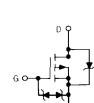
Advance Information

Medium Power Surface Mount Products

TMOS Single P-Channel with Monolithic Zener ESD Protected Gate

EZFETs™ are an advanced series of power MOSFETs which utilize Motorola's High Cell Density TMOS process and contain monolithic back—to—back zener diodes. These zener diodes provide protection against ESD and unexpected transients. These miniature surface mount MOSFETs feature ultra low RDS(on) amd true logic level performance. They are capable of withstanding high energy in the avalanche and commutation modes and the drain—to—source diode has a very low reverse recovery time. EZFET devices are designed for use in low voltage, high speed switching applications where power efficiency is important. Typical applications are dc—dc converters, and power management in portable and battery powered products such as computers, printers, cellular and cordless phones. They can also be used for low voltage motor controls in mass storage products such as disk drives and tape drives.



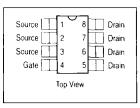
THD

MMSF4P01Z

Motorola Preferred Device

SINGLE TMOS POWER MOSFET 4.0 AMPERES 20 VOLTS RDS(on) = 0.070 OHM





- Zener Protected Gates Provide Electrostatic Discharge Protection
- Ultra Low RDS(on) Provides Higher Efficiency and Extends Battery Life
- Designed to withstand 200V Machine Model and 2000V Human Body Model
- Logic Level Gate Drive Can Be Driven by Logic ICs
- Miniature SO–8 Surface Mount Package Saves Board Space
- Diode Is Characterized for Use In Bridge Circuits
- Diode Exhibits High Speed, With Soft Recovery
- · IDSS Specified at Elevated Temperature
- Mounting Information for SO–8 Package Provided

MAXIMUM RATINGS (T 1 - 25 C unless otherwise noted) *

Rating		Value	Unit
Drain- to Source Voltage	VDSS	20	Vdc
Drain-to-Gate Voltage (R _{GS} = 1.0 MΩ)	V _{DGR}	20	Vdc
Gate -to-Source Voltage - Continuous	V _{GS}	± 8.0	Vdc
Drain Current Continuous @ T _A = 25 C (1) - Continuous @ T _A = 70 C (1) - Pulsed Drain Current (3)	1 _D d Mal	5.7 4.0 46	Adc Apk
Total Power Dissipation @ T _A = 25 C (1) Linear Derating Factor (1)	PD	2.5 20	Watts mW/ C
Total Power Dissipation @ T _A = 25 C (2) Linear Derating Factor (2)	P _D	1.6 12	Watts mW/ C
Operating and Storage Temperature Range	T _J , T _{sta}	- 55 to 150	·C
Thermal Resistance	R _{IJA}	50 80	C/W

^{*} Negative sign for P-Channel omitted for clarity.

(1) When mounted on 1 inch square FR-4 or G-10 board (VGS = 4.5 V, @ 10 Seconds)

(2) When mounted on minimum recommended FR-4 or G-10 board (VGS = 4.5 V. @ Steady State)

(3) Repetitive rating, pulse width limited by maximum junction temperature

DEVICE MARKING

ORDERING INFORMATION

S4P01Z	Device	Reel Size	Tape Width	Quantity	
	MMSF4P01ZR2	13"	12 mm embossed tape	2500 units	
The desired to the second	1 1 0 1				

This document contains information on a new product. Specifications and information are subject to change without notice.

Preferred devices are Motorola recommended choices for future use and best overall value,

REV 1

ELECTRICAL CHARACTERISTICS ($T_C = 25^{\circ}C$ unless otherwise noted)

Characteristic			Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS							
Drain-to-Source Breakdown Volta (VGS = 0 Vdc, I _D = 250 μAdc) Temperature Coefficient (Positiv		(1) (3)	V(BR)DSS	20	— 16.6	<u>-</u>	Vdc mV/°C
Zero Gate Voltage Drain Current (V _{DS} = 12 Vdc, V _{GS} = 0 Vdc) (V _{DS} = 12 Vdc, V _{GS} = 0 Vdc, T _J = 125 C)		loss	1 1	0.05 0.55	2.0 10	μAdc	
Gate-Body Leakage Current (VGS = ± 8.0 Vdc, VDS = 0)		lgss		0.15	5.0	μAdc	
ON CHARACTERISTICS(1)							
Gate Threshold Voltage (VDS = VGS, ID = 250 μAdc) Threshold Temperature Coeffici	(Cpk ≥ 2.0) ent (Negative)	(1) (3)	VGS(th)	0.7	0.85 2.5	1.1	Vdc mV/°C
Static Drain-to-Source On-Resis $(V_{GS} = 4.5 \text{ Vdc}, I_D = 4.0 \text{ Adc})$ $(V_{GS} = 2.7 \text{ Vdc}, I_D = 2.0 \text{ Adc})$	stance (Cpk ≥ 2.0)	(1) (3)	RDS(on)		50 70	70 90	m()
Forward Transconductance (VDS	= 3.0 Vdc, I _D = 2.0 Adc)	(1)	9FS	4.0	7.5	_	Mhos
DYNAMIC CHARACTERISTICS							
Input Capacitance			C _{iss}	-	270	540	pF
Output Capacitance	$V_{DS} = 10 \text{ Vdc}, V_{GS} = 0 \text{ Vol}$ f = 1.0 MHz	dc,	Coss		825	1650	
Transfer Capacitance	1 = 1.0 (W) (2)	C _{rss}	_	100	200	1	
SWITCHING CHARACTERISTICS	(2)						•
Turn-On Delay Time			td(on)	-	150	300	ns
Rise Time	(V _{DD} = 6.0 Vdc, I _D = 4.0 A	(Vnn = 6.0 Vdc. In = 4.0 Adc.		_	800	1600	1 J
Turn-Off Delay Time	$V_{GS} = 4.5 \text{ Vdc}, R_G = 6.0 \Omega$ (1)		td(off)		1420	2840	
Fall Time	7		tf	-	1830	3660	1
Turn-On Delay Time			td(on)	_	260	520	ns
Rise Time	(Vnn = 6.0 Vdc, In = 4.0 A	$(V_{DD} = 6.0 \text{ Vdc. } I_D = 4.0 \text{ Adc.}$ $V_{GS} = 2.7 \text{ Vdc. } R_G = 6.0 \Omega)$ (1)		-	1950	3900	
Turn-Off Delay Time					600	1200	
Fall Time	7		tf	-	1390	2780	1
Gale Charge	(V _{DS} = 10 Vdc, I _D = 4.0 Adc, V _{GS} = 4.5 Vdc) (1)		QT	_	24	34	nC
			Q ₁		3.0		
			Q ₂		11	_	
			Q ₃	_	8.0		
SOURCE-DRAIN DIODE CHARA	CTERISTICS				<u> </u>		
Forward On-Voltage(1)	(1 _S = 4.0 Adc, V _{GS} = 0 Vdc) (1 _S = 4.0 Adc, V _{GS} = 0 Vdc, T _J =	(1) = 125 C)	VSD	-	1.1 0.75	1.8	Vdc
Reverse Recovery Time	(1 _S = 4.0 Adc, V _{GS} = 0 Vdc, d1 _S /dt = 100 A/µs) (1)		¹rr		373		ns
,			ta		750	-	7
			t _b		1120	_	1
Reverse Recovery Storage Charge			QBB	—	9.0		μС

- (1) Pulse Test: Pulse Width : 300 µs. Duty Cycle ≤ 2%.
 (2) Switching characteristics are independent of operating junction temperature.
 (3) Reflects typical values.
 C_{pk} = | Max limit Typ | 3 x SIGMA |

TYPICAL ELECTRICAL CHARACTERISTICS

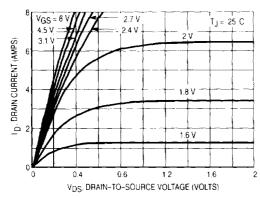


Figure 1. On-Region Characteristics

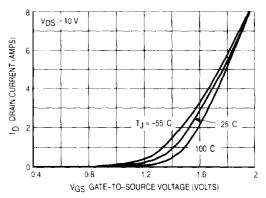


Figure 2. Transfer Characteristics

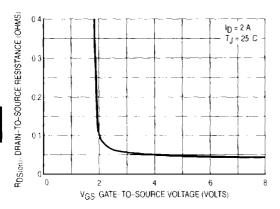


Figure 3. On-Resistance versus Gate-to-Source Voltage

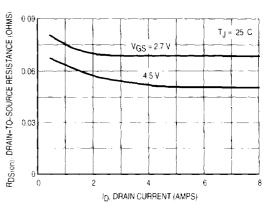


Figure 4. On-Resistance versus Drain Current and Gate Voltage

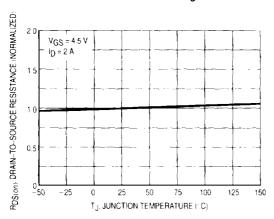


Figure 5. On-Resistance Variation with Temperature

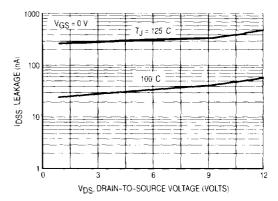


Figure 6. Drain-to-Source Leakage Current versus Voltage

POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain—gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

$$t = Q/I_{G(AV)}$$

During the rise and fall time interval when switching a resistive load, VGS remains virtually constant at a level known as the plateau voltage, VSGP. Therefore, rise and fall times may be approximated by the following:

$$t_r = Q_2 \times R_G/(V_{GG} - V_{GSP})$$

tr = Q2 x RG/VGSP

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_G = the gate drive resistance

and Q2 and VGSP are read from the gate charge curve.

During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

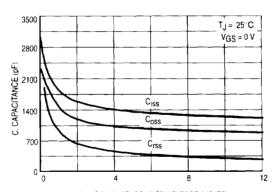
$$t_{d(on)} = R_G C_{iss} In [V_{GG}/(V_{GG} - V_{GSP})]$$

td(off) = RG Ciss In (VGG/VGSP)

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

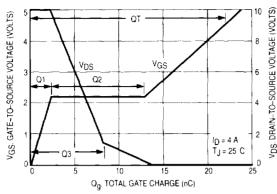
At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

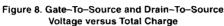
The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



 $V_{\mbox{DS}}$, DRAIN-TO-SOURCE VOLTAGE (VOLTS)

Figure 7. Capacitance Variation





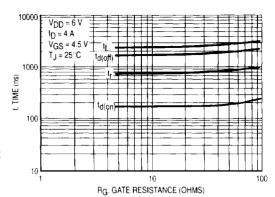


Figure 9. Resistive Switching Time Variation versus Gate Resistance

DRAIN-TO-SOURCE DIODE CHARACTERISTICS

The switching characteristics of a MOSFET body diode are very important in systems using it as a freewheeling or commutating diode. Of particular interest are the reverse recovery characteristics which play a major role in determining switching losses, radiated noise, EMI and RFI.

System switching losses are largely due to the nature of the body diode itself. The body diode is a minority carrier device, therefore it has a finite reverse recovery time, $t_{\rm fr}$, due to the storage of minority carrier charge, Q_{RR} , as shown in the typical reverse recovery wave form of Figure 11. It is this stored charge that, when cleared from the diode, passes through a potential and defines an energy loss. Obviously, repeatedly forcing the diode through reverse recovery further increases switching losses. Therefore, one would like a diode with short $t_{\rm ff}$ and low $Q_{\rm RR}$ specifications to minimize these losses.

The abruptness of diode reverse recovery effects the amount of radiated noise, voltage spikes, and current ringing. The mechanisms at work are finite irremovable circuit parasitic inductances and capacitances acted upon by high

di/dts. The diode's negative di/dt during t_a is directly controlled by the device clearing the stored charge. However, the positive di/dt during t_b is an uncontrollable diode characteristic and is usually the culprit that induces current ringing. Therefore, when comparing diodes, the ratio of t_b/t_a serves as a good indicator of recovery abruptness and thus gives a comparative estimate of probable noise generated. A ratio of 1 is considered ideal and values less than 0.5 are considered snappy

Compared to Motorola standard cell density low voltage MOSFETs, high cell density MOSFET diodes are faster (shorter t_{rr}), have less stored charge and a softer reverse recovery characteristic. The softness advantage of the high cell density diode means they can be forced through reverse recovery at a higher di/dt than a standard cell MOSFET diode without increasing the current ringing or the noise generated. In addition, power dissipation incurred from switching the diode will be less due to the shorter recovery time and lower switching losses.

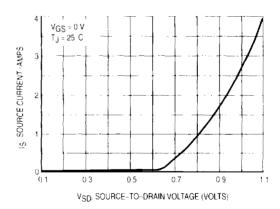


Figure 10. Diode Forward Voltage versus Current

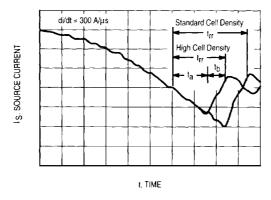


Figure 11. Reverse Recovery Time (trr)

SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance ~ General Data and Its Use."

Switching between the off–state and the on–state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (VDSS) is exceeded, and that the transition time (t_f, t_f) does not exceed 10 μ s. In addition the total power averaged over a complete switching cycle must not exceed (TJ(MAX) = TC)/(R θ JC).

A power MOSFET designated E-FET can be safely used

in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and must be adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E–FETs can withstand the stress of drain-to–source avalanche at currents up to rated pulsed current (IDM), the energy rating is specified at rated continuous current (ID), in accordance with industry custom. The energy rating must be derated for temperature. Maximum energy at currents below rated continuous ID can safely be assumed to equal the values indicated.

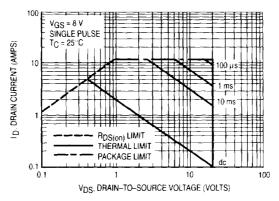


Figure 12. Maximum Rated Forward Biased Safe Operating Area

TYPICAL ELECTRICAL CHARACTERISTICS

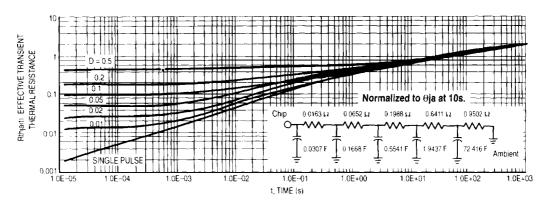


Figure 13. Thermal Response

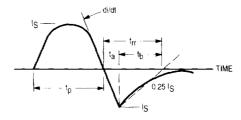


Figure 14. Diode Reverse Recovery Waveform