


# 325MHz, Single/Dual, Rail-to-Rail Input and Output, Low Distortion, Low Noise Precision Op Amps

## FEATURES

- Gain Bandwidth Product: 325MHz
- Slew Rate: 140V/ $\mu$ s
- Wide Supply Range: 2.5V to 12.6V
- Large Output Current: 85mA
- Low Distortion, 5MHz: -80dBc
- Low Voltage Noise: 3.5nV/ $\sqrt{\text{Hz}}$
- Input Common Mode Range Includes Both Rails
- Output Swings Rail-to-Rail
- Input Offset Voltage (Rail-to-Rail): 550 $\mu$ V Max
- Common Mode Rejection: 106dB Typ
- Power Supply Rejection: 105dB Typ
- Unity-Gain Stable
- Power Down Pin (LT1806)
- Single in SO-8 and 6-Pin SOT-23 Packages
- Dual in SO-8 and 8-Pin MSOP Packages
- Operating Temperature Range: -40°C to 85°C

## APPLICATIONS

- Low Voltage, High Frequency Signal Processing
- Driving A/D Converters
- Rail-to-Rail Buffer Amplifiers
- Active Filters
- Video Line Driver

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## DESCRIPTION

The LT<sup>®</sup>1806/LT1807 are single/dual low noise rail-to-rail input and output unity-gain stable op amps that feature a 325MHz gain-bandwidth product, a 140V/ $\mu$ s slew rate and a 85mA output current. They are optimized for low voltage, high performance signal conditioning systems.

The LT1806/LT1807 have a very low distortion of -80dBc at 5MHz, a low input referred noise voltage of 3.5nV/ $\sqrt{\text{Hz}}$  and a maximum offset voltage of 550 $\mu$ V that allows them to be used in high performance data acquisition systems.

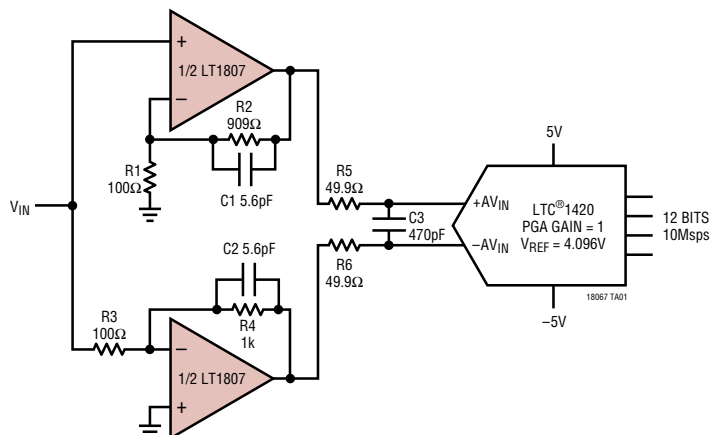
The LT1806/LT1807 have an input range that includes both supply rails and an output that swings within 20mV of either supply rail to maximize the signal dynamic range in low supply applications.

The LT1806/LT1807 maintain their performance for supplies from 2.5V to 12.6V and are specified at 3V, 5V and  $\pm$ 5V supplies. The inputs can be driven beyond the supplies without damage or phase reversal of the output.

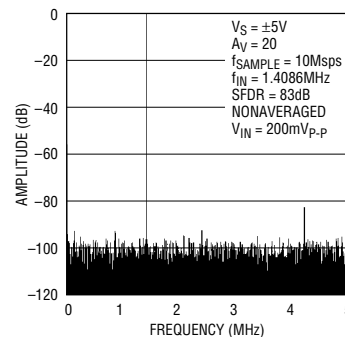
The LT1806 is available in an 8-pin SO package with the standard op amp pinout and a 6-pin SOT-23 package. The LT1807 features the standard dual op amp pinout and is available in 8-pin SO and MSOP packages. These devices can be used as plug-in replacements for many op amps to improve input/output range and performance.

## TYPICAL APPLICATION

Gain of 20 Differential A/D Driver



4096 Point FFT Response

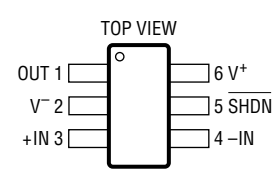
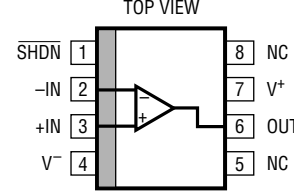
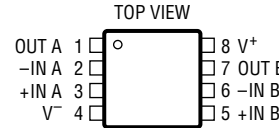
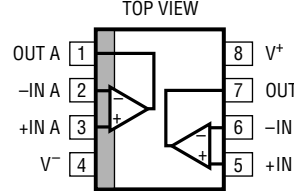


# LT1806/LT1807

## ABSOLUTE MAXIMUM RATINGS (Note 1)

Total Supply Voltage ( $V^+$ to $V^-$ ) .....	12.6V	Specified Temperature Range (Note 5) ...	$-40^{\circ}\text{C}$ to $85^{\circ}\text{C}$
Input Voltage (Note 2) .....	$\pm V_S$	Junction Temperature .....	$150^{\circ}\text{C}$
Input Current (Note 2) .....	$\pm 10\text{mA}$	Storage Temperature Range .....	$-65^{\circ}\text{C}$ to $150^{\circ}\text{C}$
Output Short-Circuit Duration (Note 3) .....	Indefinite	Lead Temperature (Soldering, 10 sec) .....	$300^{\circ}\text{C}$
Operating Temperature Range (Note 4) ..	$-40^{\circ}\text{C}$ to $85^{\circ}\text{C}$		

## PACKAGE/ORDER INFORMATION

 <p>S6 PACKAGE 6-LEAD PLASTIC SOT-23 <math>T_{JMAX} = 150^{\circ}\text{C}</math>, <math>\theta_{JA} = 160^{\circ}\text{C/W}</math> (Note 9)</p>	ORDER PART NUMBER	 <p>S8 PACKAGE 8-LEAD PLASTIC SO <math>T_{JMAX} = 150^{\circ}\text{C}</math>, <math>\theta_{JA} = 100^{\circ}\text{C/W}</math> (Note 9)</p>	ORDER PART NUMBER
	LT1806CS6 LT1806IS6		LT1806CS8 LT1806IS8
	S6 PART MARKING		S8 PART MARKING
	LTNK LTNL		1806 1806I
 <p>MS8 PACKAGE 8-LEAD PLASTIC MSOP <math>T_{JMAX} = 150^{\circ}\text{C}</math>, <math>\theta_{JA} = 135^{\circ}\text{C/W}</math> (Note 9)</p>	ORDER PART NUMBER	 <p>S8 PACKAGE 8-LEAD PLASTIC SO <math>T_{JMAX} = 150^{\circ}\text{C}</math>, <math>\theta_{JA} = 100^{\circ}\text{C/W}</math> (Note 9)</p>	ORDER PART NUMBER
	LT1807CMS8 LT1807IMS8		LT1807CS8 LT1807IS8
	MS8 PART MARKING		S8 PART MARKING
	LTTT LTTV		1807 1807I

Consult factory for parts specified with wider operating temperature ranges.

## ELECTRICAL CHARACTERISTICS

$T_A = 25^{\circ}\text{C}$ .  $V_S = 5\text{V}$ ,  $0\text{V}$ ;  $V_S = 3\text{V}$ ,  $0\text{V}$ ;  $V_{SHDN} = \text{open}$ ;  $V_{CM} = V_{OUT} = \text{half supply}$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
$V_{OS}$	Input Offset Voltage	$V_{CM} = V^+$		100	550	$\mu\text{V}$
		$V_{CM} = V^-$		100	550	$\mu\text{V}$
		$V_{CM} = V^+$ (LT1806 SOT-23)		100	700	$\mu\text{V}$
		$V_{CM} = V^-$ (LT1806 SOT-23)		100	700	$\mu\text{V}$
$\Delta V_{OS}$	Input Offset Voltage Shift	$V_{CM} = V^-$ to $V^+$		50	550	$\mu\text{V}$
		$V_{CM} = V^-$ to $V^+$ (LT1806 SOT-23)		100	700	$\mu\text{V}$
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	$V_{CM} = V^-$ to $V^+$		200	1000	$\mu\text{V}$
$I_B$	Input Bias Current	$V_{CM} = V^+$		1	4	$\mu\text{A}$
		$V_{CM} = V^- + 0.2\text{V}$	-13	-5		$\mu\text{A}$
$\Delta I_B$	Input Bias Current Shift	$V_{CM} = V^-$ to $V^+$		6	17	$\mu\text{A}$
		Input Bias Current Match (Channel-to-Channel) (Note 10)	$V_{CM} = V^+$	0.03	1.2	$\mu\text{A}$
		$V_{CM} = V^- + 0.2\text{V}$		0.05	3.0	$\mu\text{A}$

## ELECTRICAL CHARACTERISTICS

T<sub>A</sub> = 25°C. V<sub>S</sub> = 5V, 0V; V<sub>S</sub> = 3V, 0V; V<sub>SHDN</sub> = open; V<sub>CM</sub> = V<sub>OUT</sub> = half supply unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
I <sub>OS</sub>	Input Offset Current	V <sub>CM</sub> = V <sup>+</sup> V <sub>CM</sub> = V <sup>-</sup> + 0.2V		0.03 0.05	0.6 1.5	μA μA
ΔI <sub>OS</sub>	Input Offset Current Shift	V <sub>CM</sub> = V <sup>-</sup> + 0.2V to V <sup>+</sup>		0.08	2.1	μA
	Input Noise Voltage	0.1Hz to 10Hz		800		nV <sub>P-P</sub>
e <sub>n</sub>	Input Noise Voltage Density	f = 10kHz		3.5		nV/√Hz
i <sub>n</sub>	Input Noise Current Density	f = 10kHz		1.5		pA/√Hz
C <sub>IN</sub>	Input Capacitance			2		pF
A <sub>VOL</sub>	Large-Signal Voltage Gain	V <sub>S</sub> = 5V, V <sub>O</sub> = 0.5V to 4.5V, R <sub>L</sub> = 1k to V <sub>S</sub> /2 V <sub>S</sub> = 5V, V <sub>O</sub> = 1V to 4V, R <sub>L</sub> = 100 to V <sub>S</sub> /2 V <sub>S</sub> = 3V, V <sub>O</sub> = 0.5V to 2.5V, R <sub>L</sub> = 1k to V <sub>S</sub> /2	75 9 60	220 22 150		V/mV V/mV V/mV
CMRR	Common Mode Rejection Ratio	V <sub>S</sub> = 5V, V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup> V <sub>S</sub> = 3V, V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup>	79 74	100 95		dB dB
	CMRR Match (Channel-to-Channel) (Note 10)	V <sub>S</sub> = 5V, V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup> V <sub>S</sub> = 3V, V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup>	73 68	100 95		dB dB
	Input Common Mode Range		V <sup>-</sup>		V <sup>+</sup>	V
PSRR	Power Supply Rejection Ratio	V <sub>S</sub> = 2.5V to 10V, V <sub>CM</sub> = 0V	90	105		dB
	PSRR Match (Channel-to-Channel) (Note 10)	V <sub>S</sub> = 2.5V to 10V, V <sub>CM</sub> = 0V	84	105		dB
	Minimum Supply Voltage (Note 6)			2.3	2.5	V
V <sub>OL</sub>	Output Voltage Swing LOW (Note 7)	No Load I <sub>SINK</sub> = 5mA I <sub>SINK</sub> = 25mA		8 50 170	50 130 375	mV mV mV
V <sub>OH</sub>	Output Voltage Swing HIGH (Note 7)	No Load I <sub>SOURCE</sub> = 5mA I <sub>SOURCE</sub> = 25mA		15 85 350	65 180 650	mV mV mV
I <sub>SC</sub>	Short-Circuit Current	V <sub>S</sub> = 5V V <sub>S</sub> = 3V	±35 ±30	±85 ±65		mA mA
I <sub>S</sub>	Supply Current per Amplifier			9	13	mA
	Disable Supply Current	V <sub>S</sub> = 5V, V <sub>SHDN</sub> = 0.3V V <sub>S</sub> = 3V, V <sub>SHDN</sub> = 0.3V		0.40 0.22	0.9 0.7	mA mA
I <sub>SHDN</sub>	SHDN Pin Current	V <sub>S</sub> = 5V, V <sub>SHDN</sub> = 0.3V V <sub>S</sub> = 3V, V <sub>SHDN</sub> = 0.3V		150 100	350 300	μA μA
	Shutdown Output Leakage Current	V <sub>SHDN</sub> = 0.3V		0.1	75	μA
V <sub>L</sub>	SHDN Pin Input Voltage LOW				0.3	V
V <sub>H</sub>	SHDN Pin Input Voltage HIGH		V <sup>+</sup> - 0.5			V
t <sub>ON</sub>	Turn-On Time	V <sub>SHDN</sub> = 0.3V to 4.5V, R <sub>L</sub> = 100Ω		80		ns
t <sub>OFF</sub>	Turn-Off Time	V <sub>SHDN</sub> = 4.5V to 0.3V, R <sub>L</sub> = 100Ω		50		ns
GBW	Gain Bandwidth Product	Frequency = 6MHz		325		MHz
SR	Slew Rate	V <sub>S</sub> = 5V, A <sub>V</sub> = -1, R <sub>L</sub> = 1k, V <sub>O</sub> = 4V		125		V/μs
FPBW	Full Power Bandwidth	V <sub>S</sub> = 5V, V <sub>OUT</sub> = 4V <sub>P-P</sub>		10		MHz
HD	Harmonic Distortion	V <sub>S</sub> = 5V, A <sub>V</sub> = 1, R <sub>L</sub> = 1k, V <sub>O</sub> = 2V <sub>P-P</sub> , f <sub>C</sub> = 5MHz		-78		dBc
t <sub>S</sub>	Settling Time	0.01%, V <sub>S</sub> = 5V, V <sub>STEP</sub> = 2V, A <sub>V</sub> = 1, R <sub>L</sub> = 1k		60		ns
ΔG	Differential Gain (NTSC)	V <sub>S</sub> = 5V, A <sub>V</sub> = 2, R <sub>L</sub> = 150		0.015		%
Δθ	Differential Phase (NTSC)	V <sub>S</sub> = 5V, A <sub>V</sub> = 2, R <sub>L</sub> = 150		0.05		Deg

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the  $0^{\circ}\text{C} < T_A < 70^{\circ}\text{C}$  temperature range.  $V_S = 5\text{V}, 0\text{V}; V_S = 3\text{V}, 0\text{V}; V_{\text{SHDN}} = \text{open}; V_{\text{CM}} = V_{\text{OUT}} = \text{half supply, unless otherwise noted.}$

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
$V_{\text{OS}}$	Input Offset Voltage	$V_{\text{CM}} = V^+$	●	200	700	$\mu\text{V}$
		$V_{\text{CM}} = V^-$	●	200	700	$\mu\text{V}$
		$V_{\text{CM}} = V^+$ (LT1806 SOT-23)	●	200	850	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ (LT1806 SOT-23)	●	200	850	$\mu\text{V}$
$V_{\text{OS TC}}$	Input Offset Voltage Drift (Note 8)	$V_{\text{CM}} = V^+$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
		$V_{\text{CM}} = V^-$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
$\Delta V_{\text{OS}}$	Input Offset Voltage Shift	$V_{\text{CM}} = V^- \text{ to } V^+$	●	100	700	$\mu\text{V}$
		$V_{\text{CM}} = V^- \text{ to } V^+$ (LT1806 SOT-23)	●	100	850	$\mu\text{V}$
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^-, V_{\text{CM}} = V^+$	●	300	1200	$\mu\text{V}$
$I_{\text{B}}$	Input Bias Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	1	5	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	-15	-5	$\mu\text{A}$
$\Delta I_{\text{B}}$	Input Bias Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V} \text{ to } V^+ - 0.2\text{V}$	●	6	20	$\mu\text{A}$
		Input Bias Current Match (Channel-to-Channel) (Note 10)	●	0.03	1.5	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.05	3.5	$\mu\text{A}$
$I_{\text{OS}}$	Input Offset Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	0.03	0.75	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.05	1.80	$\mu\text{A}$
$\Delta I_{\text{OS}}$	Input Offset Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V} \text{ to } V^+ - 0.2\text{V}$	●	0.08	2.55	$\mu\text{A}$
$A_{\text{VOL}}$	Large-Signal Voltage Gain	$V_S = 5\text{V}, V_O = 0.5\text{V} \text{ to } 4.5\text{V}, R_L = 1\text{k} \text{ to } V_S/2$	●	60	175	V/mV
		$V_S = 5\text{V}, V_O = 1\text{V} \text{ to } 4\text{V}, R_L = 100\Omega \text{ to } V_S/2$	●	7.5	20	V/mV
		$V_S = 3\text{V}, V_O = 0.5\text{V} \text{ to } 2.5\text{V}, R_L = 1\text{k} \text{ to } V_S/2$	●	45	140	V/mV
CMRR	Common Mode Rejection Ratio	$V_S = 5\text{V}, V_{\text{CM}} = V^- \text{ to } V^+$	●	77	94	dB
		$V_S = 3\text{V}, V_{\text{CM}} = V^- \text{ to } V^+$	●	72	89	dB
	CMRR Match (Channel-to-Channel) (Note 10)	$V_S = 5\text{V}, V_{\text{CM}} = V^- \text{ to } V^+$	●	71	94	dB
		$V_S = 3\text{V}, V_{\text{CM}} = V^- \text{ to } V^+$	●	66	89	dB
	Input Common Mode Range		●	$V^-$	$V^+$	V
PSRR	Power Supply Rejection Ratio	$V_S = 2.5\text{V} \text{ to } 10\text{V}, V_{\text{CM}} = 0\text{V}$	●	88	105	dB
		PSRR Match (Channel-to-Channel) (Note 10)	●	82	105	dB
	Minimum Supply Voltage (Note 6)	$V_{\text{CM}} = V_O = 0.5\text{V}$	●	2.3	2.5	V
$V_{\text{OL}}$	Output Voltage Swing LOW (Note 7)	No Load	●	12	60	mV
		$I_{\text{SINK}} = 5\text{mA}$	●	60	140	mV
		$I_{\text{SINK}} = 25\text{mA}$	●	180	425	mV
$V_{\text{OH}}$	Output Voltage Swing HIGH (Note 7)	No Load	●	30	120	mV
		$I_{\text{SOURCE}} = 5\text{mA}$	●	110	220	mV
		$I_{\text{SOURCE}} = 25\text{mA}$	●	360	700	mV
$I_{\text{SC}}$	Short-Circuit Current	$V_S = 5\text{V}$	●	$\pm 30$	$\pm 65$	mA
		$V_S = 3\text{V}$	●	$\pm 25$	$\pm 55$	mA
$I_{\text{S}}$	Supply Current per Amplifier		●	10	14	mA
		Disable Supply Current	$V_S = 5\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	0.40	1.1
		$V_S = 3\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	0.22	0.9	mA
$I_{\text{SHDN}}$	$\overline{\text{SHDN}}$ Pin Current	$V_S = 5\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	160	400	$\mu\text{A}$
		$V_S = 3\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	110	350	$\mu\text{A}$
	Shutdown Output Leakage Current	$V_{\text{SHDN}} = 0.3\text{V}$	●	1		$\mu\text{A}$
$V_{\text{L}}$	$\overline{\text{SHDN}}$ Pin Input Voltage LOW		●		0.3	V
$V_{\text{H}}$	$\overline{\text{SHDN}}$ Pin Input Voltage HIGH		●	$V^+ - 0.5$		V
$t_{\text{ON}}$	Turn-On Time	$V_{\text{SHDN}} = 0.3\text{V} \text{ to } 4.5\text{V}, R_L = 100\Omega$	●	80		ns
$t_{\text{OFF}}$	Turn-Off Time	$V_{\text{SHDN}} = 4.5\text{V} \text{ to } 0.3\text{V}, R_L = 100\Omega$	●	50		ns
GBW	Gain Bandwidth Product	Frequency = 6MHz	●	300		MHz
SR	Slew Rate	$V_S = 5\text{V}, A_V = -1, R_L = 1\text{k}, V_O = 4\text{V}$	●	100		V/ $\mu\text{s}$
FPBW	Full Power Bandwidth	$V_S = 5\text{V}, V_O = 4V_{\text{P-P}}$	●	8		MHz

**ELECTRICAL CHARACTERISTICS** The ● denotes the specifications which apply over the  $-40^{\circ}\text{C} < T_A < 85^{\circ}\text{C}$  temperature range.  $V_S = 5\text{V}, 0\text{V}; V_S = 3\text{V}, 0\text{V}; V_{\text{SHDN}} = \text{open}; V_{\text{CM}} = V_{\text{OUT}} = \text{half supply, unless otherwise noted. (Note 5)}$

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
$V_{\text{OS}}$	Input Offset Voltage	$V_{\text{CM}} = V^+$	●	200	800	$\mu\text{V}$
		$V_{\text{CM}} = V^-$	●	200	800	$\mu\text{V}$
		$V_{\text{CM}} = V^+$ (LT1806 SOT-23)	●	200	950	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ (LT1806 SOT-23)	●	200	950	$\mu\text{V}$
$V_{\text{OS TC}}$	Input Offset Voltage Drift (Note 8)	$V_{\text{CM}} = V^+$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
		$V_{\text{CM}} = V^-$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
$\Delta V_{\text{OS}}$	Input Offset Voltage Shift	$V_{\text{CM}} = V^-$	●	100	800	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ to $V^+$ (LT1806 SOT-23)	●	100	950	$\mu\text{V}$
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^+, V_{\text{CM}} = V^-$	●	200	1400	$\mu\text{V}$
$I_B$	Input Bias Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	1	6	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	-16	-5	$\mu\text{A}$
$\Delta I_B$	Input Bias Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V}$ to $V^+ - 0.2\text{V}$	●	6	22	$\mu\text{A}$
		Input Bias Current Match (Channel-to-Channel) (Note 10)	●	0.02	1.8	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.05	4.0	$\mu\text{A}$
$I_{\text{OS}}$	Input Offset Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	0.02	0.9	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.05	2.1	$\mu\text{A}$
$\Delta I_{\text{OS}}$	Input Offset Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V}$ to $V^+ - 0.2\text{V}$	●	0.07	3	$\mu\text{A}$
$A_{\text{VOL}}$	Large-Signal Voltage Gain	$V_S = 5\text{V}, V_O = 0.5\text{V}$ to $4.5\text{V}, R_L = 1\text{k}$ to $V_S/2$	●	50	140	$\text{V}/\text{mV}$
		$V_S = 5\text{V}, V_O = 1\text{V}$ to $4\text{V}, R_L = 100\Omega$ to $V_S/2$	●	6	16	$\text{V}/\text{mV}$
		$V_S = 3\text{V}, V_O = 0.5\text{V}$ to $2.5\text{V}, R_L = 1\text{k}$ to $V_S/2$	●	35	100	$\text{V}/\text{mV}$
CMRR	Common Mode Rejection Ratio	$V_S = 5\text{V}, V_{\text{CM}} = V^-$ to $V^+$	●	75	94	$\text{dB}$
		$V_S = 3\text{V}, V_{\text{CM}} = V^-$ to $V^+$	●	71	89	$\text{dB}$
	CMRR Match (Channel-to-Channel) (Note 10)	●	69	94	$\text{dB}$	
		$V_S = 3\text{V}, V_{\text{CM}} = V^-$ to $V^+$	●	65	89	$\text{dB}$
	Input Common Mode Range		●	$V^-$	$V^+$	$\text{V}$
PSRR	Power Supply Rejection Ratio	$V_S = 2.5\text{V}$ to $10\text{V}, V_{\text{CM}} = 0\text{V}$	●	86	105	$\text{dB}$
		PSRR Match (Channel-to-Channel) (Note 10)	●	80	105	$\text{dB}$
	Minimum Supply Voltage (Note 6)	$V_{\text{CM}} = V_O = 0.5\text{V}$	●	2.3	2.5	$\text{V}$
$V_{\text{OL}}$	Output Voltage Swing LOW (Note 7)	No Load	●	15	70	$\text{mV}$
		$I_{\text{SINK}} = 5\text{mA}$	●	65	150	$\text{mV}$
		$I_{\text{SINK}} = 20\text{mA}$	●	170	400	$\text{mV}$
$V_{\text{OH}}$	Output Voltage Swing HIGH (Note 7)	No Load	●	30	130	$\text{mV}$
		$I_{\text{SOURCE}} = 5\text{mA}$	●	110	240	$\text{mV}$
		$I_{\text{SOURCE}} = 20\text{mA}$	●	350	700	$\text{mV}$
$I_{\text{SC}}$	Short-Circuit Current	$V_S = 5\text{V}$	●	$\pm 22$	$\pm 45$	$\text{mA}$
		$V_S = 3\text{V}$	●	$\pm 20$	$\pm 40$	$\text{mA}$
$I_S$	Supply Current per Amplifier		●	11	16	$\text{mA}$
		Disable Supply Current	●	0.4	1.2	$\text{mA}$
		$V_S = 5\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	0.3	1.0	$\text{mA}$
$I_{\text{SHDN}}$	$\overline{\text{SHDN}}$ Pin Current	$V_S = 5\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	170	450	$\mu\text{A}$
		$V_S = 3\text{V}, V_{\text{SHDN}} = 0.3\text{V}$	●	120	400	$\mu\text{A}$
	Shutdown Output Leakage Current	$V_{\text{SHDN}} = 0.3\text{V}$	●	1.2		$\mu\text{A}$
$V_L$	$\overline{\text{SHDN}}$ Pin Input Voltage LOW		●		0.3	$\text{V}$
$V_H$	$\overline{\text{SHDN}}$ Pin Input Voltage HIGH		●	$V^+ - 0.5$		$\text{V}$
$t_{\text{ON}}$	Turn-On Time	$V_{\text{SHDN}} = 0.3\text{V}$ to $4.5\text{V}, R_L = 100\Omega$	●	80		$\text{ns}$
$t_{\text{OFF}}$	Turn-Off Time	$V_{\text{SHDN}} = 4.5\text{V}$ to $0.3\text{V}, R_L = 100\Omega$	●	50		$\text{ns}$
GBW	Gain Bandwidth Product	Frequency = $6\text{MHz}$	●	250		$\text{MHz}$
SR	Slew Rate	$V_S = 5\text{V}, A_V = -1, R_L = 1\text{k}, V_O = 4\text{V}$	●	80		$\text{V}/\mu\text{V}$
FPBW	Full Power Bandwidth	$V_S = 5\text{V}, V_O = 4\text{V}_{\text{P-P}}$	●	6		$\text{MHz}$

# LT1806/LT1807

## ELECTRICAL CHARACTERISTICS

$T_A = 25^\circ\text{C}$ .  $V_S = \pm 5\text{V}$ ,  $V_{\text{SHDN}} = \text{open}$ ;  $V_{\text{CM}} = 0\text{V}$ ,  $V_{\text{OUT}} = 0\text{V}$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
$V_{\text{OS}}$	Input Offset Voltage	$V_{\text{CM}} = V^+$		100	700	$\mu\text{V}$
		$V_{\text{CM}} = V^-$		100	700	$\mu\text{V}$
		$V_{\text{CM}} = V^+$ (LT1806 SOT-23)		100	750	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ (LT1806 SOT-23)		100	750	$\mu\text{V}$
$\Delta V_{\text{OS}}$	Input Offset Voltage Shift	$V_{\text{CM}} = V^-$ to $V^+$		50	700	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ to $V^+$ (LT1806 SOT-23)		50	750	$\mu\text{V}$
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^-$ , $V_{\text{CM}} = V^+$		200	1200	$\mu\text{V}$
$I_{\text{B}}$	Input Bias Current	$V_{\text{CM}} = V^+$		1	5	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.2\text{V}$	-14	-5		$\mu\text{A}$
$\Delta I_{\text{B}}$	Input Bias Current Shift	$V_{\text{CM}} = V^- + 0.2\text{V}$ to $V^+$		6	19	$\mu\text{A}$
		Input Bias Current Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^+$ $V_{\text{CM}} = V^- + 0.2\text{V}$	0.03 0.05	1.4 3.2	$\mu\text{A}$ $\mu\text{A}$
$I_{\text{OS}}$	Input Offset Current	$V_{\text{CM}} = V^+$		0.03	0.7	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.2\text{V}$		0.04	1.6	$\mu\text{A}$
$\Delta I_{\text{OS}}$	Input Offset Current Shift	$V_{\text{CM}} = V^- + 0.2\text{V}$ to $V^+$		0.07	2.3	$\mu\text{A}$
		Input Noise Voltage	0.1Hz to 10Hz	800		$\text{nV}_{\text{P-P}}$
$e_{\text{n}}$	Input Noise Voltage Density	$f = 10\text{kHz}$		3.5		$\text{nV}/\sqrt{\text{Hz}}$
$i_{\text{n}}$	Input Noise Current Density	$f = 10\text{kHz}$		1.5		$\text{pA}/\sqrt{\text{Hz}}$
$C_{\text{IN}}$	Input Capacitance	$f = 100\text{kHz}$		2		$\text{pF}$
$A_{\text{VOL}}$	Large-Signal Voltage Gain	$V_{\text{O}} = -4\text{V}$ to $4\text{V}$ , $R_{\text{L}} = 1\text{k}$	100	300		$\text{V}/\text{mV}$
		$V_{\text{O}} = -2.5\text{V}$ to $2.5\text{V}$ , $R_{\text{L}} = 100\Omega$	10	27		$\text{V}/\text{mV}$
CMRR	Common Mode Rejection Ratio	$V_{\text{CM}} = V^-$ to $V^+$	83	106		$\text{dB}$
	CMRR Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^-$ to $V^+$	77	106		$\text{dB}$
	Input Common Mode Range		$V^-$		$V^+$	$\text{V}$
PSRR	Power Supply Rejection Ratio	$V^+ = 2.5\text{V}$ to $10\text{V}$ , $V^- = 0\text{V}$	90	105		$\text{dB}$
	PSRR Match (Channel-to-Channel) (Note 10)	$V^+ = 2.5\text{V}$ to $10\text{V}$ , $V^- = 0\text{V}$	84	105		$\text{dB}$
$V_{\text{OL}}$	Output Voltage Swing LOW (Note 7)	No Load		14	60	$\text{mV}$
		$I_{\text{SINK}} = 5\text{mA}$		55	140	$\text{mV}$
		$I_{\text{SINK}} = 25\text{mA}$		180	450	$\text{mV}$
$V_{\text{OH}}$	Output Voltage Swing HIGH (Note 7)	No Load		20	70	$\text{mV}$
		$I_{\text{SOURCE}} = 5\text{mA}$		90	200	$\text{mV}$
		$I_{\text{SOURCE}} = 25\text{mA}$		360	700	$\text{mV}$
$I_{\text{SC}}$	Short-Circuit Current		$\pm 40$	$\pm 85$		$\text{mA}$
$I_{\text{S}}$	Supply Current per Amplifier			11	16	$\text{mA}$
	Disable Supply Current	$V_{\text{SHDN}} = 0.3\text{V}$		0.4	1.2	$\text{mA}$
$I_{\text{SHDN}}$	SHDN Pin Current	$V_{\text{SHDN}} = 0.3\text{V}$		150	350	$\mu\text{A}$
	Shutdown Output Leakage Current	$V_{\text{SHDN}} = 0.3\text{V}$		0.3	75	$\mu\text{A}$
$V_{\text{L}}$	SHDN Pin Input Voltage LOW				0.3	$\text{V}$
$V_{\text{H}}$	SHDN Pin Input Voltage HIGH		$V^+ - 0.5$			$\text{V}$
$t_{\text{ON}}$	Turn-On Time	$V_{\text{SHDN}} = 0.3\text{V}$ to $4.5\text{V}$ , $R_{\text{L}} = 100\Omega$		80		$\text{ns}$
$t_{\text{OFF}}$	Turn-Off Time	$V_{\text{SHDN}} = 4.5\text{V}$ to $0.3\text{V}$ , $R_{\text{L}} = 100\Omega$		50		$\text{ns}$
GBW	Gain Bandwidth Product	Frequency = $6\text{MHz}$	170	325		$\text{MHz}$
SR	Slew Rate	$A_{\text{V}} = -1$ , $R_{\text{L}} = 1\text{k}$ , $V_{\text{O}} = \pm 4\text{V}$ , Measured at $V_{\text{O}} = \pm 3\text{V}$	70	140		$\text{V}/\mu\text{s}$
FPBW	Full Power Bandwidth	$V_{\text{O}} = 8\text{V}_{\text{P-P}}$		5.5		$\text{MHz}$
HD	Harmonic Distortion	$A_{\text{V}} = 1$ , $R_{\text{L}} = 1\text{k}$ , $V_{\text{O}} = 2\text{V}_{\text{P-P}}$ , $f_{\text{C}} = 5\text{MHz}$		-80		$\text{dBc}$
$t_{\text{S}}$	Settling Time	0.01%, $V_{\text{STEP}} = 8\text{V}$ , $A_{\text{V}} = 1$ , $R_{\text{L}} = 1\text{k}$		120		$\text{ns}$
$\Delta\text{G}$	Differential Gain (NTSC)	$A_{\text{V}} = 2$ , $R_{\text{L}} = 150$		0.01		%
$\Delta\theta$	Differential Phase (NTSC)	$A_{\text{V}} = 2$ , $R_{\text{L}} = 150$		0.01		Deg

**ELECTRICAL CHARACTERISTICS** The ● denotes specifications which apply over the 0°C < T<sub>A</sub> < 70°C temperature range. V<sub>S</sub> = ±5V, V<sub>SHDN</sub> = open; V<sub>CM</sub> = 0V, V<sub>OUT</sub> = 0V, unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	V <sub>CM</sub> = V <sup>+</sup>	●	200	800	μV
		V <sub>CM</sub> = V <sup>-</sup>	●	200	800	μV
		V <sub>CM</sub> = V <sup>+</sup> (LT1806 SOT-23)	●	200	900	μV
		V <sub>CM</sub> = V <sup>-</sup> (LT1806 SOT-23)	●	200	900	μV
V <sub>OS</sub> TC	Input Offset Voltage Drift (Note 8)	V <sub>CM</sub> = V <sup>+</sup>	●	1.5	5	μV/°C
		V <sub>CM</sub> = V <sup>-</sup>	●	1.5	5	μV/°C
ΔV <sub>OS</sub>	Input Offset Voltage Shift	V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup>	●	100	800	μV
		V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup> (LT1806 SOT-23)	●	100	900	μV
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	V <sub>CM</sub> = V <sup>-</sup> , V <sub>CM</sub> = V <sup>+</sup>	●	300	1400	μV
I <sub>B</sub>	Input Bias Current	V <sub>CM</sub> = V <sup>+</sup> - 0.2V	●	1	6	μA
		V <sub>CM</sub> = V <sup>-</sup> + 0.4V	●	-15	-6	μA
ΔI <sub>B</sub>	Input Bias Current Shift	V <sub>CM</sub> = V <sup>-</sup> + 0.4V to V <sup>+</sup> - 0.2V	●	7	21	μA
	Input Bias Current Match (Channel-to-Channel) (Note 10)	V <sub>CM</sub> = V <sup>+</sup> - 0.2V	●	0.03	1.8	μA
		V <sub>CM</sub> = V <sup>-</sup> + 0.4V	●	0.04	3.8	μA
I <sub>OS</sub>	Input Offset Current	V <sub>CM</sub> = V <sup>+</sup> - 0.2V	●	0.03	0.9	μA
		V <sub>CM</sub> = V <sup>-</sup> + 0.4V	●	0.04	1.9	μA
ΔI <sub>OS</sub>	Input Offset Current Shift	V <sub>CM</sub> = V <sup>-</sup> + 0.4V to V <sup>+</sup> - 0.2V	●	0.07	2.8	μA
A <sub>VOL</sub>	Large-Signal Voltage Gain	V <sub>O</sub> = -4V to 4V, R <sub>L</sub> = 1k	●	80	250	V/mV
		V <sub>O</sub> = -2.5V to 2.5V, R <sub>L</sub> = 100Ω	●	8	25	V/mV
CMRR	Common Mode Rejection Ratio	V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup>	●	81	100	dB
	CMRR Match (Channel-to-Channel) (Note 10)	V <sub>CM</sub> = V <sup>-</sup> to V <sup>+</sup>	●	75	100	dB
	Input Common Mode Range		●	V <sup>-</sup>	V <sup>+</sup>	V
PSRR	Power Supply Rejection Ratio	V <sup>+</sup> = 2.5V to 10V, V <sup>-</sup> = 0V	●	88	105	dB
	PSRR Match (Channel-to-Channel) (Note 10)	V <sup>+</sup> = 2.5V to 10V, V <sup>-</sup> = 0V	●	82	106	dB
V <sub>OL</sub>	Output Voltage Swing LOW (Note 7)	No Load	●	18	80	mV
		I <sub>SINK</sub> = 5mA	●	60	160	mV
		I <sub>SINK</sub> = 25mA	●	185	500	mV
V <sub>OH</sub>	Output Voltage Swing HIGH (Note 7)	No Load	●	40	140	mV
		I <sub>SOURCE</sub> = 5mA	●	110	240	mV
		I <sub>SOURCE</sub> = 25mA	●	360	750	mV
I <sub>SC</sub>	Short-Circuit Current		●	±35	±75	mA
I <sub>S</sub>	Supply Current per Amplifier		●	14	20	mA
	Disable Supply Current	V <sub>SHDN</sub> = 0.3V	●	0.4	1.4	mA
I <sub>SHDN</sub>	SHDN Pin Current	V <sub>SHDN</sub> = 0.3V	●	160	400	μA
	Shutdown Output Leakage Current	V <sub>SHDN</sub> = 0.3V	●	1		μA
V <sub>L</sub>	SHDN Pin Input Voltage LOW		●		0.3	V
V <sub>H</sub>	SHDN Pin Input Voltage HIGH		●	V <sup>+</sup> - 0.5		V
t <sub>ON</sub>	Turn-On Time	V <sub>SHDN</sub> = 0.3V to 4.5V, R <sub>L</sub> = 100Ω	●	80		ns
t <sub>OFF</sub>	Turn-Off Time	V <sub>SHDN</sub> = 4.5V to 0.3V, R <sub>L</sub> = 100Ω	●	50		ns
GBW	Gain Bandwidth Product	Frequency = 6MHz	●	150	300	MHz
SR	Slew Rate	A <sub>V</sub> = -1, R <sub>L</sub> = 1k, V <sub>O</sub> = ±4V, Measure at V <sub>O</sub> = ±3V	●	60	120	V/μs
FPBW	Full Power Bandwidth	V <sub>O</sub> = 8V <sub>P-P</sub>	●	4.5		MHz

# LT1806/LT1807

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the  $-40^{\circ}\text{C} < T_A < 85^{\circ}\text{C}$  temperature range.  $V_S = \pm 5\text{V}$ ,  $V_{\text{SHDN}} = \text{open}$ ;  $V_{\text{CM}} = 0\text{V}$ ,  $V_{\text{OUT}} = 0\text{V}$ , unless otherwise noted. (Note 5)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
$V_{\text{OS}}$	Input Offset Voltage	$V_{\text{CM}} = V^+$	●	200	900	$\mu\text{V}$
		$V_{\text{CM}} = V^-$	●	200	900	$\mu\text{V}$
		$V_{\text{CM}} = V^+$ (LT1806 SOT-23)	●	200	975	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ (LT1806 SOT-23)	●	200	975	$\mu\text{V}$
$V_{\text{OS TC}}$	Input Offset Voltage Drift (Note 8)	$V_{\text{CM}} = V^+$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
		$V_{\text{CM}} = V^-$	●	1.5	5	$\mu\text{V}/^{\circ}\text{C}$
$\Delta V_{\text{OS}}$	Input Offset Voltage Shift	$V_{\text{CM}} = V^-$ to $V^+$	●	100	900	$\mu\text{V}$
		$V_{\text{CM}} = V^-$ to $V^+$ (LT1806 SOT-23)	●	100	975	$\mu\text{V}$
	Input Offset Voltage Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^-$ to $V^+$	●	300	1600	$\mu\text{V}$
$I_{\text{B}}$	Input Bias Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	1.2	7	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	-16	-5	$\mu\text{A}$
$\Delta I_{\text{B}}$	Input Bias Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V}$ to $V^+ - 0.2\text{V}$	●	6	23	$\mu\text{A}$
		Input Bias Current Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	0.03	2.0
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.04	4.5	$\mu\text{A}$
$I_{\text{OS}}$	Input Offset Current	$V_{\text{CM}} = V^+ - 0.2\text{V}$	●	0.03	1.0	$\mu\text{A}$
		$V_{\text{CM}} = V^- + 0.4\text{V}$	●	0.04	2.2	$\mu\text{A}$
$\Delta I_{\text{OS}}$	Input Offset Current Shift	$V_{\text{CM}} = V^- + 0.4\text{V}$ to $V^+ - 0.2\text{V}$	●	0.07	3.2	$\mu\text{A}$
$A_{\text{VOL}}$	Large-Signal Voltage Gain	$V_{\text{O}} = -4\text{V}$ to $4\text{V}$ , $R_{\text{L}} = 1\text{k}$	●	60	175	$\text{V}/\text{mV}$
		$V_{\text{O}} = -2\text{V}$ to $2\text{V}$ , $R_{\text{L}} = 100\Omega$	●	7	17	$\text{V}/\text{mV}$
CMRR	Common Mode Rejection Ratio	$V_{\text{CM}} = V^-$ to $V^+$	●	80	100	dB
	CMRR Match (Channel-to-Channel) (Note 10)	$V_{\text{CM}} = V^-$ to $V^+$	●	74	100	dB
	Input Common Mode Range		●	$V^-$	$V^+$	V
PSRR	Power Supply Rejection Ratio	$V^+ = 2.5\text{V}$ to $10\text{V}$ , $V^- = 0\text{V}$	●	86	105	dB
	PSRR Match (Channel-to-Channel) (Note 10)		●	80	105	dB
$V_{\text{OL}}$	Output Voltage Swing LOW (Note 7)	No Load	●	20	100	mV
		$I_{\text{SINK}} = 5\text{mA}$	●	65	170	mV
		$I_{\text{SINK}} = 20\text{mA}$	●	200	500	mV
$V_{\text{OH}}$	Output Voltage Swing HIGH (Note 7)	No Load	●	50	160	mV
		$I_{\text{SOURCE}} = 5\text{mA}$	●	115	260	mV
		$I_{\text{SOURCE}} = 20\text{mA}$	●	360	700	mV
$I_{\text{SC}}$	Short-Circuit Current		●	$\pm 25$	$\pm 55$	mA
$I_{\text{S}}$	Supply Current		●	15	22	mA
	Disable Supply Current	$V_{\text{SHDN}} = 0.3\text{V}$	●	0.45	1.5	mA
$I_{\text{SHDN}}$	SHDN Pin Current	$V_{\text{SHDN}} = 0.3\text{V}$	●	170	450	$\mu\text{A}$
	Shutdown Output Leakage Current	$V_{\text{SHDN}} = 0.3\text{V}$	●	1.2		$\mu\text{A}$
$V_{\text{L}}$	SHDN Pin Input Voltage LOW		●		0.3	V
$V_{\text{H}}$	SHDN Pin Input Voltage HIGH		●	$V^+ - 0.5$		V
$t_{\text{ON}}$	Turn-On Time	$V_{\text{SHDN}} = 0.3\text{V}$ to $4.5\text{V}$ , $R_{\text{L}} = 100\Omega$	●	80		ns
$t_{\text{OFF}}$	Turn-Off Time	$V_{\text{SHDN}} = 4.5\text{V}$ to $0.3\text{V}$ , $R_{\text{L}} = 100\Omega$	●	50		ns
GBW	Gain Bandwidth Product	Frequency = 6MHz	●	125	290	MHz
SR	Slew Rate	$A_{\text{V}} = -1$ , $R_{\text{L}} = 1\text{k}$ , $V_{\text{O}} = \pm 4\text{V}$ , Measured at $V_{\text{O}} = \pm 3\text{V}$	●	50	100	$\text{V}/\mu\text{s}$
FPBW	Full Power Bandwidth	$V_{\text{O}} = 8\text{V}_{\text{P-P}}$	●	4		MHz

**Note 1:** Absolute maximum ratings are those values beyond which the life of the device may be impaired.

**Note 2:** The inputs are protected by back-to-back diodes. If the differential input voltage exceeds 1.4V, the input current should be limited to less than 10mA.



## ELECTRICAL CHARACTERISTICS

**Note 3:** A heat sink may be required to keep the junction temperature below the absolute maximum rating when the output is shorted indefinitely.

**Note 4:** The LT1806C/LT1806I and LT1807C/LT1807I are guaranteed functional over the temperature range of  $-40^{\circ}\text{C}$  and  $85^{\circ}\text{C}$ .

**Note 5:** The LT1806C/LT1807C are guaranteed to meet specified performance from  $0^{\circ}\text{C}$  to  $70^{\circ}\text{C}$ . The LT1806C/LT1807C are designed, characterized and expected to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$  but are not tested or QA sampled at these temperatures. The LT1806I/LT1807I are guaranteed to meet specified performance from  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ .

**Note 6:** Minimum supply voltage is guaranteed by power supply rejection ratio test.

**Note 7:** Output voltage swings are measured between the output and power supply rails.

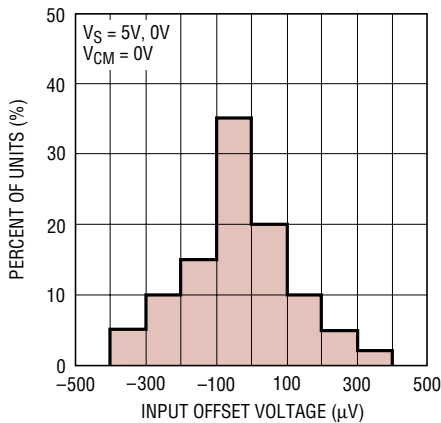
**Note 8:** This parameter is not 100% tested.

**Note 9:** Thermal resistance varies depending upon the amount of PC board metal attached to the  $V^-$  pin of the device.  $\theta_{JA}$  is specified for a certain amount of 2oz copper metal trace connecting to the  $V^-$  pin as described in the thermal resistance tables in the Applications Information section.

**Note 10:** Matching parameters are the difference between the two amplifiers of the LT1807.

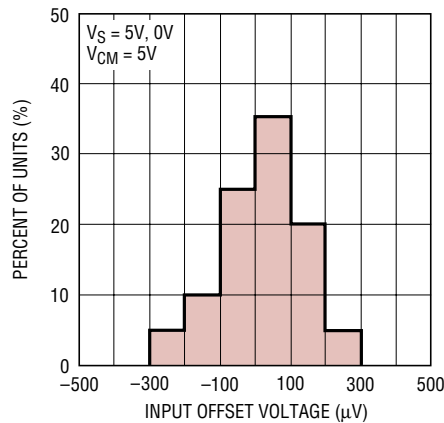
## TYPICAL PERFORMANCE CHARACTERISTICS

**$V_{OS}$  Distribution,  $V_{CM} = 0\text{V}$   
(PNP Stage)**



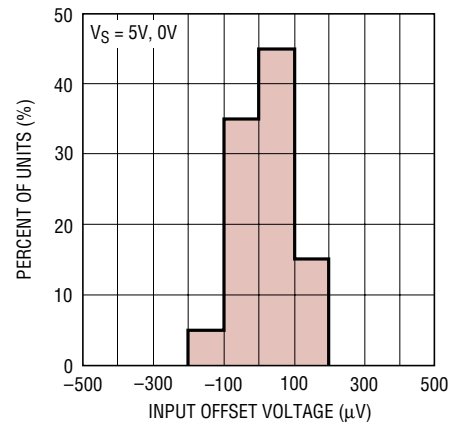
18067 G01

**$V_{OS}$  Distribution,  $V_{CM} = 5\text{V}$   
(NPN Stage)**



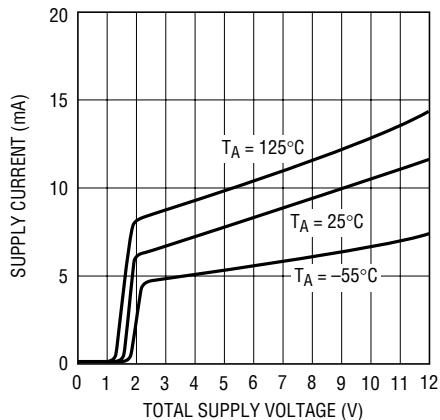
18067 G02

**$\Delta V_{OS}$  Shift for  $V_{CM} = 0\text{V}$  to  $5\text{V}$**



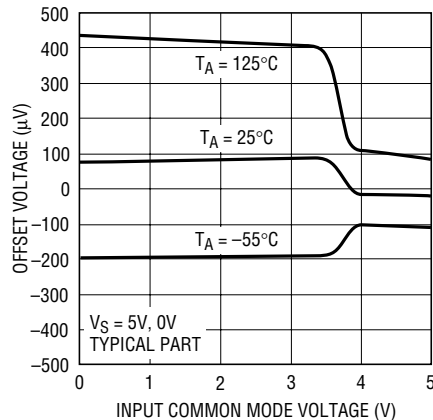
18067 G03

**Supply Current per Amp  
vs Supply Voltage**



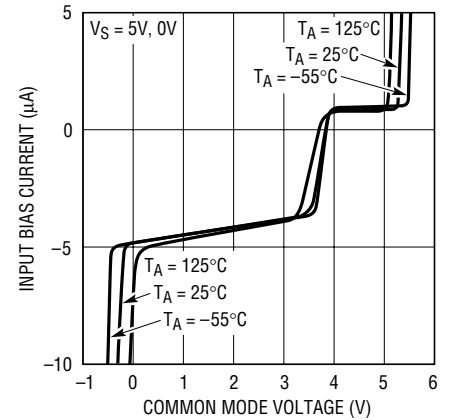
18067 G04

**Offset Voltage  
vs Input Common Mode**



18067 G05

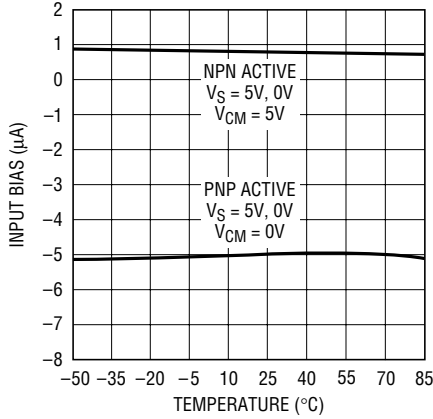
**Input Bias Current  
vs Common Mode Voltage**



18067 G06

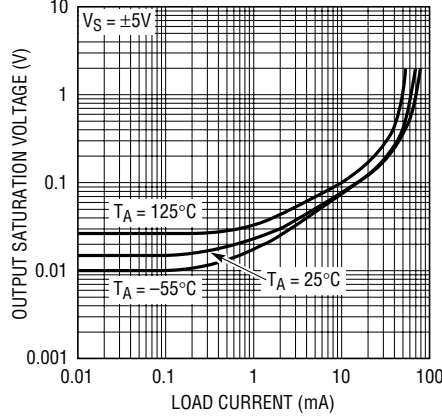
# TYPICAL PERFORMANCE CHARACTERISTICS

**Input Bias Current vs Temperature**



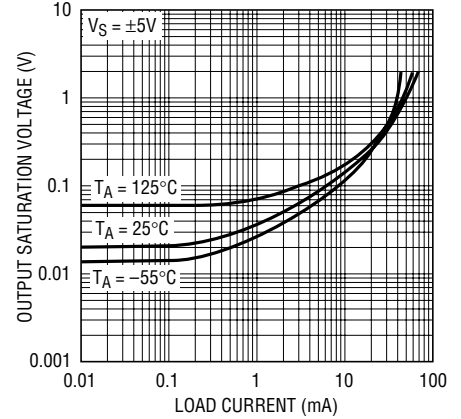
18067 G07

**Output Saturation Voltage vs Load Current (Output Low)**



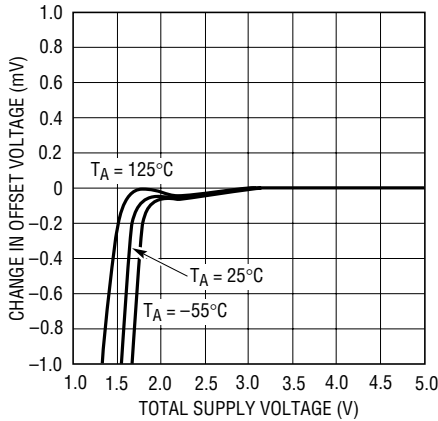
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**Output Saturation Voltage vs Load Current (Output High)**



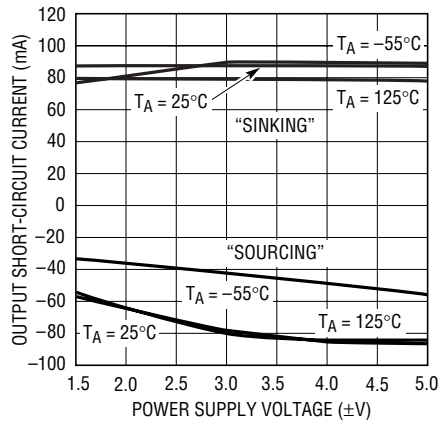
18067 G09

**Minimum Supply Voltage**



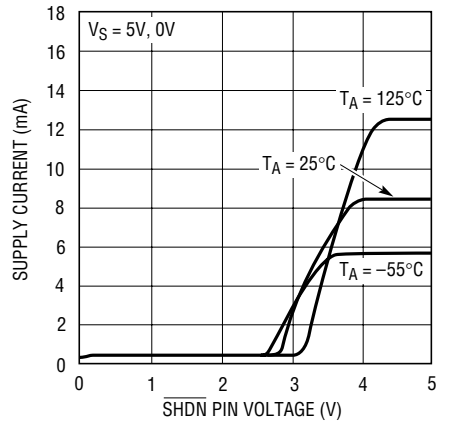
18067 G10

**Output Short-Circuit Current vs Power Supply Voltage**



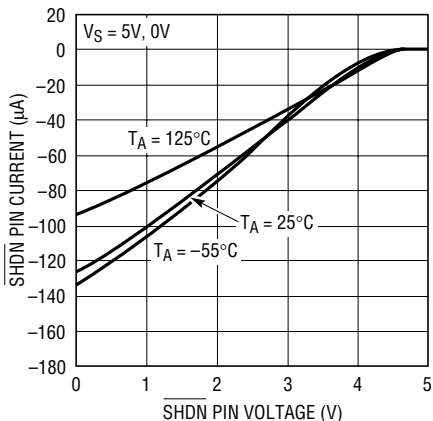
18067 G11

**Supply Current vs SHDN Pin Voltage**



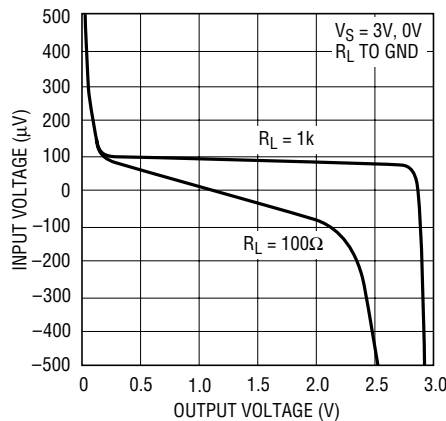
18067 G12

**SHDN Pin Current vs SHDN Pin Voltage**



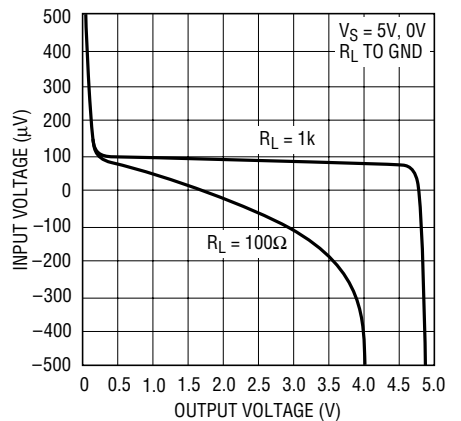
18067 G13

**Open-Loop Gain**



18067 G14

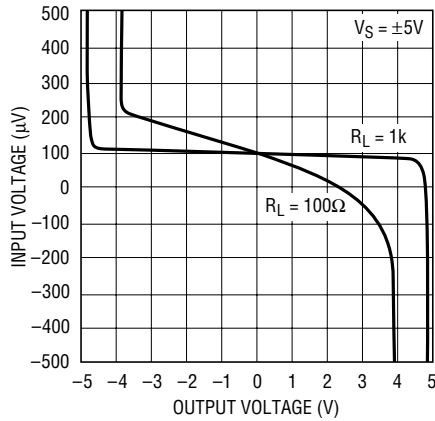
**Open-Loop Gain**



18067 G15

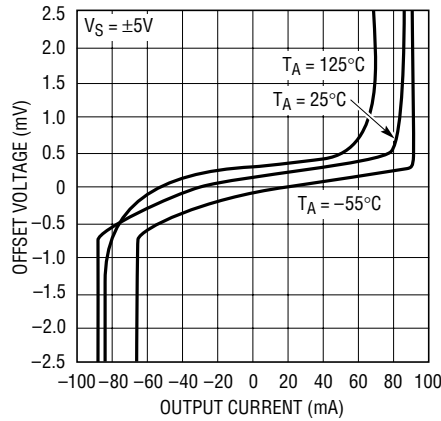
# TYPICAL PERFORMANCE CHARACTERISTICS

**Open-Loop Gain**



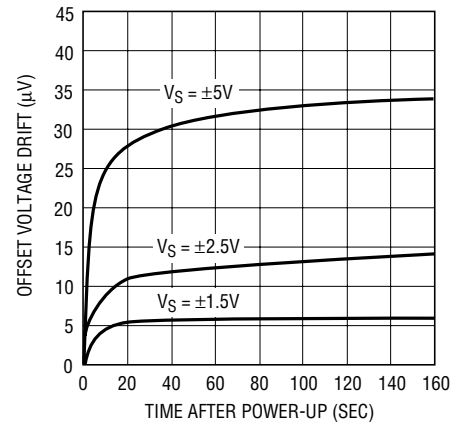
18067 G16

**Offset Voltage vs Output Current**



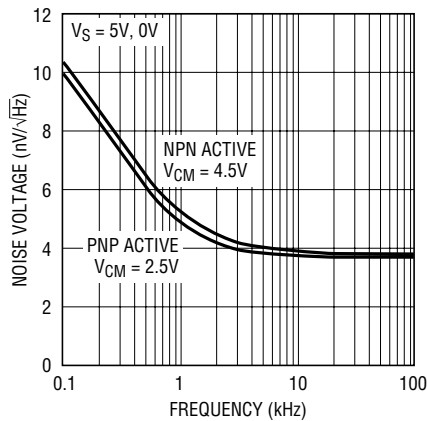
18067 G17

**Warm-Up Drift vs Time (LT1806S8)**



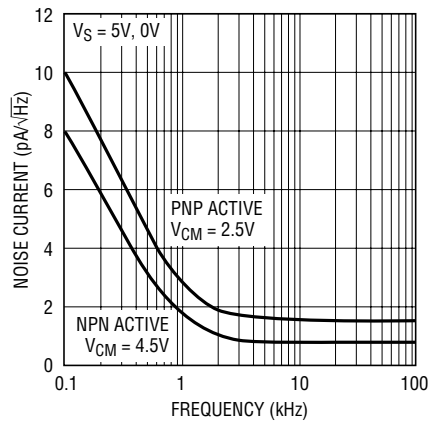
18067 G18

**Input Noise Voltage vs Frequency**



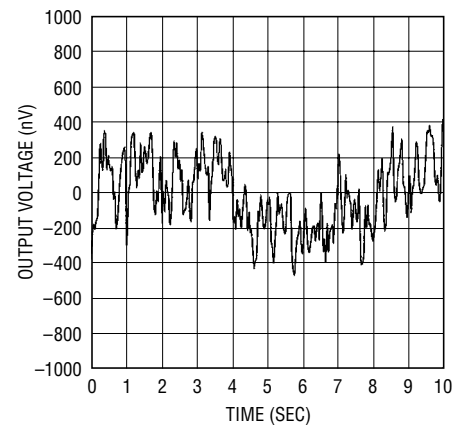
18067 G19

**Input Noise Current vs Frequency**



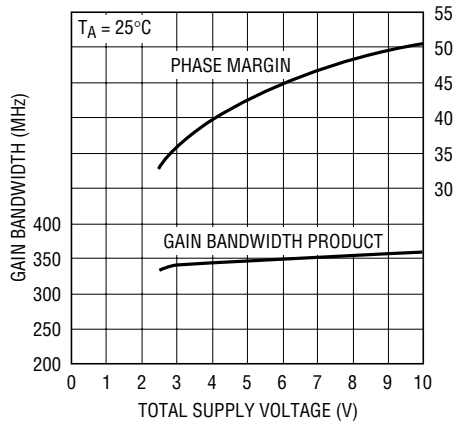
18067 G19

**0.1Hz to 10Hz Output Voltage Noise**



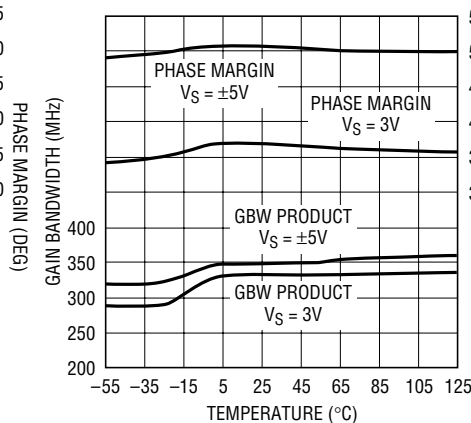
18067 G21

**Gain Bandwidth and Phase Margin vs Supply Voltage**



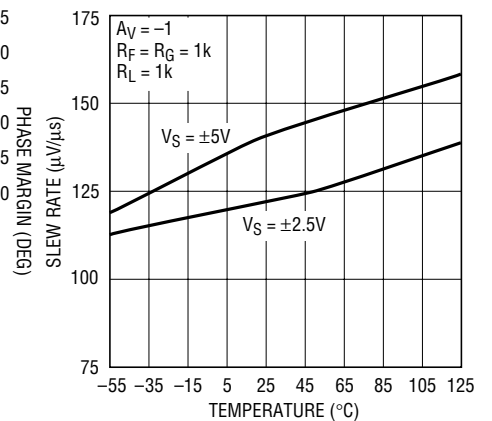
18067 G22

**Gain Bandwidth and Phase Margin vs Temperature**



18067 G23

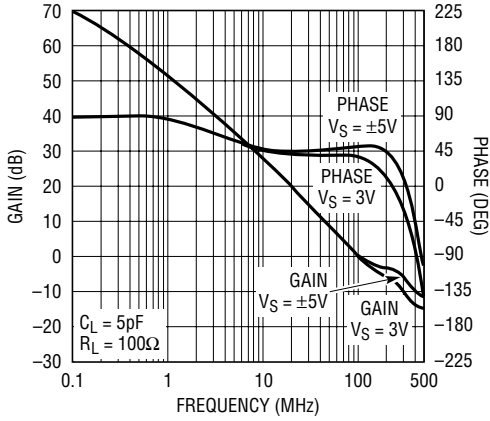
**Slew Rate vs Temperature**



18067 G24

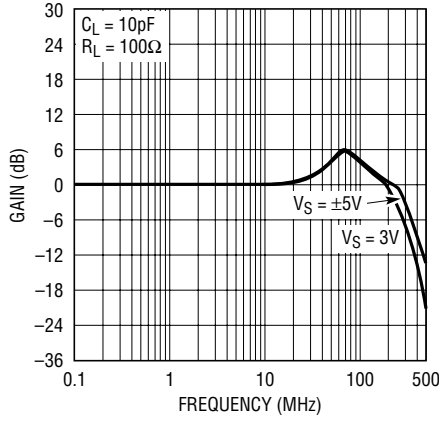
**TYPICAL PERFORMANCE CHARACTERISTICS**

**Gain and Phase vs Frequency**



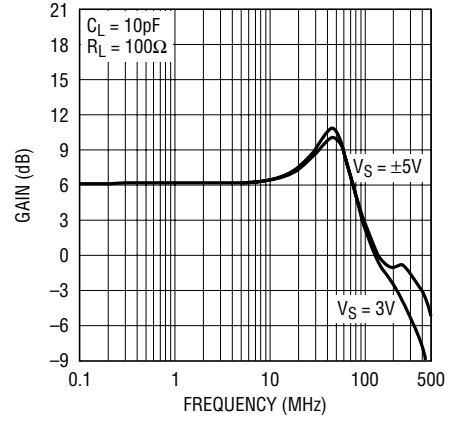
18067 G25

**Gain vs Frequency ( $A_V = 1$ )**



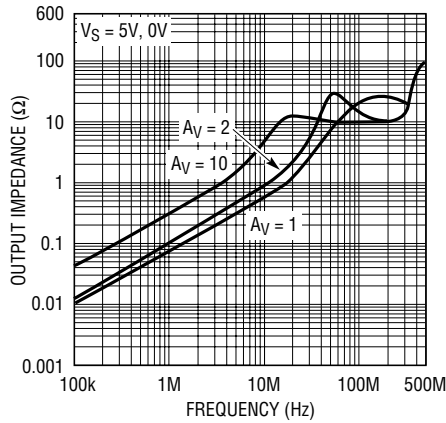
18067 G26

**Gain vs Frequency ( $A_V = 2$ )**



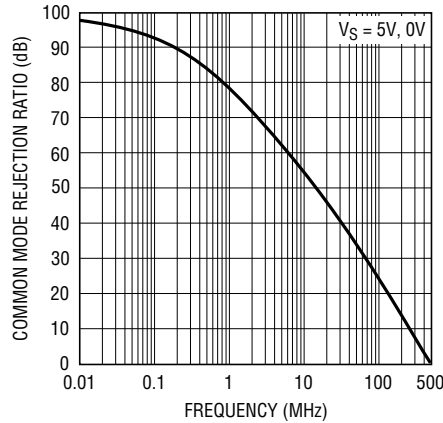
18067 G27

**Output Impedance vs Frequency**



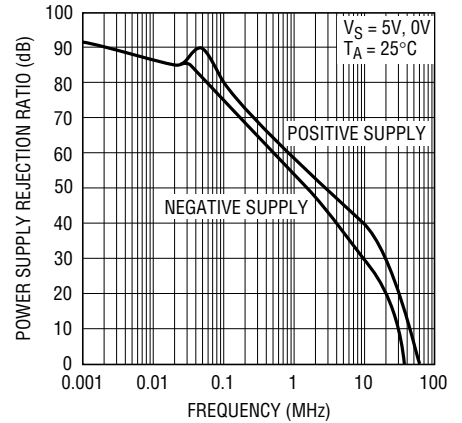
18067 G28

**Common Mode Rejection Ratio vs Frequency**



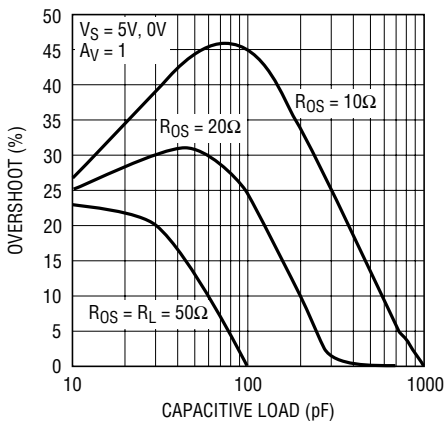
18067 G29

**Power Supply Rejection Ratio vs Frequency**



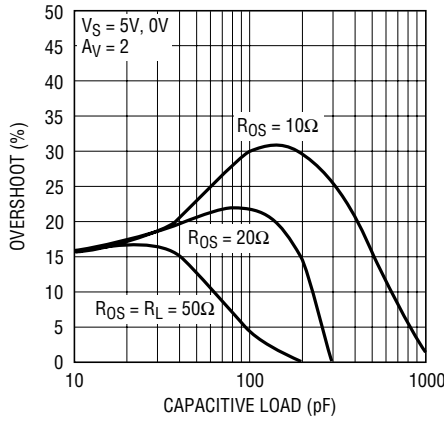
18067 G30

**Series Output Resistor vs Capacitive Load**



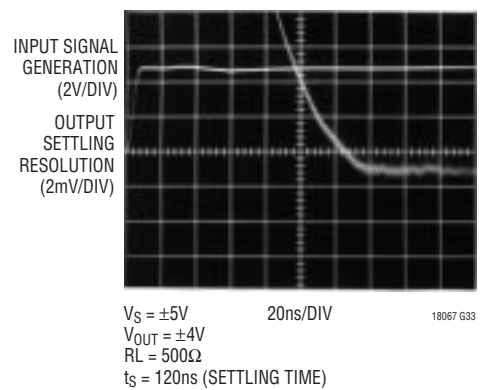
18067 G31

**Series Output Resistor vs Capacitive Load**



18067 G32

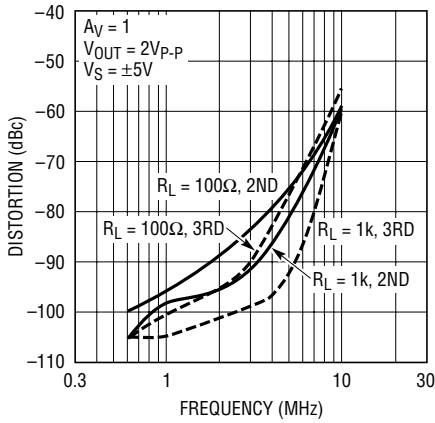
**0.01% Settling Time**



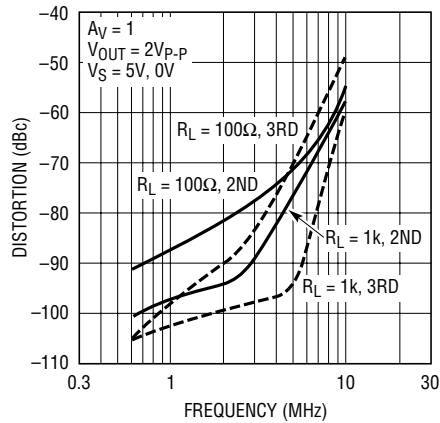
18067 G33

# TYPICAL PERFORMANCE CHARACTERISTICS

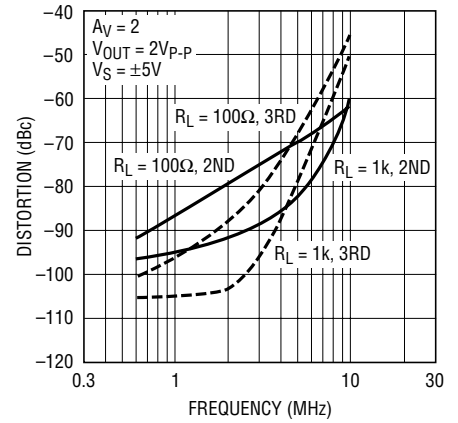
**Distortion vs Frequency**



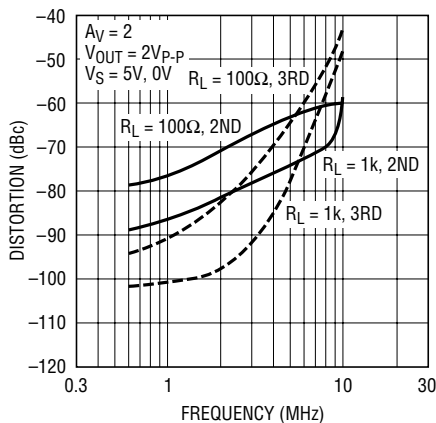
**Distortion vs Frequency**



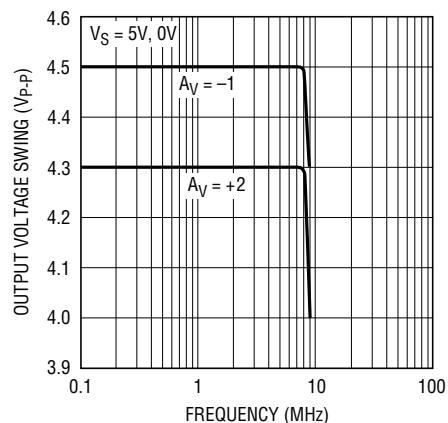
**Distortion vs Frequency**



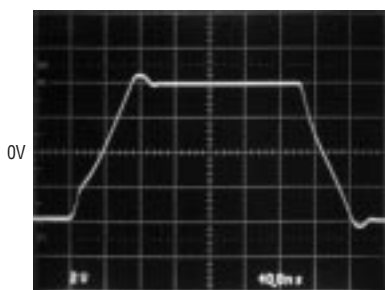
**Distortion vs Frequency**



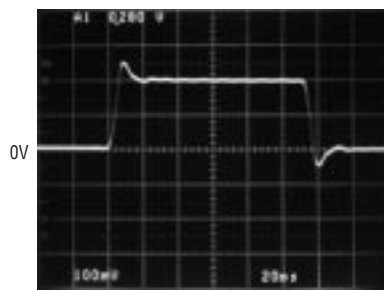
**Maximum Undistorted Output Signal vs Frequency**



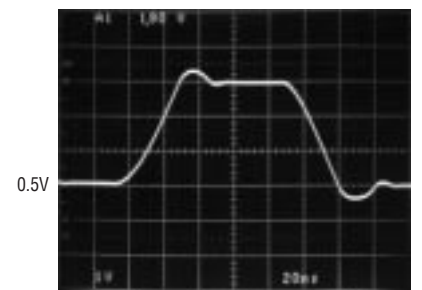
**±5V Large-Signal Response**



**±5V Small-Signal Response**



**5V Large-Signal Response**



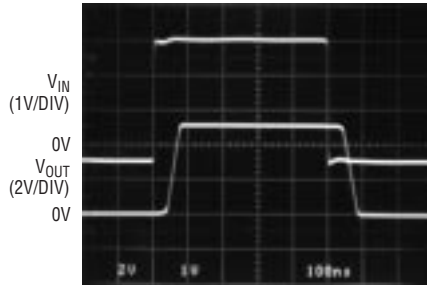
## TYPICAL PERFORMANCE CHARACTERISTICS

5V Small-Signal Response



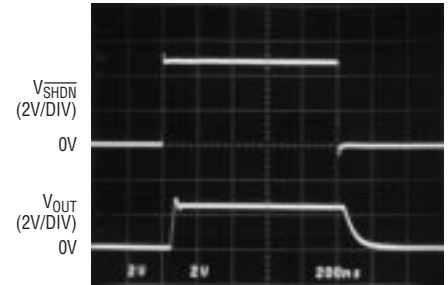
$V_S = 5V, 0V$  10ns/DIV 18067 G42  
 $A_V = 1$   
 $R_L = 1k$

Output Overdriven Recovery



$V_S = 5V, 0V$  100ns/DIV 18067 G43  
 $A_V = 2$   
 $R_L = 1k$

Shutdown Response



$V_S = 5V, 0V$  200ns/DIV 18067 G44  
 $A_V = 2$   
 $R_L = 100\Omega$

## APPLICATIONS INFORMATION

### Rail-to-Rail Characteristics

The LT1806/LT1807 have input and output signal range that covers from negative power supply to positive power supply. Figure 1 depicts a simplified schematic of the amplifier. The input stage is comprised of two differential amplifiers, a PNP stage Q1/Q2 and a NPN stage Q3/Q4 that are active over different ranges of common mode input voltage. The PNP differential pair is active between the negative supply to approximately 1.5V below the positive

supply. As the input voltage moves closer toward the positive supply, the transistor Q5 will steer the tail current  $I_1$  to the current mirror Q6/Q7, activating the NPN differential pair. The PNP pair becomes inactive for the rest of the input common mode range up to the positive supply.

A pair of complementary common emitter stages Q14/Q15 that enable the output to swing from rail to rail constructs the output stage. The capacitors C1 and C2 form the local feedback loops that lower the output

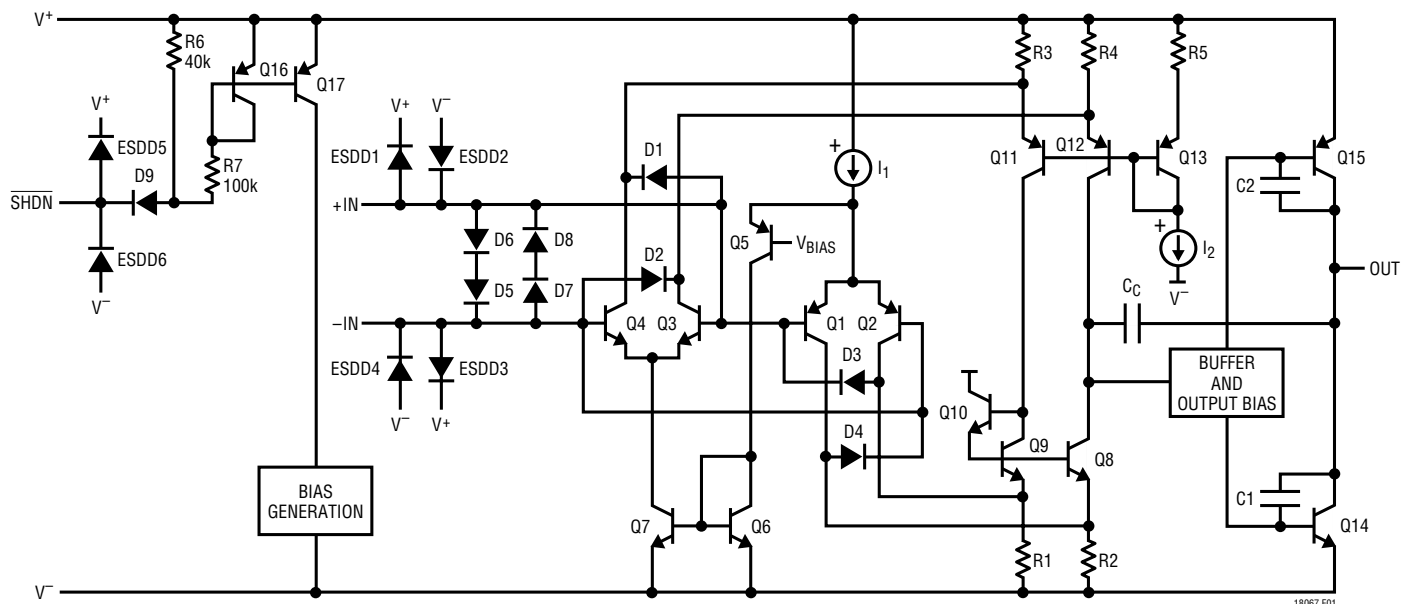


Figure 1. LT1806 Simplified Schematic Diagram

## APPLICATIONS INFORMATION

impedance at high frequency. These devices are fabricated on Linear Technology's proprietary high speed complementary bipolar process.

### Power Dissipation

The LT1806/LT1807 amplifiers combine high speed with large output current in a small package, so there is a need to ensure that the die's junction temperature does not exceed 150°C. The LT1806 is housed in an SO-8 package or a 6-lead SOT-23 package and the LT1807 is in an SO-8 or 8-lead MSOP package. All packages have the V<sup>-</sup> supply pin fused to the lead frame to enhance the thermal conductance when connecting to a ground plane or a large metal trace. Metal trace and plated through-holes can be used to spread the heat generated by the device to the backside of the PC board. For example, on a 3/32" FR-4 board with 2oz copper, a total of 660 square millimeters connects to Pin 4 of LT1807 in an SO-8 package (330 square millimeters on each side of the PC board) will bring the thermal resistance,  $\theta_{JA}$ , to about 85°C/W. Without extra metal trace beside the power line connecting to the V<sup>-</sup> pin to provide a heat sink, the thermal resistance will be around 105°C/W. More information on thermal resistance for all packages with various metal areas connecting to the V<sup>-</sup> pin is provided in Tables 1, 2 and 3.

**Table 1. LT1806 6-Lead SOT-23 Package**

COPPER AREA		BOARD AREA (mm <sup>2</sup> )	THERMAL RESISTANCE (JUNCTION-TO-AMBIENT)
TOPSIDE (mm <sup>2</sup> )	BACKSIDE (mm <sup>2</sup> )		
270		2500	135°C/W
100		2500	145°C/W
20		2500	160°C/W
0		2500	200°C/W

Device is mounted on topside.

**Table 2. LT1806/LT1807 SO-8 Package**

COPPER AREA		BOARD AREA (mm <sup>2</sup> )	THERMAL RESISTANCE (JUNCTION-TO-AMBIENT)
TOPSIDE (mm <sup>2</sup> )	BACKSIDE (mm <sup>2</sup> )		
1100	1100	2500	65°C/W
330	330	2500	85°C/W
35	35	2500	95°C/W
35	0	2500	100°C/W
0	0	2500	105°C/W

Device is mounted on topside.

**Table 3. LT1807 8-Lead MSOP Package**

COPPER AREA		BOARD AREA (mm <sup>2</sup> )	THERMAL RESISTANCE (JUNCTION-TO-AMBIENT)
TOPSIDE (mm <sup>2</sup> )	BACKSIDE (mm <sup>2</sup> )		
540	540	2500	110°C/W
100	100	2500	120°C/W
100	0	2500	130°C/W
30	0	2500	135°C/W
0	0	2500	140°C/W

Device is mounted on topside.

Junction temperature T<sub>J</sub> is calculated from the ambient temperature T<sub>A</sub> and power dissipation P<sub>D</sub> as follows:

$$T_J = T_A + (P_D \cdot \theta_{JA})$$

The power dissipation in the IC is the function of the supply voltage, output voltage and the load resistance. For a given supply voltage, the worst-case power dissipation P<sub>D(MAX)</sub> occurs at the maximum quiescent supply current and at the output voltage which is half of either supply voltage (or the maximum swing if it is less than 1/2 the supply voltage). P<sub>D(MAX)</sub> is given by:

$$P_{D(MAX)} = (V_S \cdot I_{S(MAX)}) + (V_S/2)^2/R_L$$

Example: An LT1807 in SO-8 mounted on a 2500mm<sup>2</sup> area of PC board without any extra heat spreading plane connected to its V<sup>-</sup> pin has a thermal resistance of 105°C/W,  $\theta_{JA}$ . Operating on ±5V supplies with both amplifiers simultaneously driving 50Ω loads, the worst-case power dissipation is given by:

$$\begin{aligned} P_{D(MAX)} &= 2 \cdot (10 \cdot 14mA) + 2 \cdot (2.5)^2/50 \\ &= 0.28 + 0.25 = 0.53W \end{aligned}$$

The maximum ambient temperature that the part is allowed to operate is:

$$\begin{aligned} T_A &= T_J - (P_{D(MAX)} \cdot 105^\circ\text{C/W}) \\ &= 150^\circ\text{C} - (0.53W \cdot 105^\circ\text{C/W}) = 94^\circ\text{C} \end{aligned}$$

To operate the device at higher ambient temperature, connect more metal area to the V<sup>-</sup> pin to reduce the thermal resistance of the package as indicated in Table 2.

## APPLICATIONS INFORMATION

### Input Offset Voltage

The offset voltage will change depending upon which input stage is active and the maximum offset voltage is guaranteed to be less than  $550\mu\text{V}$ . To maintain the precision characteristics of the amplifier, the change of  $V_{OS}$  over the entire input common mode range (CMRR) is limited to be less than  $550\mu\text{V}$  on a single 5V and 3V supply.

### Input Bias Current

The input bias current polarity depends on a given input common voltage at which the input stage is operating. When the PNP input stage is active, the input bias currents flow out of the input pins. When the NPN input stage is activated, the input bias current flows into the input pins. Because the input offset current is less than the input bias current, matching the source resistances at the input pins will reduce total offset error.

### Output

The LT1806/LT1807 can deliver a large output current, so the short-circuit current limit is set around 90mA to prevent damage to the device. Attention must be paid to keep the junction temperature of the IC below the absolute maximum rating of  $150^{\circ}\text{C}$  (refer to the Power Dissipation section) when the output is continuously short-circuited. The output of the amplifier has reverse-biased diodes connected to each supply. If the output is forced beyond either supply, unlimited current will flow through these diodes. If the current is transient and limited to one hundred milliamps or less, no damage to the device will occur.

### Overdrive Protection

When the input voltage exceeds the power supplies, two pairs of crossing diodes D1 to D4 will prevent the output from reversing polarity. If the input voltage exceeds either power supply by 700mV, diode D1/D2 or D3/D4 will turn on to keep the output at the proper polarity. For the phase reversal protection to perform properly, the input current must be limited to less than 5mA. If the amplifier is

severely overdriven, an external resistor should be used to limit the overdrive current.

The LT1806/LT1807's input stages are also protected against large differential input voltages of 1.4V or higher by a pair of back-to-back diodes, D5/D8, that prevent the emitter-base breakdown of the input transistors. The current in these diodes should be limited to less than 10mA when they are active. The worst-case differential input voltage usually occurs when the input is driven while the output is shorted to ground in a unity gain configuration. In addition, the amplifier is protected against ESD strikes up to 3kV on all pins by a pair of protection diodes, ESDD1 to ESDD6, on each pin that are connected to the power supplies as shown in Figure 1.

### Capacitive Load

The LT1806/LT1807 are optimized for high bandwidth and low distortion applications. They can drive a capacitive load of about 20pF in a unity-gain configuration, and more for higher gain. When driving a larger capacitive load, a resistor of  $10\Omega$  to  $50\Omega$  should be connected between the output and the capacitive load to avoid ringing or oscillation. The feedback should still be taken from the output so that the resistor will isolate the capacitive load to ensure stability. Graphs on capacitive loads indicate the transient response of the amplifier when driving the capacitive load with a specified series resistor.

### Feedback Components

When feedback resistors are used to set up gain, care must be taken to ensure that the pole formed by the feedback resistors and the total capacitance at the inverting input does not degrade stability. For instance, the LT1806/LT1807 in a noninverting gain of 2, set up with two 1k resistors and a capacitance of 3pF (part plus PC board) will probably ring in transient response. The pole is formed at 106MHz that will reduce phase margin by 34 degrees when the crossover frequency of the amplifier is around 70MHz. A capacitor of 3pF or higher connected across the feedback resistor will eliminate any ringing or oscillation.



## APPLICATIONS INFORMATION

### SHDN Pin

The LT1806 has a  $\overline{\text{SHDN}}$  pin to reduce the supply current to less than 0.9mA. When the SHDN pin is pulled low, it will generate a signal to power down the device. If the pin is left unconnected, an internal pull-up resistor of 40k will keep the part fully operating as shown in Figure 1. The output

will be high impedance during shutdown, and the turn-on and turn-off time is less than 100ns. Because the input is protected by a pair of back to back diodes, the input signal will feed through to the output during shutdown mode if the amplitude of signal between the inputs is larger than 1.4V.

## TYPICAL APPLICATIONS

### Driving A/D Converter

The LT1806/LT1807 have 60ns settling time to 0.01% on a 2V step signal, and 20 $\Omega$  output impedance at 100MHz, that makes them ideal for driving high speed A/D converters. With the rail-to-rail input and output, and low supply voltage operation, the LT1806/LT1807 are also desirable for single supply applications. As shown in the application on the front page of this data sheet, the LT1807 drives a 10Msps, 12-bit, LTC1420 ADC in a gain of 20. Driving the LTC1420 differentially will optimize the signal-to-noise ratio, SNR, and the total harmonic distortion, THD, of the A/D converter. The lowpass filter, R5, R6 and C3 reduce

noise or distortion products that might come from the input signal. High quality capacitors and resistors, NPO chip capacitor and metal film surface mount resistors, should be used since these components can add to distortion. The voltage glitch of the converter, due to its sampling nature is buffered by the LT1807, and the ability of the amplifier to settle it quickly will affect the spurious free dynamic range of the system. Figure 2 depicts the LT1806 driving LTC1420 at noninverting gain of 2 configuration. The FFT responses show a better than 92dB of spurious free dynamic range, SFDR.

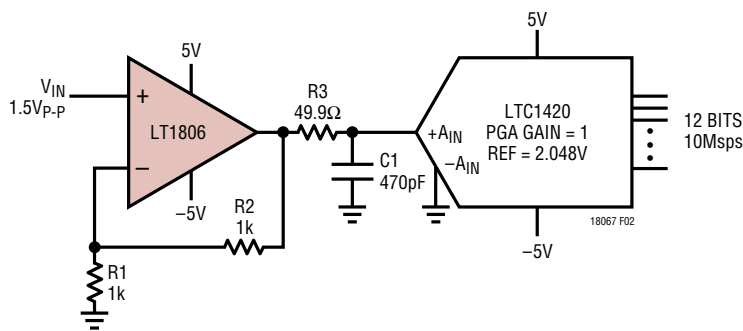


Figure 2. Noninverting A/D Driver

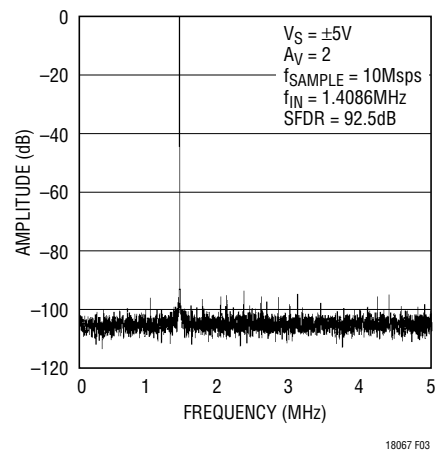


Figure 3. 4096 Point FFT Response

## TYPICAL APPLICATIONS

### Single Supply Video Line Driver

The LT1806/LT1807 are wideband rail-to-rail op amps with large output current that allows them to drive video signals in low supply applications. Figure 4 depicts a single supply video line driver with AC coupling to minimize the quiescent power dissipation. Resistors R1 and R2 are used to level-shift the input and output to provide the largest signal swing. The gain of 2 is set up with R3 and R4 to restore the signal at  $V_{OUT}$ , which is attenuated by 6dB due to the matching of the 75Ω line with the back-terminated

resistor, R5. The back termination will eliminate any reflection of the signal that comes from the load. The input termination resistor,  $R_T$ , is optional—it is used only if matching of the incoming line is necessary. The values of C1, C2 and C3 are selected to minimize the droop of the luminance signal. In some less stringent requirements, the value of capacitors could be reduced. The -3dB bandwidth of the driver is about 90MHz on 5V supply, and the amount of peaking will vary upon the value of capacitor C4.

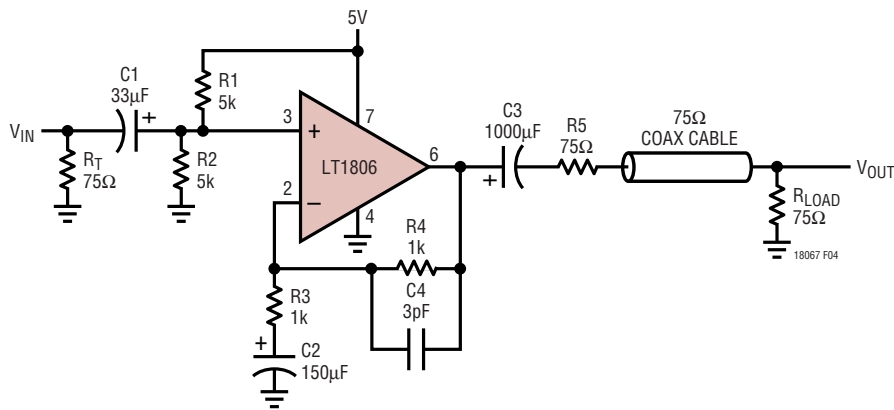


Figure 4. 5V Single Supply Video Line Driver

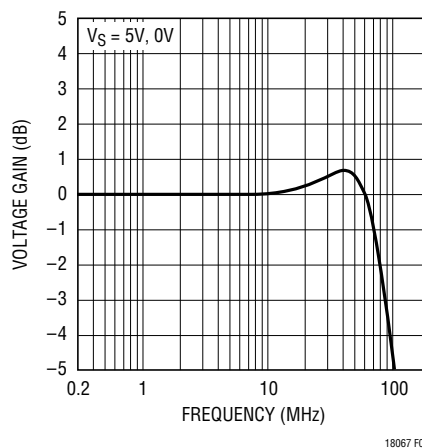


Figure 5. Video Line Driver Frequency Response

## TYPICAL APPLICATIONS

### Single 3V Supply, 4MHz, 4<sup>th</sup> Order Butterworth Filter

Benefiting from a low voltage supply operation, low distortion and rail-to-rail output of LT1806/LT1807, a low distortion filter that is suitable for antialiasing can be built as shown in Figure 6.

On a 3V supply, the filter built with LT1807 has a passband of 4MHz with 2.5V<sub>P-P</sub> signal and stopband that is greater than 70dB to frequency of 100MHz. As an option to minimize the DC offset voltage at the output, connect a series resistor of 365Ω and a bypass capacitor at the noninverting inputs of the amplifiers as shown in Figure 6.

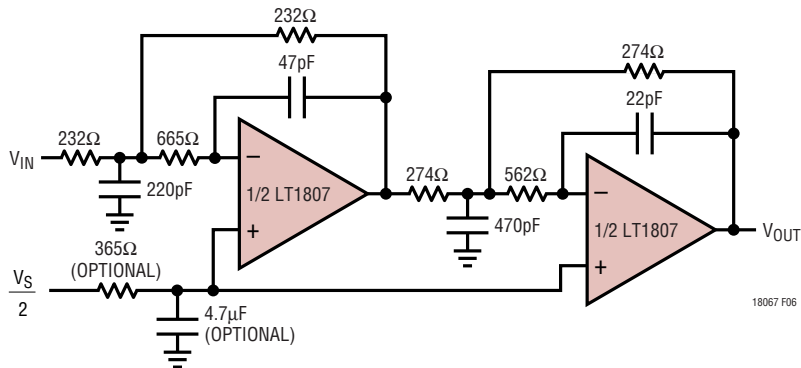


Figure 6. Single 3V Supply, 4MHz, 4th Order Butterworth Filter

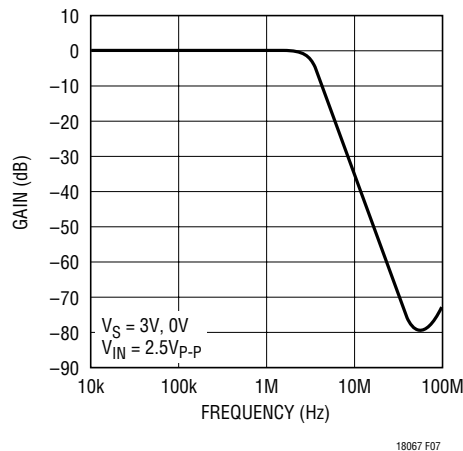


Figure 7. Filter Frequency Response

## TYPICAL APPLICATIONS

### 1MHz Series Resonant Crystal Oscillator with Square and Sinusoid Outputs

Figure 8 shows a classic 1MHz series resonant crystal oscillator. At series resonance, the crystal is a low impedance and the positive feedback connection is what brings about oscillation at the series resonance frequency. The RC feedback around the other path ensures that the circuit does not find a stable DC operating point and refuse to oscillate. The comparator output is a 1MHz square wave with a measured jitter of  $28\text{ps}_{\text{RMS}}$  with a 5V supply and  $40\text{ps}_{\text{RMS}}$  with a 3V supply. On the other side of the crystal, however, is an excellent looking sine wave except for the fact of the small high frequency glitch caused by the fast

edge and the crystal capacitance (middle trace of Figure 9). Sinusoid amplitude stability is maintained by the fact that the sine wave is basically a filtered version of the square wave; the usual amplitude control loops associated with sinusoidal oscillators are not immediately necessary.<sup>1</sup> One can make use of this sine wave by buffering and filtering it, and this is the combined task of the LT1806. It is configured as a bandpass filter with a Q of 5 and does a good job of cleaning up and buffering the sine wave. Distortion was measured at  $-70\text{dBc}$  and  $-60\text{dBc}$  on the second and third harmonics.

<sup>1</sup>Amplitude will be a linear function of comparator output swing, which is supply dependent and therefore controllable. The important difference here is that any added amplitude stabilization loop will not be faced with the classical task of avoiding regions of nonoscillation versus clipping.

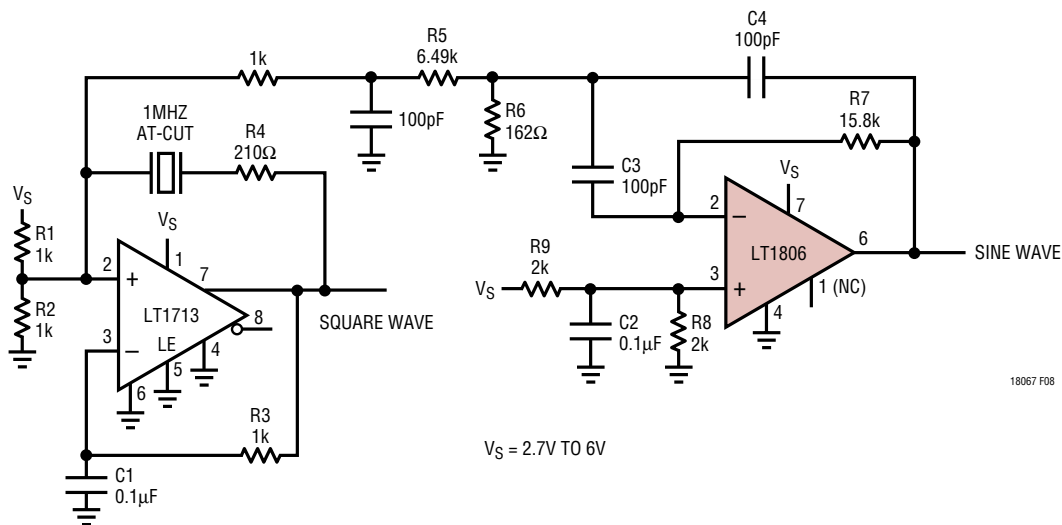


Figure 8. LT1713 Comparator is Configured as a Series Resonant Crystal Oscillator. The LT1806 Op Amp is Configured in a Q = 5 Bandpass Filter with  $f_c = 1\text{MHz}$

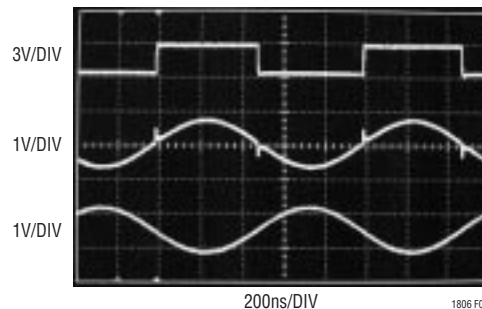
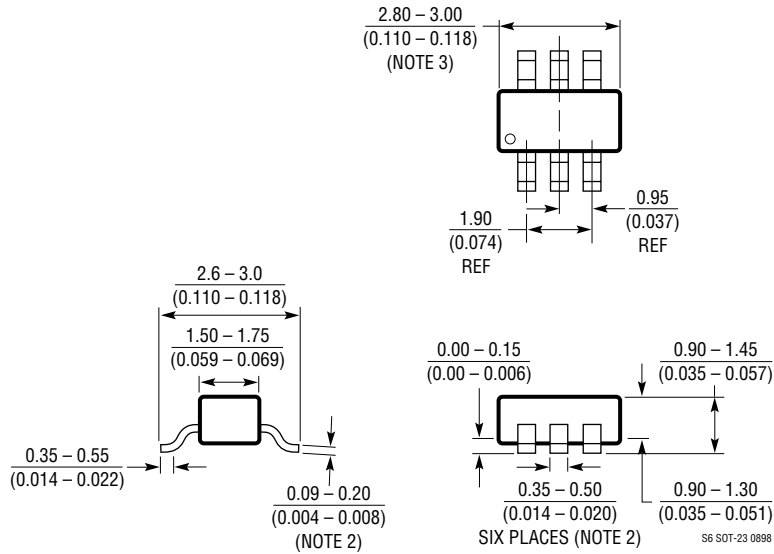


Figure 9. Oscillator Waveforms with  $V_S = 3\text{V}$ . Top Trace is Comparator Output. Middle Trace is Crystal Feedback to Pin 2 at LT1713. Bottom Trace is Buffered, Inverted and Bandpass Filtered with a Q of 5 by the LT1806

**PACKAGE DESCRIPTION** Dimensions in inches (millimeters) unless otherwise noted.

**S6 Package**  
**6-Lead Plastic SOT-23**  
 (LTC DWG # 05-08-1634)

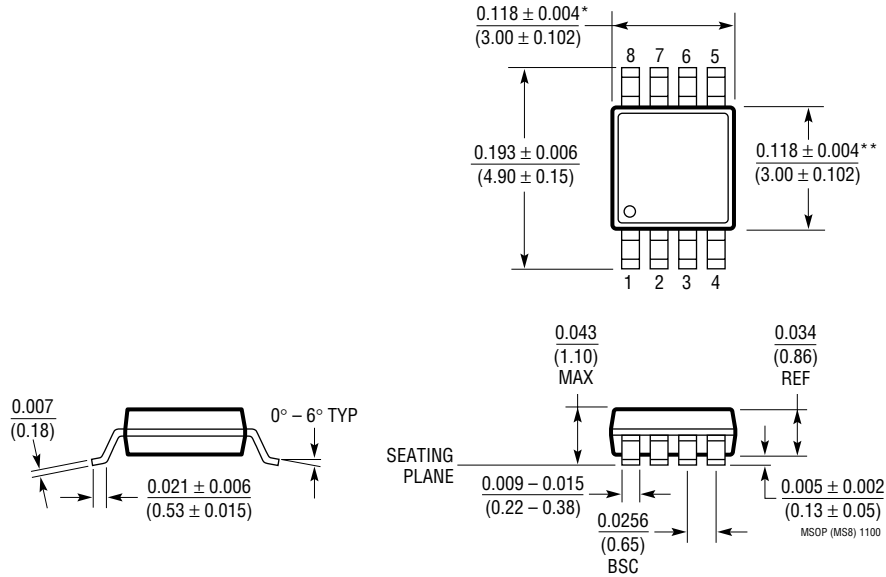


- NOTE:
1. DIMENSIONS ARE IN MILLIMETERS
  2. DIMENSIONS ARE INCLUSIVE OF PLATING
  3. DIMENSIONS ARE EXCLUSIVE OF MOLD FLASH AND METAL BURR
  4. MOLD FLASH SHALL NOT EXCEED 0.254mm
  5. PACKAGE EIAJ REFERENCE IS SC-74A (EIAJ)

**PACKAGE DESCRIPTION**

Dimensions in inches (millimeters) unless otherwise noted.

**MS8 Package**  
**8-Lead Plastic MSOP**  
 (LTC DWG # 05-08-1660)

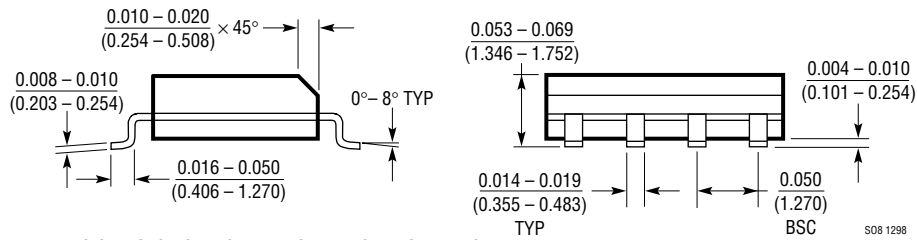
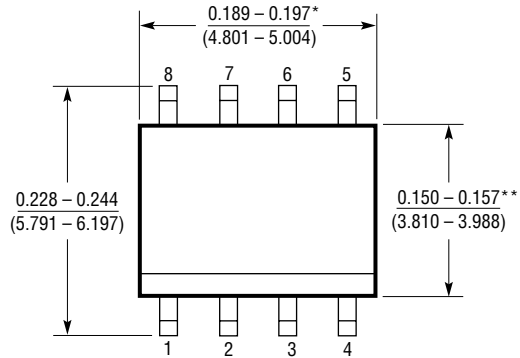


\* DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

\*\* DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS. INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

**PACKAGE DESCRIPTION** Dimensions in inches (millimeters) unless otherwise noted.

**S8 Package**  
**8-Lead Plastic Small Outline (Narrow 0.150)**  
 (LTC DWG # 05-08-1610)



\*DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE  
 \*\*DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

## TYPICAL APPLICATION

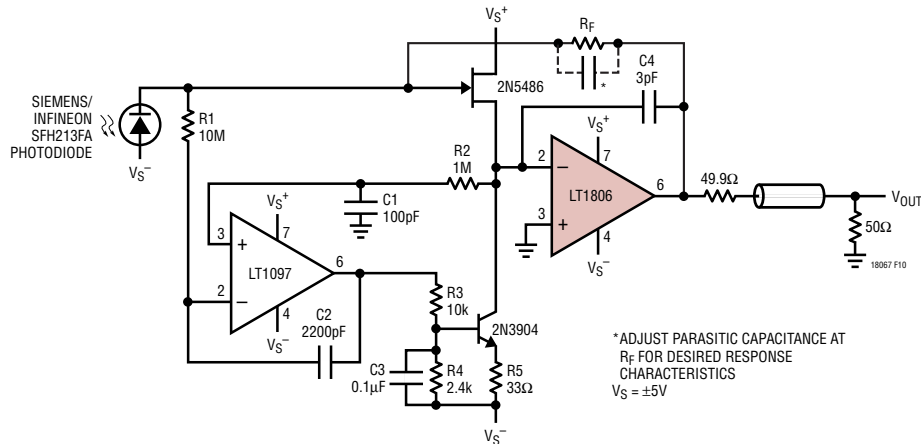
### FET Input, Fast, High Gain Photodiode Amplifier

Figure 10 shows a fast, high gain transimpedance amplifier applied to a photodiode. A JFET buffer is used for its extremely low input bias current and high speed. The LT1097 and 2N3904 keep the JFET biased at  $I_{DSS}$  for zero offset and lowest voltage noise. The JFET then drives the LT1806, with  $R_F$  closing the high speed loop back to the JFET input and setting the transimpedance gain.  $C_4$  helps improve the phase margin of the fast loop. Output voltage noise density was measured as  $9nV/\sqrt{Hz}$  with  $R_F$  short circuited. With  $R_F$  varied from 100k to 1M, total output

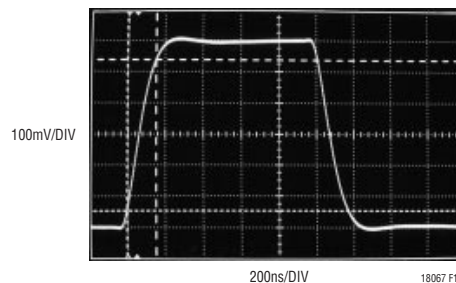
noise was below  $1mV_{RMS}$  measured over a 10MHz bandwidth. Table 4 shows results achieved with various values of  $R_F$  and Figure 11 shows the time domain response with  $R_F = 499k$ .

**Table 4. Results Achieved for Various  $R_F$ , 1.2V Output Step**

$R_F$	10% to 90% RISE TIME	-3dB BANDWIDTH
100k	64ns	6.8MHz
200k	94ns	4.6MHz
499k	154ns	3MHz
1M	263ns	1.8MHz



**Figure 10. Fast, High Gain Photodiode Amplifier**



**Figure 11. Step Response with  $R_F = 499k$**

## RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1395	400MHz Current Feedback Amplifier	800V/ $\mu$ s Slew Rate, Shutdown
LT1399	Triple 300MHz Current Feedback Amplifier	0.1dB Gain Flatness to 150MHz, Shutdown
LT1632/LT1633	Dual/Quad 45MHz, 45V/ $\mu$ s Rail-to-Rail Input and Output Amplifiers	High DC Accuracy 1.35mV $V_{OS(MAX)}$ , 70mA Output Current, Max Supply Current 5.2mA/Amp
LT1809/LT1810	Single/Dual 180MHz Input and Output Rail-to-Rail Amplifiers	350V/ $\mu$ s Slew Rate, Shutdown, Low Distortion -90dBc at 5MHz