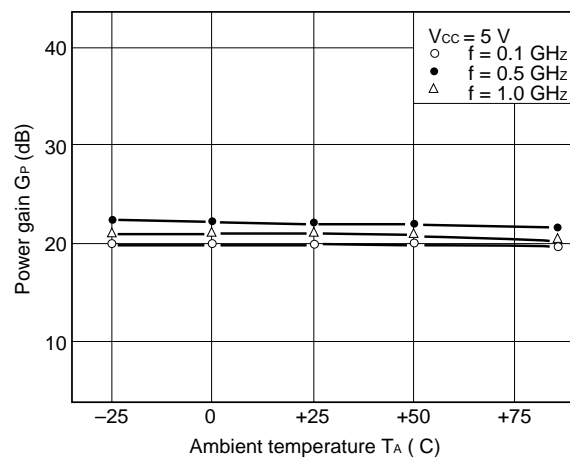


Figure 18 (a).  $S_{11}$  vs.  $f$  Characteristics of  $\mu$ PC1675G

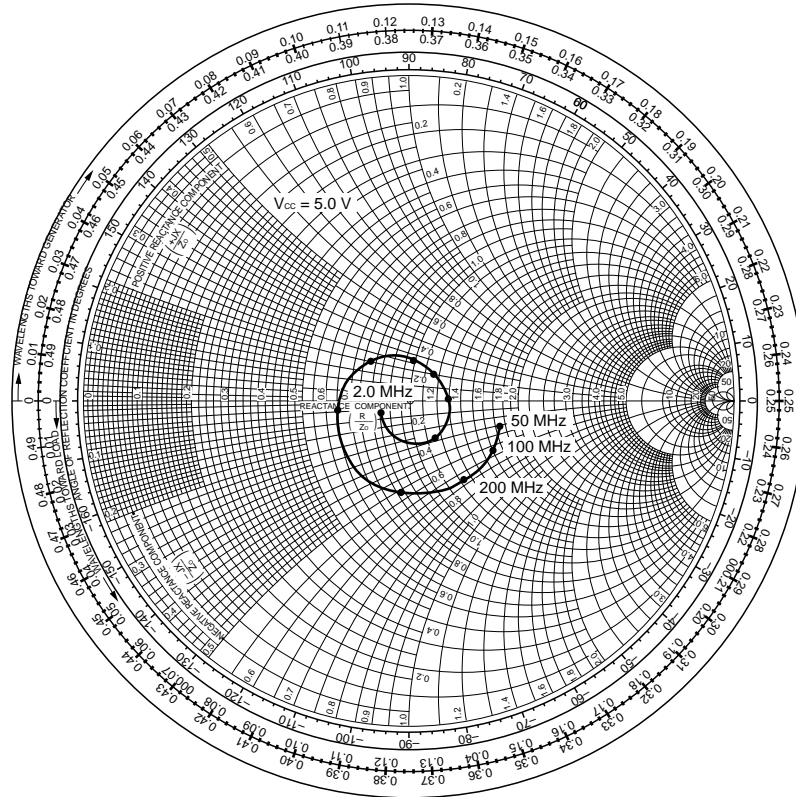


Figure 18 (b).  $S_{22}$  vs.  $f$  Characteristics of  $\mu$ PC1675G

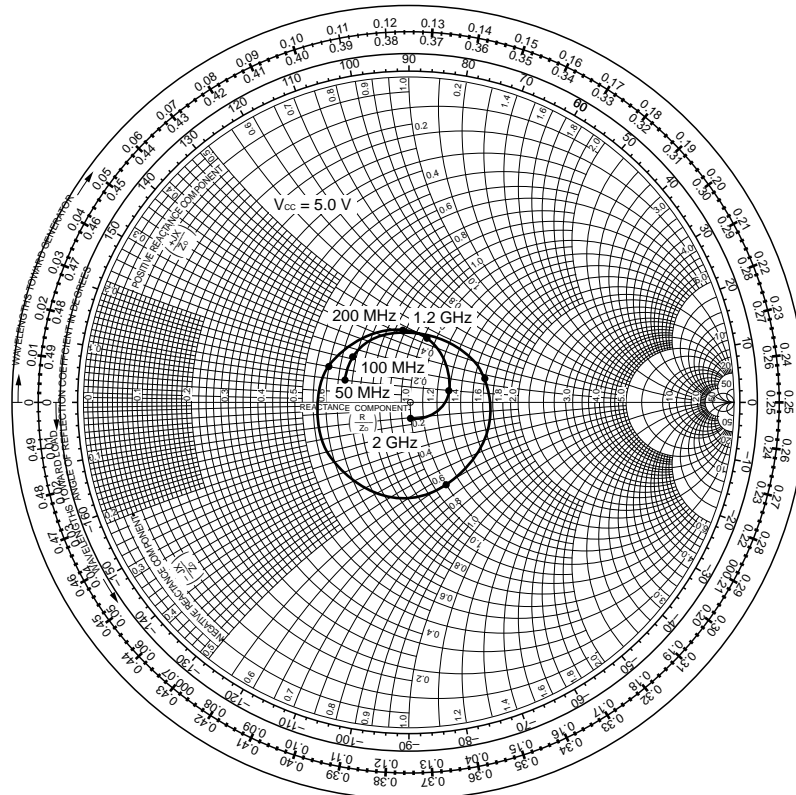




Figure 18 (c).  $S_{11}$  vs.  $f$  Characteristics of  $\mu\text{PC1676G}$

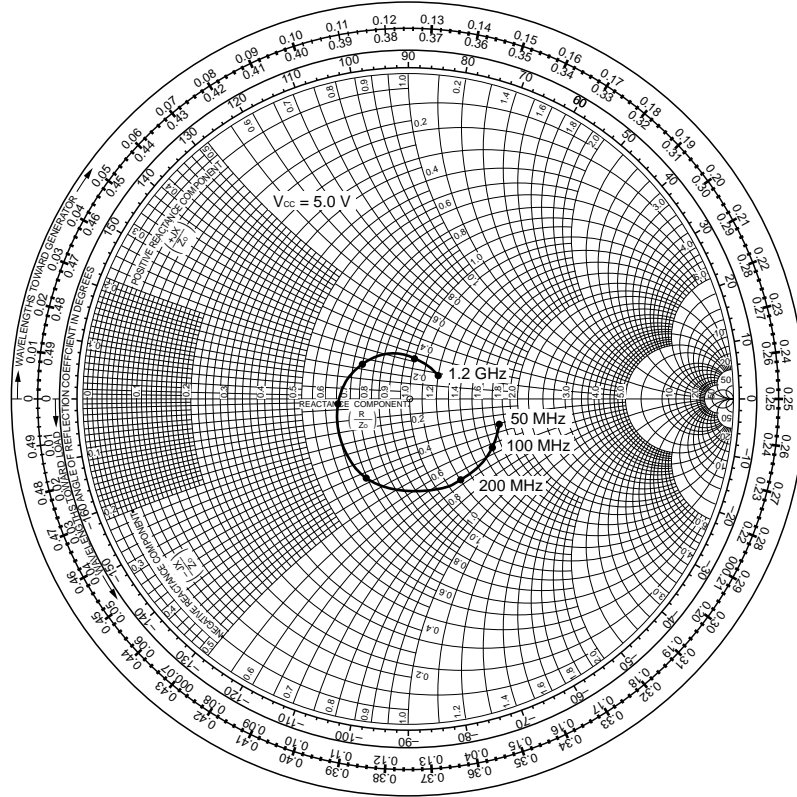
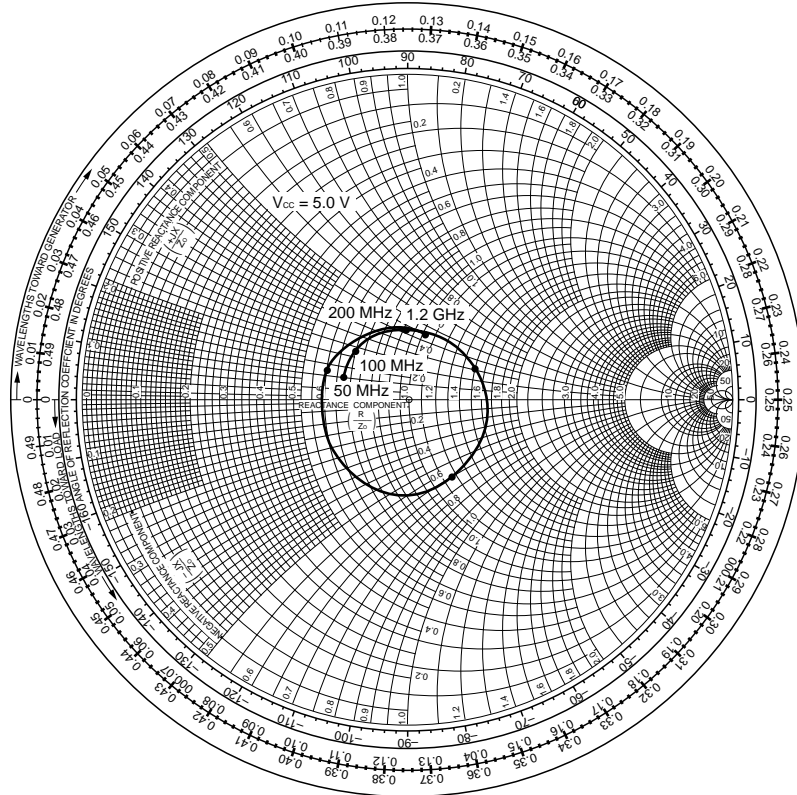


Figure 18 (d).  $S_{22}$  vs.  $f$  Characteristics of  $\mu\text{PC1676G}$



#### 4. PRINTED PATTERN MOUNTING EXAMPLE

The  $\mu\text{PC1675G}/\mu\text{PC1676G}/\mu\text{PC1688G}$  are wideband amplifiers of simple construction with only four pins: input, output, power, and GND.

Because the upper-limit operating frequency is as high as 1900 MHz TYP. in the case of  $\mu\text{PC1675G}$  and 1200 MHz TYP. with the  $\mu\text{PC1676G}$ , the frequency characteristics substantially vary depending on the conditions of the print pattern (especially at high frequencies).

Figure 19 shows these variations in the characteristics of the  $\mu\text{PC1675G}$ . Print boards A, B, and C in this figure are:

Board A : Double-sided copper clad epoxy glass board with GND on the back and front surfaces connected, and a GND line inserted between input and output to provide an isolation effect.

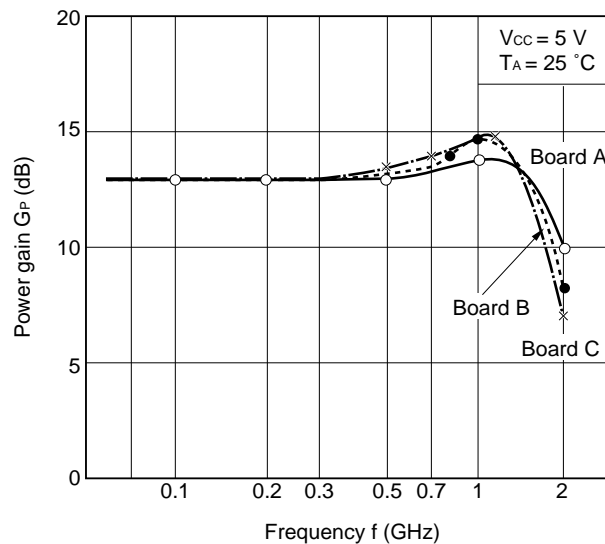
Figure 20 shows an example pattern.

Board B : Board A without GND line between input and output.

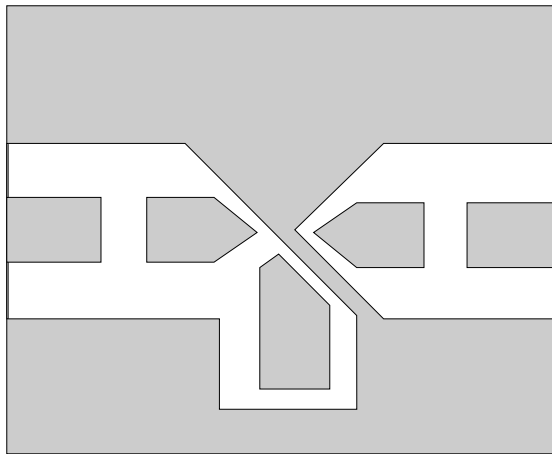
Board C : Board B without GND on back side.

As shown in figure 19, a print board equivalent to A is necessary because of peaking in the vicinity of  $f = 1$  GHz and an increase in the frequency characteristics. The GND line between input and output has an especially important effect. Board A is used to measure characteristics in Chapter 3.

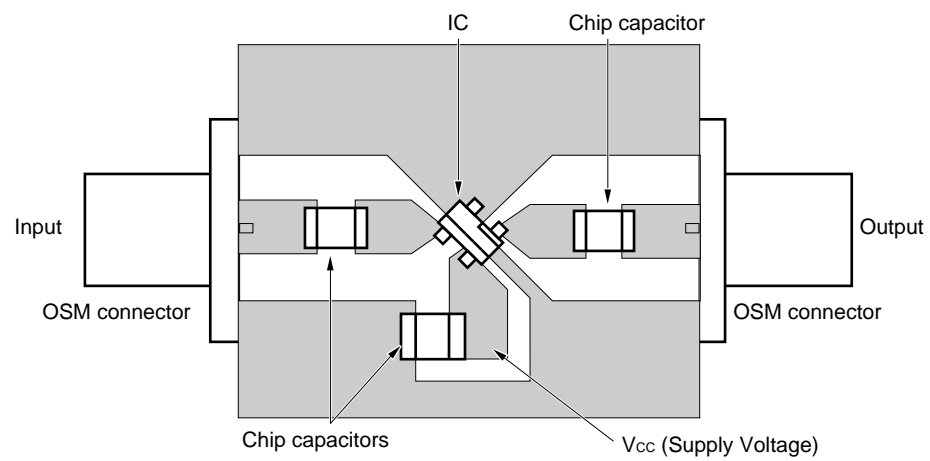
**Figure 19. Mounting Characteristics Example of  $\mu\text{PC1675G}$  ( $G_P = 13$  dB)**



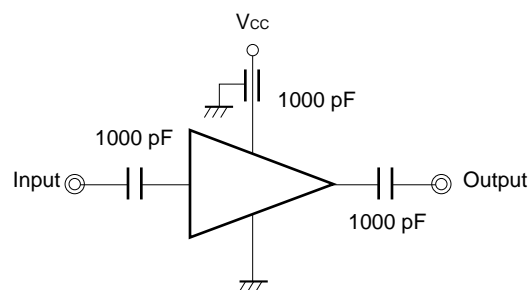
**Figure 20 (a). Pattern Example (Top View)**



**Figure 20 (b). Mounting Example (Top View)**



**Figure 20 (c). Operation Circuit**



## 5. APPLICATION EXAMPLE

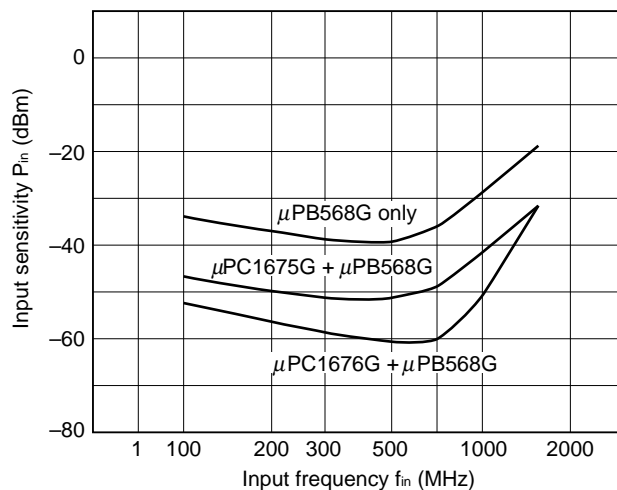
### (1) Buffer amplifier for prescaler

The input sensitivity of 1-GHz-class prescalers used in UHF and VHF TV tuners has recently increased. Even so, a buffer amplifier is connected in the stage preceding these prescalers. The purpose of this is to decrease coupling with the local oscillation stage and to improve isolation after the oscillation stage and prescaler.

Figure 21 shows the sensitivity characteristics when NEC's  $\mu$ PB568G 1-GHz prescaler is used, and Figure 22 shows a circuit example. As the load on the  $\mu$ PC1675G/1676G, a 51- $\Omega$  resistor is connected to GND. Values of 50 to 200  $\Omega$  are suitable for this resistor. Because the saturation output of the  $\mu$ PC1675G/1676G can be kept to 4 to 5 dBm, overload input to the prescaler can also be prevented (usually, a prescaler does not divide the frequency when an input higher than 8 to 10 dBm is applied).

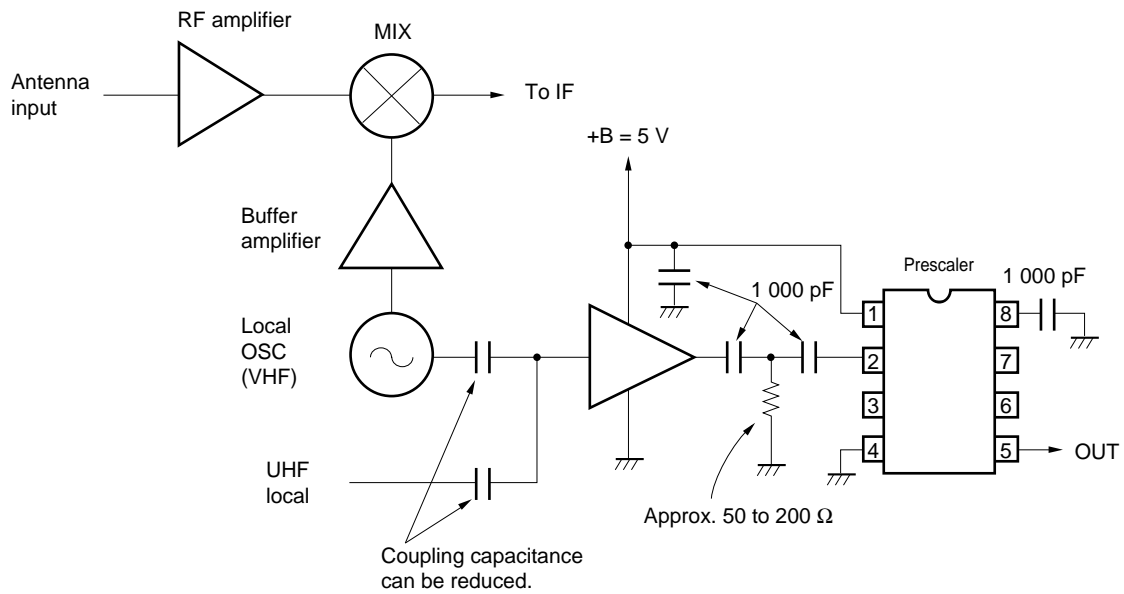
As another local oscillation peripheral, the amplifier IC can also be used as a buffer amplifier to the MIX stage to prevent oscillation drift when a high input is applied to the antenna (Figure 22).

Figure 21. Input Sensitivity Characteristics of  $\mu$ PC1675G/1676G + Prescaler  $\mu$ PB568G



**Note**  $\mu$ PB568G has been discontinued.

**Figure 22. Prescaler Buffer Amplifier**



## (2) Cascade amplifier

The input/output impedance of the  $\mu\text{PC1675G/1676G/1688G}$  is matched to  $50\ \Omega$  so that multiple amplifier ICs can be connected.

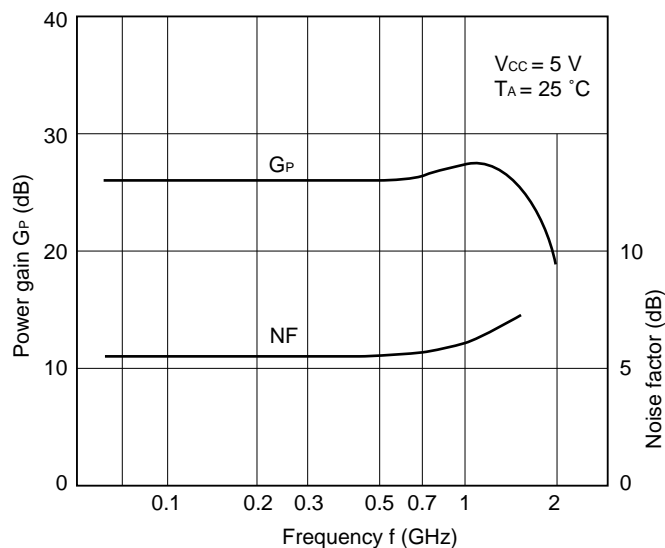
Therefore, the amplifier ICs can be used as a cascade amplifier.

Figure 23 shows an example of the characteristics of two  $\mu\text{PC1675Gs}$  connected in cascade. For the print pattern, a double-sided copper clad epoxy glass board is used as described in Chapter 4, and the input and output are isolated by the GND line.

The  $\mu\text{PC1676G}$  is a high-gain type IC. However, because of peaking at  $f = 700\ \text{MHz}$ , the targeted characteristics must be considered of the combination.

As a combination to produce output  $P_o \cong 10\ \text{dBm}$ , use the  $\mu\text{PC1675G} + \mu\text{PC1658G}$ .

**Figure 23. Cascade Amplifier Characteristics of Two  $\mu\text{PC1675Gs}$**



[MEMO]

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