

CURRENT MODE PWM CONTROL CIRCUIT

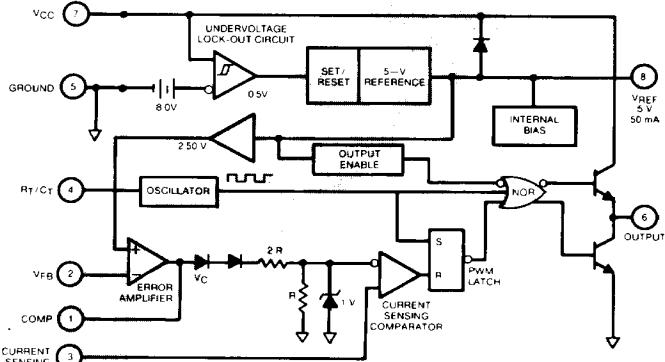
DESCRIPTION

The CS-2841B provides all the necessary features to implement off-line fixed frequency current-mode control with a minimum number of external components.

The CS-2841B is a variation of the CS-2843A designed specifically for use in automotive operation. The low start threshold voltage of typically 8.0V, and the ability to survive 42 volt automotive load dump transients are important for automotive subsystem designs. The CS-2841 series has a history of quality and reliability in automotive applications.

The CS-2841B incorporates a precision temperature-controlled oscillator with an internally trimmed discharge current to minimize variations in frequency. A precision duty-cycle clamp eliminates any need for an external oscillator when at, or near, a 50% duty-cycle condition. Duty-cycles greater than 50% are also possible. Special logic ensures that Vref is stabilized before the output stage is enabled. Ion-implant resistors provide tighter control of undervoltage lockout.

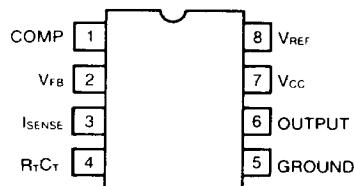
BLOCK DIAGRAM



FEATURES:

- Optimized for off-line control
- Internally trimmed temperature compensated oscillator
- Maximum duty-cycle clamp
- Vref stabilized before output stage is enabled
- Low start-up current
- Pulse-by-pulse current limiting
- Improved U/V lockout
- Double pulse suppression
- 1% trimmed bandgap reference
- High current totem pole output

PIN CONNECTIONS
(TOP VIEW)
DIP



ABSOLUTE MAXIMUM RATINGS

Supply Voltage ($I_{cc} < 30mA$)	Self Limiting	Output Energy (Capacitive Load)	5 μ J
Supply Voltage (Low Impedance Source)	30V	Analog Inputs (Pin 2, Pin 3)	-0.3V to 5.5V
Output Current	$\pm 1A$	Error Amp Output Sink Current	10mA

ELECTRICAL SPECIFICATIONS: Unless otherwise stated, specifications apply for $-40^{\circ}C \leq T_a \leq 85^{\circ}C$
 $R_T=680\Omega$, $C_T=0.22\mu F$ for triangular mode, $R_T=10K$, $C_T=3.3nF$ for sawtooth mode (see Fig. 3)

PARAMETER	TEST CONDITIONS	CS-2841B			UNITS
		MIN.	TYP.	MAX.	

Reference Section

Output Voltage	$T_f=25^{\circ}C$, $I_o=1mA$	4.90	5.00	5.10	V
Line Regulation	$8.4 \leq V_{cc} \leq 16V$		6	20	mV
Load Regulation	$1 \leq I_o \leq 20mA$		6	25	mV
Temp. Stability	(Note 2)		0.2	0.4	mV/ $^{\circ}C$
Total Output Variation	Line, Load, Temp. (Note 2)	4.82		5.18	V
Output Noise Voltage	$10Hz \leq f \leq 10KHz$, $T_f=25^{\circ}C$ (Note 2)		50		μ V
Long Term Stability	$T_A=125^{\circ}C$, 1000 Hrs. (Note 2)		5	25	mV
Output Short Circuit	$T_A=25^{\circ}C$	-30	-100	-180	mA

Oscillator Section

Initial Accuracy	Sawtooth Mode (See Fig. 3) $T_f=25^{\circ}C$	47	52	57	kHz
	Sawtooth Mode: $-40^{\circ}C \leq T_a \leq +85^{\circ}$	44	52	60	kHz
	Triangular Mode (see Fig. 3), $T_f=25^{\circ}C$	44	52	60	kHz
Voltage Stability	$8.4 \leq V_{cc} \leq 16V$		0.2	1	%
	Sawtooth Mode $T_{MIN} \leq T_a \leq T_{MAX}$ (Note 2)		5		%
Temp. Stability	Triangular Mode $T_{MIN} \leq T_a \leq T_{MAX}$ (Note 2)		8		%
	Vospeak to peak		1.7		V
Amplitude	$T_f=25^{\circ}C$	7.4	8.3	9.2	mA
Discharge Current	$T_{MIN} \leq T_a \leq T_{MAX}$	7.2		9.4	mA

Error Amp Section

Input Voltage	$V_{COMP}=2.5V$	2.42	2.50	2.58	V
Input Bias Current	$V_{FB}=0V$		-0.3	-2	μ A
A_{VL}	$2 \leq V_O \leq 4V$	65	90		dB
Unity Gain Bandwidth	(Note 2)	0.7	1		MHz
PSRR	$8.4 \leq V_{cc} \leq 16V$	60	70		dB
Output Sink Current	$V_{FB}=2.7V$, $V_{COMP}=1.1V$	2	6		mA
Output Source Current	$V_{FB}=2.3V$, $V_{COMP}=5V$	-0.5	-0.8		mA
V _{out} High	$V_{FB}=2.3V$, $R_L=15K$ to ground	5	6		V
V _{out} Low	$V_{FB}=2.7V$, $R_L=15K$ to Pin 8		0.7	1.1	V

Current Sense Section

Gain	(Notes 3 & 4)	2.85	3	3.15	V/V
Maximum Input Signal	$V_{COMP}=5V$ (Note 3)	0.9	1	1.1	V
PSRR	$8.4 \leq V_{cc} \leq 16V$ (Note 3)		70		dB
Input Bias Current	$V_{SENSE}=0V$		-2	-10	μ A
Delay to Output	$T_f=25^{\circ}C$ (Note 2)	150	300		ns

Output Section

Output Low Level	$I_{SINK}=20mA$	0.1	0.4	V	
	$I_{SINK}=200mA$	1.5	2.2	V	
Output High Level	$I_{SOURCE}=20mA$	13	13.5	V	
	$I_{SOURCE}=200mA$	12	13.5	V	
Rise Time	$T_f=25^{\circ}C$, $C_L=1nF$ (Note 2)	50	150	ns	
	$T_f=25^{\circ}C$, $C_L=1nF$ (Note 2)	50	150	ns	
Output Leakage	$V_{cc}=14V$, UVLO Active, $V_{PIN\ 6}=0$	-0.01	-10		μ A

Total Standby Current

Start-Up Current		0.5	1	mA
Operating Supply Current	$V_{FB}=V_{SENSE}=0V$ $R_T=10K$, $C_T=3.3nF$	11	17	mA

Notes: 1. Adjust V_{cc} above the start threshold before setting at 15V.
 2. These parameters, although guaranteed, are not 100% tested in production.

3. Parameter measured at trip point of latch with $V_{PIN\ 2}=0$.

4. Gain defined as:

$$A = \frac{\Delta V_{PIN\ 1}}{\Delta V_{PIN\ 3}}, 0 \leq V_{PIN\ 3} \leq 0.8V.$$

ELECTRICAL SPECIFICATIONS

PARAMETER	TEST CONDITIONS	CS-2841B			UNITS
		MIN.	TYP.	MAX.	
Under-Voltage Lockout Section					
Start Threshold		7.6	8.4	V	
Min. Operating Voltage	After Turn On	7.0	7.8	V	

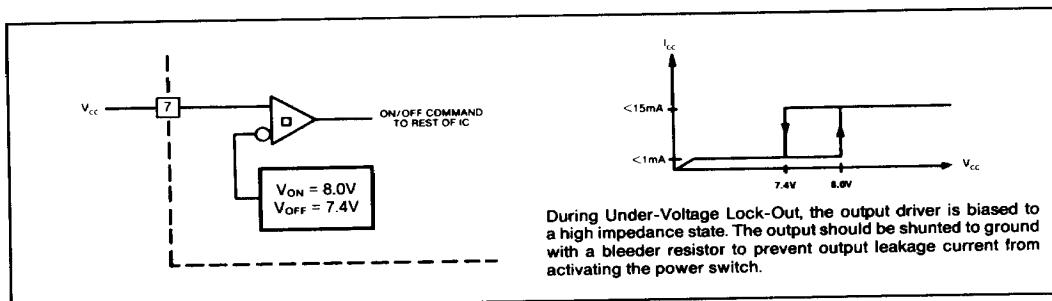


Fig. 1

TIMING DIAGRAM

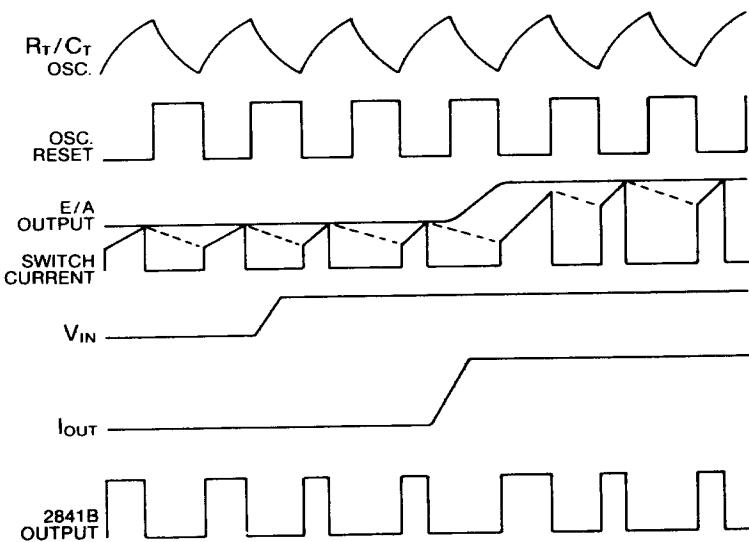


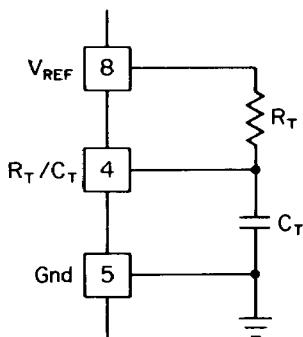
Fig. 2

NOTES ON CS-2841B TIMING DIAGRAM

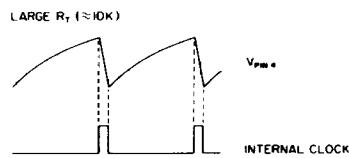
To generate the PWM waveform, the control voltage from the error amplifier is compared to a current sense signal which represents the peak output inductor current. An increase in V_{IN} causes the inductor current slope to increase, thus reducing the duty cycle. This is an inherent feed-forward characteristic of current mode control, since the control voltage does not have to change during changes of input supply voltage.

When the power supply sees a sudden large output current increase, the control voltage will increase allowing the duty cycle to momentarily increase. Since the duty cycle tends to exceed the maximum allowed, to prevent transformer saturation in some power supplies, the internal oscillator waveform provides the maximum duty cycle clamp as programmed by the selection of R_T/C_T components.

APPLICATIONS INFORMATION



Sawtooth Mode



Triangular Mode

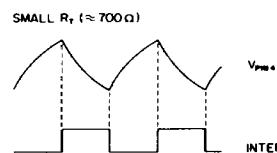
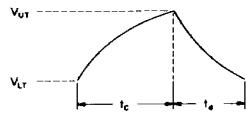


Fig. 3

Oscillator timing capacitor, C_T , is charged by V_{REF} through R_T and discharged by an internal current source. During the discharge time, the internal clock signal blanks out the output to the LO

state, thus providing a user selected maximum duty cycle clamp. Charge and discharge times are determined by the general formulas:



$$t_c = R_T C_T \ln \left(\frac{V_{REF} - V_{LT}}{V_{REF} - V_{UT}} \right)$$

$$t_d = R_T C_T \ln \left(\frac{V_{REF} - I_d R_T - V_{LT}}{V_{REF} - I_d R_T - V_{UT}} \right)$$

Assuming typical values for the parameters in the above formulas:

$$V_{REF}=5.0V, V_{UT}=2.7V, V_{LT}=1.0V, I_d=8.3A, \text{ then}$$

$$t_c \approx .5534 R_T C_T$$

$$t_d \approx R_T C_T \ln \left(\frac{2.3 - 0.0083 R_T}{4.0 - 0.0083 R_T} \right)$$

The frequency and maximum duty cycle can be approximately determined from the following graphs

OSCILLATOR FREQUENCY VS. C_T

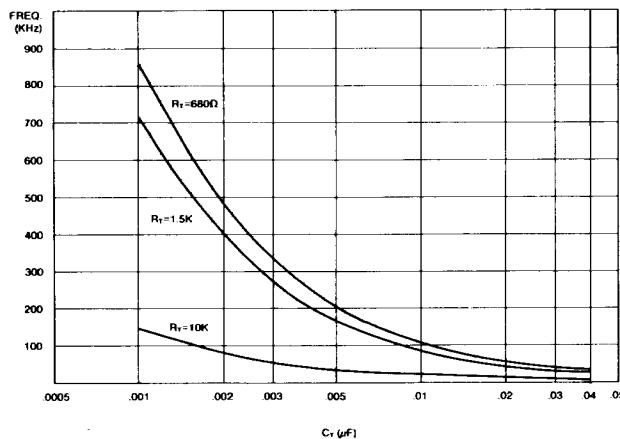


Fig. 4

OSCILLATOR DUTY CYCLE VS. R_T

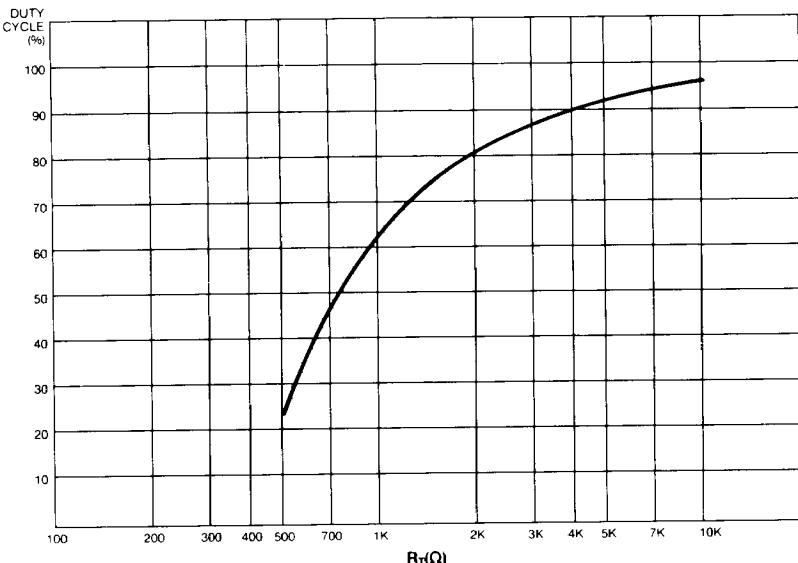
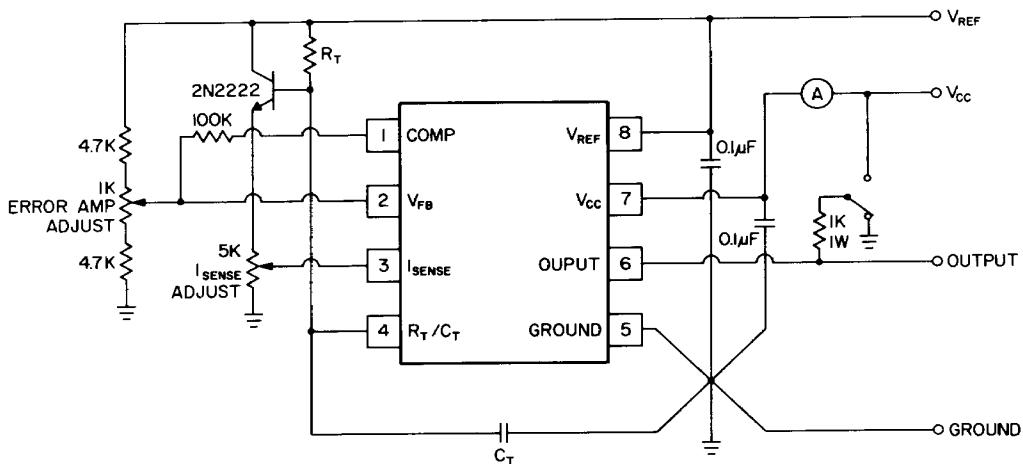


FIG. 5

OPEN-LOOP LABORATORY TEST FIXTURE



High peak currents associated with capacitive loads necessitate careful grounding techniques. Timing and bypass capacitors should be connected close to pin 5 in a single point ground.

The transistor and 5K potentiometer are used to sample the oscillator waveform and apply an adjustable ramp to pin 3.

ORDERING INFORMATION

PART NUMBER	PACKAGE
CS-2841B	8L PDIP