

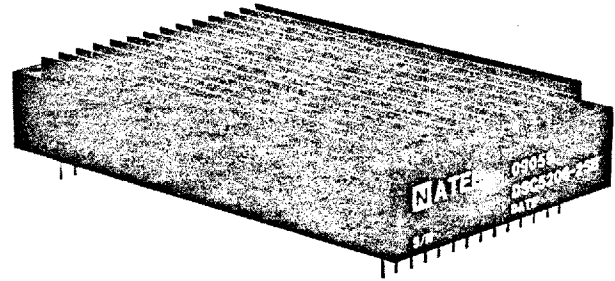
NATEL**DSC5206**

Reference Powered, 12 VA Output 16-bit, 4 Arc-minute Accuracy Digital-to-Synchro Converter

Features

T-71-35-03

- ✓ **Fully Protected 12 VA Output**
 - (current limiting)
 - (short circuit proof)
 - (thermal cut-off)
 - (over-voltage transient protected)
- **No DC Power Supplies Needed**
 - (reference powered)
- **Microprocessor Compatible**
 - (8- and 16-Bit)
- **Double-Buffered Digital Inputs**
- **4 Arc-minute Accuracy**
- ✓ **Low Power Dissipation**
 - (1.25 watts per VA delivered to load)
- **Built-in "KICK" Circuit**
 - (prevents synchro "hang-ups")
- ✓ **Fully Isolated Operation**
 - (inputs/outputs/reference)
- **BIT (built-in test) Output**
- ✓ **Compact PCB Mounting**
 - (5.2 X 3.2 X 1.0 inches)

**Applications**

Training Simulators
Remote Indicators
Gun Fire Control
Navy Re-transmission Systems
Test Equipment

Description

The Model DSC5206 is the first 4 arc-minute 12 VA synchro driver with Built-in 16-bit Digital-to-Synchro capability. The 12 VA output power is delivered efficiently through a reference-powered design that develops an internal "dynamic power supply" which reduces power dissipation by a factor of 2 over conventional designs. The 5206 has an extremely low (0.05%) scale factor variation which further helps reduce power when driving TR loads. Being reference powered, it also eliminates the need for all external DC power supplies. Packaged in a single, PCB mountable module with integral heat dissipating fins, the 5206 offers excellent thermal transfer and high reliability.

The high output drive power of 12 VA makes the 5206 the ideal choice when driving single and multiple active Torque Receiver (TR) Synchro loads, Control Differential Transmitters (CDXs) and Control Transformers (CTs). Included also is a built-in "KICK" circuit which senses when a TR load may be "hung-up" and automatically shifts the output angle by 120° to free-up the synchro. In addition, the output stage is fully

protected and includes fast-acting active current limiting, thermal cutoff, and output stage transient suppression to make the 5206 virtually indestructible.

A built-in-test circuit continuously monitors the output currents in all three output drivers along with other internal test points. An open collector logic output referenced to the logic ground immediately indicates if a fault condition is present.

The logic interface is easy, having the flexibility designed in to make interfacing possible with a minimum number of components. This includes the double-buffering of all input logic data bits. All data bits (1-16) are true binary coded and are actively pulled down to ground, so if the application requires less than 16-bits any unused bits may be left unconnected. Control bits LBE, HBE, and LDC control the operation of the data input buffers. All digital inputs are TTL and 5-V CMOS compatible, using internally derived logic thresholds that guarantee 0.8-V as a logic "0" and 2.4-V as a logic "1."

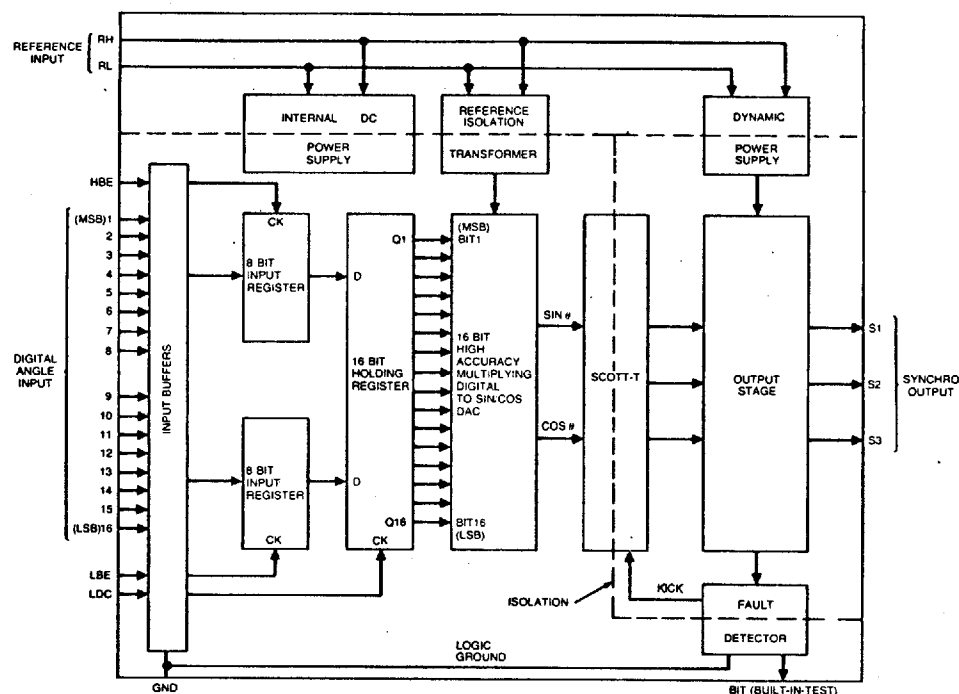


FIGURE 1 5206 Functional Block Diagram

The operation of Model 5206 is illustrated in the functional block diagram of Figure 1. The reference voltage (RH-RL) is received by both a power transformer and an isolation transformer. The power transformer has separate secondary windings. One set of windings provides bias and dynamic power supply voltages to the output stage; while another set provides power to the input circuitry, and is therefore referenced to the incoming "logic ground" line. The reference isolation transformer provides a scaled-down representation of the input reference to the Multiplying digital-to-analog sine/cosine converter (DAC).

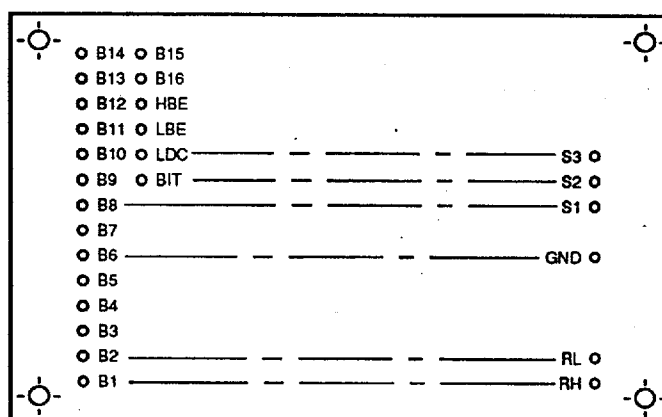
The digital word representing the input angle is applied to the input buffer registers, which are configured as two independently enabled bytes of 8 bits each. These bytes are controlled by the HBE (high byte enable) and LBE (low byte enable) input logic controls. When interfacing the 5206 to an 8-bit microprocessor, these registers are normally addressed sequentially over common data lines. When interfacing to a 16-bit data bus, both input registers are enabled simultaneously to accept a single 16-bit word. The second 16-bit "Holding Register" allows the input registers to be presented to the Sine/Cosine DAC simultaneously as a single 16-bit word. This holding register is controlled by the LDC (load converter) input. This double-buffering is especially important in 8-bit microcomputer-based systems where false codes and servo "hunting" would otherwise occur. The presence of these two registers in series allows the systems and circuit designers maximum flexibility in controlling the updating of the converter with digital data in systems with and without microprocessors. All three registers pass data from input to output whenever their respective enable signals are at logic "1," and latch data when the enable signals are at logic "0." The output of the holding register is applied to the digital input of the Multiplying Sine/Cosine DAC. This DAC accepts the ac reference as a second input and multiplies the two together while following Sine and Cosine laws. The result

are signals at the ac reference frequency and phase which precisely reflect the Sine and Cosine of the input digital angle. The operation of the Multiplying Sine/Cosine DAC is very similar to a pair of conventional four-quadrant multiplying DACs, with the exception that the transfer function is controlled by resistor ladders that follow Sine and Cosine laws instead of linear transfer functions. The format of these signals is changed from Sine/Cosine to Synchro format through an isolation Scott-tee type transformer. The resultant 3 signals are then applied to the output stage.

The output stage consists of three precision power amplifiers in push-pull class AB configurations, powered from a dynamic power supply. This dynamic supply reduces the dissipation in the output section by allowing the output transistors to operate with less average voltage across them as compared to operation from a fixed DC power source. To assure stable operation over temperature and load variations, precision operational amplifiers are used as the primary amplifier gain element. In addition to providing short circuit protection, current limiting, and voltage transient protection; the power amplifiers are designed to shut down in a high impedance output state when the amplifier temperature reaches 125 degrees centigrade, thereby making them virtually indestructible.

An internal "KICK" circuit is used in the 5206 to prevent the possibility that the torque receiver may become locked at 180° from the true angle. It does this by shifting the electrical angle by 120° if the output is in current limit for more than four seconds.

The internal BIT circuit provides a fault indication if there is a loss of reference, output short circuit or overload, internal thermal shutdown, or internal circuit failure. The "open collector" logic output allows maximum flexibility in interfacing to system fault logic.



BOTTOM VIEW

FIGURE 2 DSC5206 Pin Assignments

GND	Digital Ground - To be connected to the input logic ground. This is also the ground reference for the BIT output.	LBE*	Low Byte Enable - Data bits 9-16 enter the input buffer register when LBE is set to a logic "1." When LBE is at logic "0," the input data bits are ignored.
B1-B16*	Parallel Input Data Bits - B1 is MSB. Bit weight = 180 degrees B16 is LSB. Bit weight = 0.0055 degrees	LDC*	Load Converter - When LDC is set to logic "1," the converter will transfer the contents of the two input buffer registers to the input holding register. This presents data to the converter and results in a corresponding analog output. When LDC is set to logic "0," data is held in the holding register and the outputs of the two input buffer registers are ignored.
RH, RL	Input Reference Voltage - RH stands for reference high. RL stands for reference low.	BIT	Built-in Test - Open collector logic output signal referenced to the logic ground. Logic "0" = no fault condition present. Logic "1" (open circuit) = fault condition.
S1, S2, S3	Analog Synchro Output Signals - These outputs are the synchro equivalent of the digital input angle. They are isolated from both the reference input and the logic input ground.		
HBE*	High Byte Enable - Data bits 1-8 enter the input buffer register when HBE is set to a logic "1." When HBE is at logic "0," input data bits 1-8 are ignored.		

*Note: Unused pins may be left unconnected.

Specifications

PARAMETER	VALUE	REMARKS	TEST LEVEL
Digital Angular Resolution			
	16-bits (0.33 arc-minutes)		Note 2
Accuracy			
	± 4.0 arc-minutes (option S) ± 8.0 arc-minutes (option P)	Accuracy applies over the full operating temperature, frequency, power supply, and load ranges	Note 1
Reference/Power Input			
Voltage	115 V-rms, ±10%	For 90 V-rms nominal output	Note 2
Frequency	360 to 440 Hz		Note 3
Input Current	35 mA-rms maximum 230 mA-rms maximum	Vref = 115 V-rms, No Load Vref = 115 V-rms, 12.5 VA Load	Note 1
Breakdown Voltage	500 V-dc minimum	To logic ground or any output	Note 3
Harmonic Distortion	Up to 10 percent	Without degradation in accuracy	Note 3
Digital Inputs		Transient-protected CMOS	
Logic "0" level	- 0.3 to 0.8 V-dc		Note 2
Logic "1" level	2.4 to 5.5 V-dc		Note 2
Input Current Data bits 1-16	15 µA typical (30 µA max.), active pull down to ground	Unused pins may be left unconnected	Note 3
Input Current HBE, LBE, LDC	- 15 µA typical (-30 µA max.), active pull up to internal 5 V-dc	Unused pins may be left unconnected	Note 3
Data Bit Coding	Positive logic, natural binary angle	B1 is MSB, B16 is LSB	Note 3
Register Controls		Active-high transparent latches	
HBE	Logic "1" Logic "0"	Data bits 1-8 enter high-byte input register High-byte input register holds data	Note 1
LBE	Logic "1" Logic "0"	Data bits 9-16 enter low-byte input register Low-byte input register holds data	Note 1
LDC	Logic "1" Logic "0"	Data from input register enters holding register Holding register holds data	Note 1
Pulse Width HBE, LBE, and LDC	600 ns minimum	For guaranteed data transfer	Note 3
Data Set-up Time	200 ns minimum	Data stable before HBE or LBE low-to-high transition	Note 3
Data Hold Time	200 ns minimum	Data stable after HBE or LBE high-to-low transition	Note 3
BIT Output		Referenced to Digital Ground	
Output Current Sink Source (Leakage)	1 mA minimum @ 0.8 V-dc 10 nA typ. @ 25°C, (20 V-dc) 100 µA max. over temp. (20 V-dc)	Open collector output	Note 1
Logic "0"	- 0.3 to 0.8 V-dc @ 1 mA load	For no Fault Detected	Note 1
Logic "1"	Open collector, V max = 20 V-dc	Fault Detected	Note 1

PARAMETER	VALUE	REMARKS	TEST LEVEL
Synchro Analog Outputs			
Voltages (Line-to-Line)	90 V-rms nominal	For nominal reference voltages. The outputs vary in direct proportion to the reference amplitude	
Gain	0.783 \pm 1%	115 V-rms reference input / 90 V-rms output	Note 1
Radius Accuracy	0.05% maximum	Scale factor variation with angle	Note 2
Drive Capability	12.5 VA minimum		Note 1
Output Current Drive	225 mA peak minimum	Between S1, S2, and S3 outputs	Note 3
Output Impedance (dc to 440 Hz)	less than 2.5 ohms		Note 3
Load Regulation	0.25% maximum	From no load to full load	Note 2
Synchro Load Impedance	$ Z_{so} > 486 \Omega$	12.5 VA limit	Note 1
Output Setting Time	250 μ s maximum	To specified converter accuracy (179° step)	Note 2
Phase Shift	less than 2 degrees	Reference to output	Note 3
Quadrature Output	0.25% maximum		Note 2
Output dc Offset (Line-to-Line)	± 10 mV typical, ± 50 mV maximum		Note 2
Thermal Cut-off	85°C top-plate temperature min.		Note 2
Output Short Circuit Duration	Indefinite	All outputs together simultaneously	Note 3
Power Dissipation		Internal	
No Load 12.5 VA Load	4.0 watts maximum 15.0 watts maximum	For Resistive loads. Does not include power dissipated in the load	Note 3
Thermal Resistance		Based on internal module dissipation	
Case (Top Plate) to Ambient	3 degrees C per watt typical	Actual value depends upon cooling configuration	Note 3
Junction to Case Top	3 degrees C per watt maximum	For the worst case device junction vs. output load	Note 3
Physical Characteristics			
Size	5.20 X 3.17 X 1.04 inches (132 X 81 X 26 mm)		Note 3
Weight	17 oz. (482g) typical 24 oz. (680g) maximum		Note 3

NOTE 1. Compliance of each component to this specification is 100% guaranteed by Natel. To assure compliance, this key parameter is 100% tested.

NOTE 2. Compliance of each component to this specification is 100% guaranteed by Natel. To assure compliance, AQL levels are verified using a lot sample level in the range of one to five percent.

NOTE 3. Compliance of each component to this specification is 100% guaranteed by Natel. To assure compliance, AQL levels are verified using a lot sample level of less than one percent. Note 3 parameters are maximum design limits.

If your application requires 100% testing of any additional parameters of this specification or requires non-standard input or output characteristics, please contact a Natel Applications Engineer or the Sales Department.

Absolute Maximum Ratings

Reference Input 138 V-rms
 Digital Inputs - 0.3 V-dc to +6.5 V-dc
 Storage Temperature - 65°C to +135°C

Although the digital inputs have integral transient protection, this protection is not a substitute for proper electrostatic handling procedures. This part is ELECTROSTATIC SENSITIVE and must be treated as such.

Output Protection

The Model 5206 incorporates several protection methods that together make the 5206 virtually indestructible. These methods are:

1. Active current limiting
2. Thermal cut-off
3. Overvoltage transient protection

The active current limiting circuitry in the 5206 continuously monitors the instantaneous current in each of the three output drivers. When an overcurrent or output short circuit condition exists, the peak current that can be supplied to the load is instantly limited to a value that is safe for the components used within the 5206.

The thermal cut-off circuit of the 5206 uses a solid-state temperature-sensing element attached to the top plate. The voltage from this temperature sensor provides an indication when the power amplifiers temperature reaches 125°C. If this occurs, a disable signal is applied to each of the output power amplifiers, which removes all output current drive capability. The result is that the outputs go into a high-impedance state and are no longer capable of driving load current. When the internal temperature drops to a safe level, the output stages are automatically restored to their normal state.

The 5206 incorporates overvoltage transient protection on both the reference input and the synchro outputs. These transient protection networks utilize rugged transient suppression diodes that automatically conduct to suppress transient energy whenever the applied voltages reach dangerous levels. The reference-protection diode is connected internally across RH-RL and may begin to conduct if the reference input (RH-RL) reaches 190 volts peak. The output-protection diodes are connected in a "delta" configuration, with one diode between each of the S1-S2, S2-S3, and S1-S3 output pairs. Transient protection is necessary at the output of the 5206 due to the fact that synchros are, by nature, inductive loads and can produce voltage transients many times their nominal voltage due to inductive "kick."

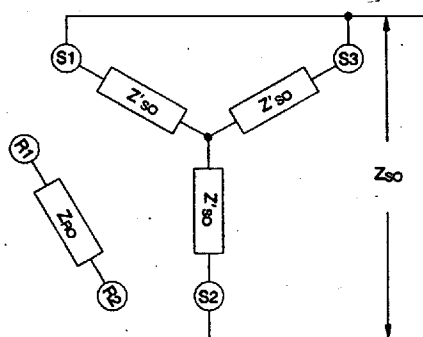


FIGURE 3 Synchro Load Schematic

Synchro Loads

There are several types of synchro loads, including Control Transformers (CTs), Torque Receivers (TRs), and Control Differential Transmitters (CDXs). The 12.5 VA output drive of the 5206 makes it possible to drive all but the heaviest TR loads easily. In many cases, the 5206 can drive multiple loads. The two most common loads driven by the 5206 are CTs and TRs.

CTs are electromechanical synchro devices which provide a null voltage output from the rotor winding whenever the actual shaft angle of the CT matches the angle sent to the CT from the S1, S2, and S3 outputs of the 5206. The actual transfer function of a CT is as follows:

$$V_{\text{rotor}} (\text{rms}) = K \times V_{\text{L-L}} \times \sin(\theta - \phi)$$

where:

- K = gain of the CT
 $V_{\text{L-L}}$ = line-to-line voltage from 5206
 θ = the angle represented by the 5206 output
 ϕ = the CT shaft angle

In systems that use CTs, they are utilized as position sensing elements rather than as torque or motor elements. The force that is used to position the shaft generally is provided by a motor coupled to the common shaft. CT impedances, therefore are relatively high.

A schematic diagram of a typical synchro load is shown in Figure 3. Z_{so} is the impedance measured between one leg (S2, for example) and the other two legs (S1, S3) shorted together, with the rotor open circuit. The relationship between Z_{so} and the individual winding impedances (Z'_{so}) is given by:

$$Z_{\text{so}} = (3/2) \times Z'_{\text{so}}$$

The relationship between the synchro output voltages, output VA, and Z_{so} is as follows:

$$VA = 3/4 \times V^2 / Z_{\text{so}}$$

where:

VA is the VA required from the 5206 to drive the load and V is the rms value of the maximum line-to-line 5206 output voltage*.

*The maximum value of an rms voltage refers to the rms voltage level when the voltage is at its maximum value, since the line-to-line output voltages vary with input digital angle. For example, the rms voltage between S3 and S1 is maximum when the input angle is 90°.

Example:

From 5206 Data Sheet, page 4, 90 V-rms output can drive $|Z_{\text{so}}| = 486$ ohms. To calculate the VA drive:

$$VA = 3/4 \times V^2 / Z_{\text{so}} = 3/4 \times (90)^2 / 486$$

$$VA = 12.5$$

TABLE 1. Typical Control Transformer Parameters

CT Type	Frequency	Voltage	Z_{so}	$ Z_{\text{so}} $	Required VA
11 CT4e	400	90 V-rms	$700 + j4900$	4950	1.23
15 CT4c	400	90 V-rms	$1020 + j8330$	8392	0.72
18 CT4c	400	90 V-rms	$1360 + j12600$	12700	0.48
23 CT4c	400	90 V-rms	$1230 + j14300$	14353	0.42

The Model 5206 can be used to drive single or multiple Torque Receiver (TR) loads. TRs are constructed in the same manner as CTs, except that they generally have much lower impedances than CTs and are meant to provide torque to the rotating shaft.

TRs provide torque as a result of the interaction of two magnetic fields within the TR; one field produced by the S1, S2, and S3 stator windings, and one field from a reference source applied to the rotor windings. The TR can be considered an "active" load in that it "acts" against the opposing 5206 output, depending upon shaft angle, to produce a torque at the TR shaft. Torque is produced whenever the TR shaft angle and the 5206 input angle are different, thereby producing a voltage gradient between the 5206 output and the TR stator output. Circulating currents are developed as a result of this voltage gradient to provide the "magnetomotive force" that produces the "opposing" magnetic field against the rotor field. The opposing magnetic fields within the TR apply a torque gradient in attempting to rotate the TR shaft until the shaft angle is equal to the 5206 input angle. When the two angles are equal, the result is a "null" condition where the torque gradient is zero.

Theoretically, the TR represents an infinite load impedance to the 5206 output when the TR shaft angle is exactly equal to the 5206 input angle. In actual practice, however, the effective load impedance at "null" (shaft angle = 5206 input angle) will be reduced by the effects of two variables:

1. Line-to-line voltage differential between the TR stator and 5206 output.
2. Line-to-line phase-shift differential between the TR stator and 5206 output.

Any such line-to-line voltage and/or phase-shift differentials will give rise to an additional VA (voltage-ampere) requirement from the 5206, resulting in a loss of available VA for producing torque. This additional VA requirement is as follows:

$$VA_{D/S} = [3(V_{LL})^2/2Z_{SS}] \times \sqrt{(\Delta E/2V_{LL})^2 + [\sin(\Delta\sigma/2)]^2}$$

where:

- V_{LL} = 5206 maximum L-L voltage (90 V-rms)
 ΔE = (5206 - TR) L-L voltage differential
 Z_{SS} = Stator impedance with rotor shorted
 $\Delta\sigma$ = (5206 - TR) phase shift differential (°)

For example, to find the additional VA required by the 5206 (excluding the VA required to produce torque), consider the following example of driving a type 15TRX4a torque receiver:

- V_{LL} = 90 V-rms
 ΔE = 2.7 V-rms (3% of 90 V-rms)
 $|Z_{SS}|$ = 66 ohms
 $\Delta\sigma$ = 5
 VA_{5206} = 8.5

As this example demonstrates, VA is easily "stolen" from the 5206 due to line-voltage and phase-shift differentials. This is an important point to consider when designing TR systems.

The torque gradient required from the TR shaft will depend upon the particular application. Some applications, such as driving indicators or other visual readouts will not require much torque. Other applications, where the TR may be driving heavier loads, will require more VA. The torque that can be provided to the shaft will depend upon the type of TR; the "available" VA after the effects outlined above are accounted for and the difference between the shaft angle and the input angle to the 5206. The VA required by the TR to produce a torque gradient is described by the following equation:

$$VA_{5206} = [3(V_{LL})^2/2Z_{SS}] \times \sin[(\theta - \phi)/2]$$

where:

- V_{LL} = 5206 maximum L-L voltage (90 V-rms)
 Z_{SS} = TR stator impedance with rotor shorted
 θ = 5206 input angle
 ϕ = TR shaft angle
 VA_{5206} = Volt-amperes needed from 5206

Consider an example where a type 15TRX4a torque receiver is required to produce a torque gradient of 4 g-cms at a differential angle ($\theta - \phi$) of 2°. The operating parameters are the same as the previous example. The required VA from the 5206 can be calculated as follows:

$$VA = [3 \times (90)^2 / (2 \times 66)] \times \sin(2/2) = 3.2 VA$$

This calculation should be combined with the previous calculation for the "additional" VA in order to predict the total VA required from 5206. In order to combine the calculations, the equation below should be used in order to take into account the phase relationship between the various current components supplied by the 5206.

$$VA_{5206} = [3(V_{LL})^2/2Z_{SS}] \times \sqrt{[(\Delta E/2V_{LL}) + \sin[(\theta - \phi)/2]]^2 + [\sin(\Delta\sigma/2)]^2}$$

The terms for this equation are defined in the previous examples.

*Note: To reduce the VA requirement, stator resistors (in series with S1, S2, S3) can be added to increase the total "Z_{SS}" impedance.

Voltage imbalance ($\Delta E/V_{LL}$) used in calculations for Table 2 is ±3%

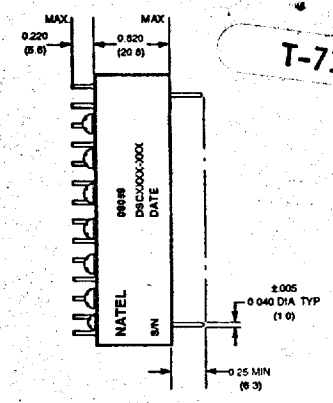
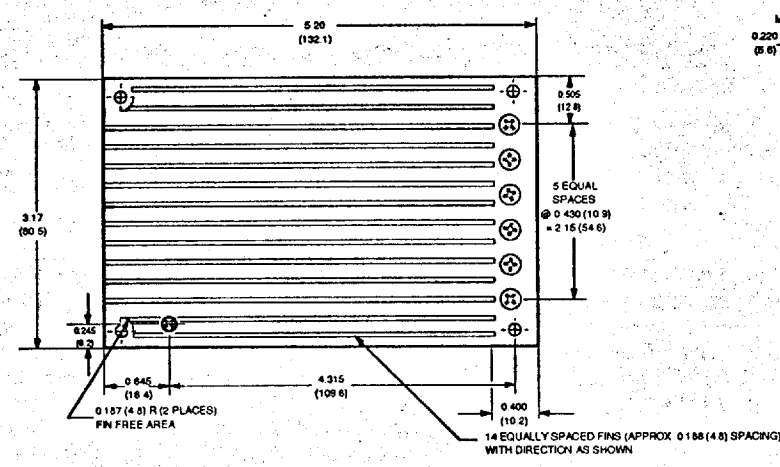
TABLE 2. VA Load on 5206 with TR at "Null"

TR Type	Frequency	Voltage (V _{LL})	Z _{SS} (Nom)	Phase Shift (Maximum)	*VA "Null"
11 TR4c	400	90.0	215.0	6.0°	3.1
15 TRX4a	400	90.0	66.0	5.0°	8.5
18 TRX4a	400	90.0	19.0	4.0°	*24.3
23 TRX4a	400	90.0	7.3	2.0°	*38.3

Voltage imbalance ($\Delta E/V_{LL}$) used in calculations: ±3%.

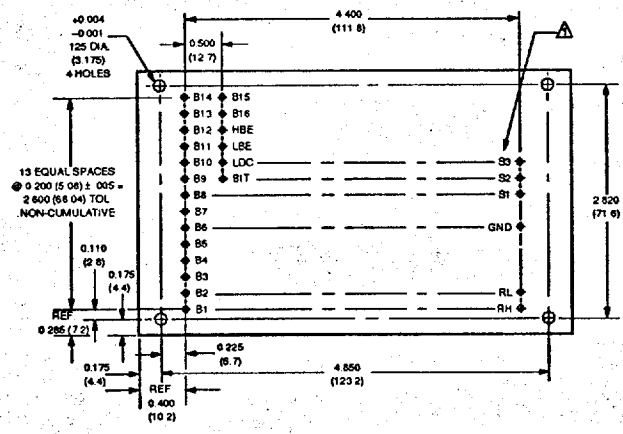
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TOP VIEW



T-71-35-03

BOTTOM VIEW



TOLERANCES:
 .XX = ±0.20 (±.51)
 .XXX = ±0.10 (±.25)

NOTES:
 Dimensions shown in inches and (mm).
 Designations are for reference only and do not appear on part as shown.

MECHANICAL OUTLINE

Ordering Information

DSC5206 - T A M

Temperature Range

1 = 0° C to +70° C
 2 = -40° C to +85° C

MIL Specification

B = MIL-STD-883B
 S = Standard

Accuracy

P = ±8.0 arc-minutes
 S = ±4.0 arc-minutes

Other products available from NATEL

- 3 arc-second accurate, Programmable Dynamic Angle Simulator that includes 4 Related Instruments and is totally A.T.E. Programmable (L200).
- Hybrid (36-pin DDIP size) Synchro(Resolver)-to-Digital converters that operate from a single +5V power supply and offer excellent features such as BIT, AGC, low power dissipation and more (Models 1006, 1056, 1046 and 1044).
- 1.3 arc-minute accuracy, high power, Digital-to-Synchro converters that do not require any DC power supplies (Models 5031 and 5131).
- 1-inch square, single +5V powered, 16-bit R/D converter with built-in Reference Oscillator.
- 2-channel Digital-to-Sin/Cos Converter in a single 36-pin hybrid (HDSC2036).
- 2-speed, 22-Bit Synchro(Resolver)-to-Digital Converter, 0.0004° accuracy in a single 40-pin TDIP (HRD/HSD1626).
- 3-channel Resolver-to-Digital Converter in a single 40-pin TDIP (HRD1346).
- Resolver Control Differential Transmitter in a single 36-pin package (HCDX3106).

A wide range of applications assistance is available from Natel. Application notes can be requested when available . . . and Natel's applications engineers are at your disposal for solving specific problems.

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