Serge Juhel

## 1. ABSTRACT

This application note gives a description of a broadband power amplifier operating over the frequency range 88-108 MHz and using the new STMicroelectronics RF MOSFET transistor SD2932.

Table 1: Typical Acheivable Performances

| Device | 1 X SD2932 |
| :--- | :--- |
| Frequency | $88-108 \mathrm{MHz}$ |
| Vdd | 50 V |
| Idq | 200 mA |
| Pout | 300 W |
| Gain | $>19 \mathrm{~dB}$ |
| Input Return Loss | $<-11 \mathrm{~dB}$ |
| Drain Efficiency | $>70 \%$ |

## 2. AMPLIFIER DESIGN.

### 2.1. Input Matching Network.

Typical input gate to gate impedance of SD2932 at 100 MHz is $\mathrm{Zin}=\mathrm{Rs}+\mathrm{jXs}=2-2.6 \mathrm{j}$, and can also be expressed as the combination of parallel resistance and reactance using the following formulae :

$$
\begin{aligned}
& R p=R s \times\left[1+(X s / R s)^{2}\right]=5.38 \text { ohms } \\
& X p=R p /(X s / R s)=-4.14 j \text { ohms }
\end{aligned}
$$

Therefore, in order to achieve good input matching performances over the frequency range $88-108 \mathrm{MHz}$ the unbalanced 50 ohms is to be transformed into an impedance with a value as close as possible to Rp of 5.38 ohms.

From the circuit schematic given in Fig. 6 , we can see that the input matching network is based on a two section balun (1:1 balun in cascade with a 9:1 balun transformer) which will transform the unbalanced 50 ohms to a balanced 5.56 ohms ( $2 \times 2.78$ ohms / 9:1 ratio). The first section, a 5 " long -50 ohms coaxial cable and the second section, a two 3.9" long - 25 ohms flexible coaxial cables with ferrite core NEOSIDE, are connected as described: a 10 nH inductor (L1) is connected between the two gates to compensate SD2932 input parallel reactance Xp. quasi-neutral region of the junction. The breakdown-voltage regime is the avalanching of carriers due to the electric field being greater than the critical electric field (approximately $1 \times 10^{5} \mathrm{~V} / \mathrm{cm}$ ). Under these conditions an electron can be accelerated by the electric field.

Due to elastic and inelastic scattering this electron acceleration can generate more than one carrier and thus a multiplication scheme transpires.

### 2.2. Input Matching Network Tuning.

Figure 1: Input Impedance of 1:1 Balun in Cascade with 4:1 Balun


Figure 2: Input Impedance of 1:1 Balun in Cascade with 9:1 Balun


SD2932 input matching network was tuned in order to achieve the best compromise in terms of power gain (Gp) and input return loss (Rtl) over the frequency range $88-108 \mathrm{MHz}$. Best results were achieved by adding a 10 pF chip capacitor (C1) between RFIN and the 1 nF blocking capacitor (C2).

### 2.3. Output Matching Network.

The output impedance of each side is a combination of the output capacitance $\mathrm{C}_{\text {oss }}(195 \mathrm{pF})$ and the optimum load resistance which can be determined as follows :

$$
R p=(0.85 \times V d d)^{2} /(2 \times \text { Pout })=(0.85 \times 50 \mathrm{~V}) /(2 \times 150 \mathrm{~W})=6.02 \text { ohms }
$$

The total optimum load, seen by SD2932 (drain to drain), is $2 \times 6.02=12.04$ ohms. Therefore, a simple two section balun ( $1: 1$ balun in cascade with a $4: 1$ balun transformer) is used to transform the unbalanced 50 ohms to a balanced 12.5 ohms ( $2 \times 6.25$ ohms) which is very near to the total optimum load resistance.

The first section, a 5" long - 50 ohms flexible coaxial cable, and the second section, two 5 " long - 25 ohms flexible coaxial cables, are connected as described in figure 6.
To compensate for the output capacitance $\mathrm{C}_{\text {oss }}$ of SD2932, a 40 nH inductor (L2) is connected between the two drains. This LC network ( $L 2 \& C_{o s s}$ ) is a high pass filter with a resonance frequency calculated at $10 \%$ below the minimum operating frequency :
$\mathrm{C}_{\text {oss }}=\mathrm{C}_{\text {oss }}($ per side $) / 2=180 \mathrm{pF} / 2=90 \mathrm{pF}$
Frequency of resonance $=0.9 \times 88 \mathrm{MHz}=80 \mathrm{MHz}$
L2 $x$ Coss $(2 p f)^{2}=1--->L 2=44 n H$.

Figure 3: Power Gain vs. Frequency


Figure 4: Drain Efficiency vs. Frequency
$\square$

Figure 5: Input Return Loss vs. Frequency


## 3. MEASURED SD2932 TYPICAL PERFORMANCES AND CONCLUSION.

Figures $3,4 \& 5$ show power gain, efficiency and input return loss over the frequency range 88-108 MHz at a constant output power of 300 Watts and a drain supply voltage of 50 Volts and a quiescent current of 200 mA . Typical performances are as follows:

Table 2.

|  | MIN | MAX |
| :--- | :--- | :--- |
| $G p$ | 19.3 dB | 19.6 dB |
| $\mathrm{R}_{\mathrm{TL}}$ | -18 dB | -11 dB |
| Eff | $71 \%$ | $73 \%$ |

Finally, in this report we have demonstrated ST SD2932 MOSFET transistor excellent performance as a wide band $300 \mathrm{~W}-50 \mathrm{~V}$ push-pull amplifier for FM applications.

Figure 6: 88-108MHz Circuit Schematic


Table 3: 88-108MHz Circuit Components List

| PCB | 1/32" Woven Fiberglass $0.0030 \mathrm{Cu}, 2$ side, $\varepsilon_{r}=4.8$ |
| :---: | :---: |
| T1 | 50 Ohm Flexible Coax Cable OD 0.006", 5" Long |
| T2/ T3 | 9:1 Transformer, 25 Ohm Flexible Coax Cable OD 0.1" 3.9". Ferrite Core NEOSIDE |
| T4/ T5 | 4:1 Transformer, 25 Ohm Flexible Coax Cable OD 0.1" 5.0" Long. |
| T6 | 50 Ohm Flexible Coax Cable OD 0.1" 5.0" Long. |
| FB1 | VK200 |
| C1 | 10pf Ceramic Capacitor |
| C2/C3/C4/C7/C8 | 1 nF Chip Capacitor |
| C5/C6 | 1 nF ATC chip Capacitor |
| C9 | 470 pF ATC Chip Capacitor |
| C10 | 100 nF Chip Capacitor |
| R1 | 56 Ohm Resistor |
| R2/R4 | 10 Ohm Chip Resistor |
| R3 | 10K Ohm Resistor |
| R5 | 5.6K Ohm Resistor |
| R6 | 10K Ohm. 10 Turn Trim Resistor |
| R7 | 3.3K Ohm/ 1 W Resistor |
| R8 | $15 \mathrm{Ohm} / 1 \mathrm{~W}$ Resistor |
| D1 | 6.8 V Zener Diode |
| L1 | 10 nH Inductor |
| L2 | 40 nH Inductor |
| L3 | 70 nH Inductor |

Information furnished is believed to be accurate and reliable. However, STMicroelectronics assumes no responsibility for the consequences of use of such information nor for any infringement of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of STMicroelectronics. Specification mentioned in this publication are subject to change without notice. This publication supersedes and replaces all information previously supplied. STMicroelectronics products are not authorized for use as critical components in life support devices or systems without express written approval of STMicroelectronics.

The ST logo is a trademark of STMicroelectronics
© 2000 STMicroelectronics - Printed in Italy - All rights reserved

STMicroelectronics GROUP OF COMPANIES
Australia - Brazil - China - Finland - France - Germany - Hong Kong - India - Italy - Japan - Malaysia - Malta - Morocco Singapore - Spain - Sweden - Switzerland - United Kingdom - U.S.A.
http://www.st.com

