Preferred Device

Advance Information

Power MOSFET 13 Amps, 100 Volts N-Channel Enhancement-Mode TO-220

Features

- Source-to-Drain Diode Recovery Time Comparable to a Discrete Fast Recovery Diode
- Avalanche Energy Specified
- I_{DSS} and $R_{DS(on)}$ Specified at Elevated Temperature

Typical Applications

- PWM Motor Controls
- Power Supplies
- Converters

MAXIMUM RATINGS ($T_C = 25^{\circ}C$ unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-to-Source Voltage	V _{DSS}	100	Vdc
Drain-to-Source Voltage (R_{GS} = 1.0 M Ω)	V _{DGR}	100	Vdc
Gate–to–Source Voltage – Continuous – Non–Repetitive (t _p ≤10 ms)	V _{GS} V _{GSM}	$\begin{array}{c} \pm20\\ \pm30 \end{array}$	Vdc
Drain Current – Continuous @ T _A 25°C – Continuous @ T _A 100°C – Pulsed (Note 1.)	I _D I _D I _{DM}	13 8.0 39	Adc
Total Power Dissipation @ T _A = 25°C Derate above 25°C	P _D	64.7 0.43	W W/∘C
Operating and Storage Temperature Range	T _J , T _{stg}	–55 to +175	°C
$ Single Drain-to-Source Avalanche Energy - Starting T_J = 25^\circ C \\ (V_{DD} = 50 \text{ Vdc}, V_{GS} = 10 \text{ Vdc}, \\ I_L(pk) = 13 \text{ A}, L = 1.0 \text{ mH}, R_G = 25 \Omega) $	E _{AS}	85	mJ
Thermal Resistance – Junction–to–Case	$R_{ extsf{ heta}JC}$	2.32	°C/W
Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds	ΤL	260	°C

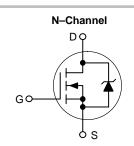
1. Pulse Test: Pulse Width = 10 μ s, Duty Cycle = 2%.



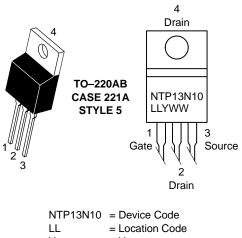
ON Semiconductor[™]

http://onsemi.com

13 AMPERES 100 VOLTS 165 mΩ @ V_{GS} = 10 V



MARKING DIAGRAM & PIN ASSIGNMENT



LL	= Location Co
Υ	= Year
WW	= Work Week

ORDERING INFORMATION

Device	Package	Shipping
NTP13N10	TO-220AB	50 Units/Rail

Preferred devices are recommended choices for future use and best overall value.

This document contains information on a new product. Specifications and information herein are subject to change without notice.

ELECTRICAL CHARACTERISTICS ($T_C = 25^{\circ}C$ unless otherwise noted)

Characteristic		Symbol	Min	Тур	Мах	Unit	
OFF CHARACTERISTICS							
Drain–to–Source Breakdown Volt (V _{GS} = 0 Vdc, I _D = 250 μAdc) Temperature Coefficient (Positive	5	V _(BR) DSS	100 -	_ 147		Vdc mV/°C	
Zero Gate Voltage Collector Curr ($V_{GS} = 0$ Vdc, $V_{DS} = 100$ Vdc, ($V_{GS} = 0$ Vdc, $V_{DS} = 100$ Vdc,	T _J = 25°C)	I _{DSS}			5.0 50	μAdc	
Gate-Body Leakage Current (VG	$_{\rm S} = \pm 20 \; {\rm Vdc}, \; {\rm V}_{\rm DS} = 0)$	I _{GSS}	-	-	±100	nAdc	
ON CHARACTERISTICS				•			
Gate Threshold Voltage $V_{DS} = V_{GS}$, $I_D = 250 \ \mu Adc$) Temperature Coefficient (Negativ	e)	V _{GS(th)}	2.0	3.2 -7.6	4.0	Vdc mV/°C	
$ Static Drain-to-Source On-State \\ (V_{GS} = 10 \ Vdc, \ I_D = 6.5 \ Adc) \\ (V_{GS} = 10 \ Vdc, \ I_D = 6.5 \ Adc, \ T_D $		R _{DS(on)}		0.130 0.250	0.165 0.400	Ω	
Drain–to–Source On–Voltage (V _{GS} = 10 Vdc, I _D = 13 Adc)		V _{DS(on)}	-	1.82	2.34	Vdc	
Forward Transconductance (V_{DS}	= 15 Vdc, I _D = 6.5 Adc)	9fs	-	6.0	-	mhos	
DYNAMIC CHARACTERISTICS							
Input Capacitance		C _{iss}	-	390	550	pF	
Output Capacitance	$(V_{DS} = 25 \text{ Vdc}, V_{GS} = 0 \text{ Vdc}, f = 1.0 \text{ MHz})$	Coss	-	115	160		
Reverse Transfer Capacitance		C _{rss}	-	35	70		
SWITCHING CHARACTERISTICS	(Notes 2. & 3.)				-		
Turn–On Delay Time		t _{d(on)}	-	11	20	ns	
Rise Time	$(V_{DD} = 80 \text{ Vdc}, I_D = 13 \text{ Adc},$	tr	-	40	80		
Turn-Off Delay Time	V_{GS} = 10 Vdc, R_{G} = 9.1 Ω)	t _{d(off)}	-	20	40		
Fall Time		t _f	-	36	70		
Gate Charge		Q _{tot}	-	14	20	nC	
	(V _{DS} = 80 Vdc, I _D = 13 Adc, V _{GS} = 10 Vdc)	Q _{gs}	-	3.0	-		
		Q _{gd}	-	7.0	-		
BODY-DRAIN DIODE RATINGS (Note 2.)						
Forward On–Voltage	$(I_{S} = 13 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $(I_{S} = 13 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 125^{\circ}\text{C})$	V _{SD}		0.98 0.88	1.3 -	Vdc	
Reverse Recovery Time	<i>"</i>	t _{rr}	-	85	_	ns	
	(I _S = 13 Adc, V _{GS} = 0 Vdc, dI _S /dt = 100 A/μs)	t _a	-	60	_]	
	U ·r··/	t.	_	28	_		

2. Indicates Pulse Test: P.W. = 300 µs max, Duty Cycle = 2%.

Reverse Recovery Stored Charge

3. Switching characteristics are independent of operating junction temperature.

28

0.3

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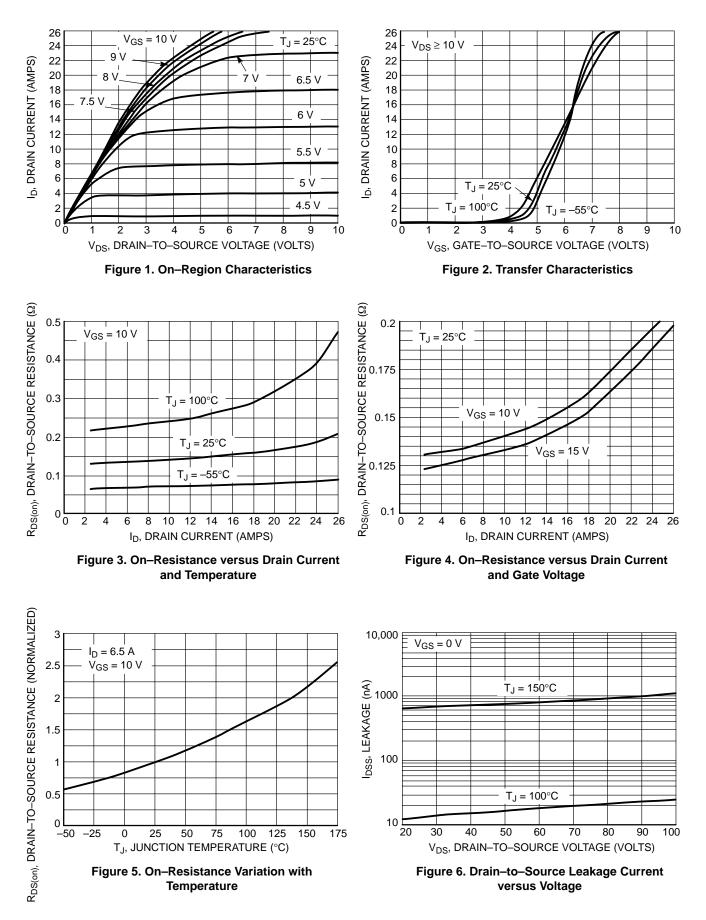
μC

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t_b

 $\mathsf{Q}_{\mathsf{R}\mathsf{R}}$



POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$

During the rise and fall time interval when switching a resistive load, V_{GS} remains virtually constant at a level known as the plateau voltage, V_{SGP} . Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 x R_G / (V_{GG} - V_{GSP})$ $t_f = Q_2 x R_G / V_{GSP}$

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG}

 R_G = the gate drive resistance

and Q_2 and V_{GSP} are read from the gate charge curve.

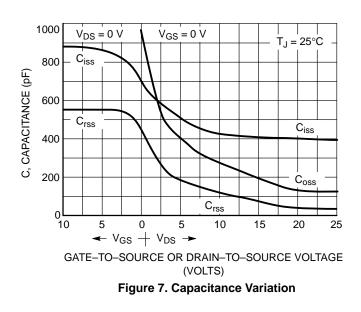
During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

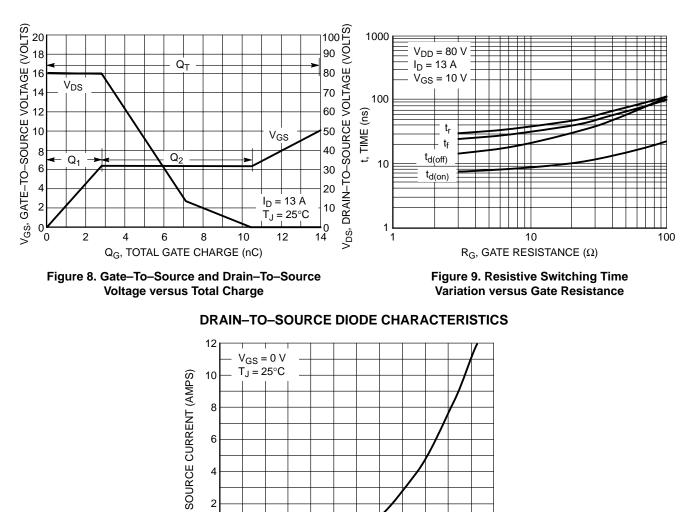
$$\begin{split} t_{d(on)} &= R_G \; C_{iss} \; In \; [V_{GG}/(V_{GG}-V_{GSP})] \\ t_{d(off)} &= R_G \; C_{iss} \; In \; (V_{GG}/V_{GSP}) \end{split}$$

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.





SAFE OPERATING AREA

0.7

V_{SD}, SOURCE-TO-DRAIN VOLTAGE (VOLTS) Figure 10. Diode Forward Voltage versus Current

0.8

0.9

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures "Transient discussed in AN569, Thermal Resistance-General Data and Its Use."

2

0 0.4

0.5

0.6

<u>ن</u>

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (IDM) nor rated voltage (VDSS) is exceeded and the transition time (t_r, t_f) do not exceed 10 µs. In addition the total power averaged over a complete switching cycle must not exceed $(T_{J(MAX)} - T_C)/(R_{\theta JC})$.

A Power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current (IDM), the energy rating is specified at rated continuous current (I_D), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 12). Maximum energy at currents below rated continuous ID can safely be assumed to equal the values indicated.

SAFE OPERATING AREA

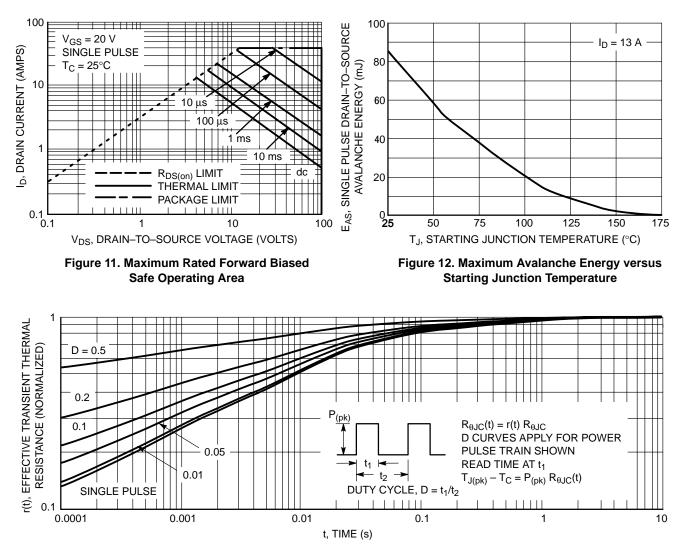


Figure 13. Thermal Response

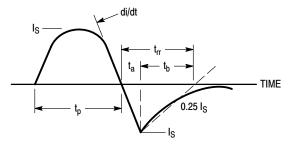
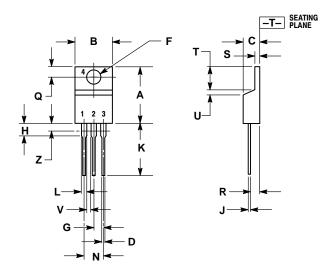


Figure 14. Diode Reverse Recovery Waveform

PACKAGE DIMENSIONS

TO-220 THREE-LEAD TO-220AB CASE 221A-09 **ISSUE AA**



NOTES: 1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982. 2. CONTROLLING DIMENSION: INCH. 3. DIMENSION Z DEFINES A ZONE WHERE ALL BODY AND LEAD IRREGULARITIES ARE ALLOWED.

	INCHES		MILLIMETER	
DIM	MIN	MAX	MIN	MAX
Α	0.570	0.620	14.48	15.75
В	0.380	0.405	9.66	10.28
С	0.160	0.190	4.07	4.82
D	0.025	0.035	0.64	0.88
F	0.142	0.147	3.61	3.73
G	0.095	0.105	2.42	2.66
Η	0.110	0.155	2.80	3.93
J	0.018	0.025	0.46	0.64
Κ	0.500	0.562	12.70	14.27
L	0.045	0.060	1.15	1.52
Ν	0.190	0.210	4.83	5.33
Q	0.100	0.120	2.54	3.04
R	0.080	0.110	2.04	2.79
S	0.045	0.055	1.15	1.39
Т	0.235	0.255	5.97	6.47
U	0.000	0.050	0.00	1.27
۷	0.045		1.15	
Ζ		0.080		2.04

STYLE 5: PIN 1. GATE 2. DRAIN 3. SOURCE 4. DRAIN

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