## DATA SHEET

## UBA2021 <br> 630 V driver IC for CFL and TL lamps

Product specification
Supersedes data of 2001 Jan 30

## FEATURES

- Adjustable preheat and ignition time
- Adjustable preheat current
- Adjustable lamp power
- Lamp temperature stress protection at higher mains voltages
- Capacitive mode protection
- Protection against a too-low drive voltage for the power MOSFETs.


## GENERAL DESCRIPTION

The UBA2021 is a high-voltage IC intended to drive and control Compact Fluorescent Lamps (CFL) or fluorescent TL-lamps. It contains a driver circuit for an external half-bridge, an oscillator and a control circuit for starting up, preheating, ignition, lamp burning and protection.

## QUICK REFERENCE DATA

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High voltage supply |  |  |  |  |  |  |
| $\mathrm{V}_{\text {FS }}$ | high side supply voltage | $\mathrm{I}_{\text {FS }}<15 \mu \mathrm{~A} ; \mathrm{t}<0.5 \mathrm{~s}$ | - | - | 630 | V |
| Start-up state |  |  |  |  |  |  |
| $\mathrm{V}_{\text {VS(start) }}$ | oscillator start voltage |  | - | 11.95 | - | V |
| $\mathrm{V}_{\mathrm{VS} \text { (stop) }}$ | oscillator stop voltage |  | - | 10.15 | - | V |
| $\mathrm{I}_{\mathrm{VS} \text { (standby) }}$ | standby current | $\mathrm{V}_{\mathrm{Vs}}=11 \mathrm{~V}$ | - | 200 | - | $\mu \mathrm{A}$ |
| Preheat mode |  |  |  |  |  |  |
| $\mathrm{f}_{\text {start }}$ | start frequency |  | - | 108 | - | kHz |
| $\mathrm{t}_{\mathrm{ph}}$ | preheat time | $\mathrm{C}_{\mathrm{CP}}=100 \mathrm{nF}$ | - | 666 | - | ms |
| $\mathrm{V}_{\text {RS(ctrl) }}$ | control voltage at pin RS |  | - | -600 | - | mV |
| Frequency sweep to ignition |  |  |  |  |  |  |
| $\mathrm{f}_{\mathrm{B}}$ | bottom frequency |  | - | 42.9 | - | kHz |
| $\mathrm{t}_{\text {ign }}$ | ignition time |  | - | 625 | - | ms |
| Normal operation |  |  |  |  |  |  |
| $\mathrm{f}_{\mathrm{B}}$ | bottom frequency |  | - | 42.9 | - | kHz |
| $\mathrm{t}_{\mathrm{no}}$ | non-overlap time |  | - | 1.4 | - | $\mu \mathrm{s}$ |
| $\mathrm{I}_{\text {tot }}$ | total supply current | $\mathrm{f}_{\mathrm{B}}=43 \mathrm{kHz}$ | - | 1 | - | mA |
| $\mathrm{R}_{\mathrm{G}_{1} \text { (on), },} \mathrm{R}_{\mathrm{G} 2 \text { (on) }}$ | high and low side on resistance |  | - | 126 | - | $\Omega$ |
| $\mathrm{R}_{\mathrm{G1} \text { (off), }}, \mathrm{R}_{\mathrm{G} 2 \text { (off) }}$ | high and low side off resistance |  | - | 75 | - | $\Omega$ |
| Feed-forward |  |  |  |  |  |  |
| fff | feed-forward frequency | $\mathrm{I}_{\mathrm{RHV}}=0.75 \mathrm{~mA}$ | - | 63.6 | - | kHz |
|  |  | $\mathrm{I}_{\mathrm{RHV}}=1.0 \mathrm{~mA}$ | - | 84.5 | - | kHz |
| $\mathrm{l}_{\text {(RHV) }}$ | operating range of input current at pin RHV |  | 0 | - | 1000 | $\mu \mathrm{A}$ |

## 630 V driver IC for CFL and TL lamps

UBA2021

ORDERING INFORMATION

| TYPE NUMBER | PACKAGE |  |  |
| :--- | :---: | :--- | :---: |
|  | NAME | DESCRIPTION | VERSION |
| UBA2021T | SO14 | plastic small outline package; 14 leads; body width 3.9 mm | SOT108-1 |
| UBA2021P | DIP14 | plastic dual in-line package; 14 leads (300 mil) | SOT27-1 |

## BLOCK DIAGRAM



Fig. 1 Block diagram.

## 630 V driver IC for CFL and TL lamps

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PINNING

| SYMBOL | PIN |  |
| :--- | :---: | :--- |
| FS | 1 | high side floating supply voltage |
| G1 | 2 | gate high transistor (T1) |
| S1 | 3 | source high transistor (T1) |
| n.c. | 4 | high-voltage spacer, not to be connected |
| VS | 5 | low voltage supply |
| G2 | 6 | gate low transistor (T2) |
| PGND | 7 | power ground |
| CP | 8 | timing/averaging capacitor |
| RS | 9 | current monitoring input |
| RREF | 10 | reference resistor |
| SGND | 11 | signal ground |
| CF | 13 | oscillator capacitor |
| RHV | 14 | start-up resistor/feed-forward resistor |
| CI | integrating capacitor |  |



Fig. 2 Pin configuration (SO14).


Fig. 3 Pin configuration (DIP14).

## FUNCTIONAL DESCRIPTION

## Introduction

The UBA2021 is an integrated circuit for electronically ballasted compact fluorescent lamps and their derivatives operating with mains voltages up to 240 V (RMS). It provides all the necessary functions for preheat, ignition and on-state operation of the lamp. In addition to the control function, the IC provides level shift and drive functions for the two discrete power MOSFETs, T1 and T2 (see Fig.7).

## Initial start-up

Initial start-up is achieved by charging capacitor CS9 with the current applied to pin RHV. At start-up, MOSFET T2 conducts and T 1 is non-conducting, ensuring $\mathrm{C}_{\mathrm{boot}}$ becomes charged. This start-up state is reached for a supply voltage $\mathrm{V}_{\mathrm{VS} \text { (reset) }}$ (this is the voltage level at pin VS at which the circuit will be reset to the initial state) and maintained until the low voltage supply ( $\mathrm{V}_{\mathrm{Vs}}$ ) reaches a value of $\mathrm{V}_{\mathrm{VS}}$ (start). The circuit is reset in the start-up state.

## Oscillation

When the low voltage supply ( $\mathrm{V}_{\mathrm{VS}}$ ) has reached the value of $\mathrm{V}_{\mathrm{VS} \text { (start) }}$ the circuit starts oscillating in the preheat state. The internal oscillator is a current-controlled circuit which generates a sawtooth waveform. The frequency of the sawtooth is determined by the capacitor $\mathrm{C}_{\mathrm{CF}}$ and the current out of pin CF (mainly set by $\mathrm{R}_{\text {RREF }}$ ). The sawtooth frequency is twice the frequency of the signal across the load. The IC brings MOSFETs T1 and T2 alternately into conduction with a duty factor of approximately $50 \%$. Figure 4 represents the timing of the IC. The circuit block 'non-overlap' generates a non-overlap time $\mathrm{t}_{\mathrm{no}}$ that ensures conduction periods of exclusively T1 or T2. Time $t_{n o}$ is dependent on the reference current I IREFF.


Fig. 4 Oscillator timing.

## Operation in the preheat mode

The circuit starts oscillating at approximately $2.5 \times f_{B}$ ( 108 kHz ). The frequency gradually decreases until a defined value of current $I_{\text {shunt }}$ is reached (see Fig.5). The slope of the decrease in frequency is determined by capacitor $\mathrm{C}_{\mathrm{CI}}$. The frequency during preheating is approximately 90 kHz . This frequency is well above the resonant frequency of the load, which means that the lamp is off; the load consists of L2, C5 and the electrode resistance only. The preheat time is determined by capacitor $\mathrm{C}_{\mathrm{CP}}$. The circuit can be locked in the preheat state by connecting pin CP to ground. During preheating, the circuit monitors the load current by measuring the voltage drop over external resistor $\mathrm{R}_{\text {shunt }}$ at the end of conduction of T 2 with decision level $\mathrm{V}_{\mathrm{RS}(\text { ctrl) }}$. The frequency is decreased as long as $\mathrm{V}_{\mathrm{RS}}>\mathrm{V}_{\mathrm{RS}(\text { ctrl) }}$. The frequency is increased for $\mathrm{V}_{\mathrm{RS}}<\mathrm{V}_{\mathrm{RS}(\text { (ctr) }}$.


Fig. 5 Operation in the preheat mode.

## Ignition state

The RS monitoring function changes from $\mathrm{V}_{\mathrm{RS} \text { (ctrl) }}$ regulation to capacitive mode protection at the end of the preheat time. Normally this results in a further frequency decrease down to the bottom frequency $f_{B}$ (approximately 43 kHz ). The rate of change of frequency in the ignition state is less than that in the preheat mode. During the downward frequency sweep, the circuit sweeps through the resonant frequency of the load. A high voltage then appears across the lamp. This voltage normally ignites the lamp.

## Failure to ignite

Excessive current levels may occur if the lamp fails to ignite. The IC does not limit these currents in any manner.

## Transition to the burn state

Assuming that the lamp has ignited during the downward frequency sweep, the frequency normally decreases to the bottom frequency. The IC can transit to the burn state in two ways:

1. In the event that the bottom frequency is not reached, transition is made after reaching the ignition time tign.
2. As soon as the bottom frequency is reached.

The bottom frequency is determined by $\mathrm{R}_{\text {RREF }}$ and $\mathrm{C}_{\mathrm{CF}}$.

## Feed-forward frequency

Above a defined voltage level the oscillation frequency also depends on the supply voltage of the half-bridge (see Fig.6). The current for the current-controlled oscillator is in the feed-forward range derived from the current through $R_{R H V}$. The feed-forward frequency is proportional to the average value of the current through $\mathrm{R}_{\mathrm{RHV}}$ within the operating range of $\mathrm{I}_{\mathrm{i}(\mathrm{RHV})}$, given the lower limit set by $\mathrm{f}_{\mathrm{B}}$. For currents beyond the operating range (i.e. between 1.0 and 1.6 mA ) the feed-forward frequency is clamped. In order to prevent feed-forward of ripple on $V_{\text {in }}$, the ripple is filtered out. The capacitor connected to pin CP is used for this purpose. This pin is also used in the preheat state and the ignition state for timing ( $\mathrm{t}_{\mathrm{ph}}$ and $\mathrm{t}_{\mathrm{ign}}$ ).


## Capacitive mode protection

When the preheat mode is completed, the IC will protect the power circuit against losing the zero voltage switching condition and getting too close to the capacitive mode of operation. This is detected by monitoring voltage $\mathrm{V}_{\mathrm{RS}}$ at pin RS. If the voltage is below $\mathrm{V}_{\mathrm{RS}(\text { cap })}$ at the time of turn-on of T 2 , then capacitive mode operation is assumed. Consequently the frequency increases as long as the capacitive mode is detected. The frequency decreases down to the feed-forward frequency if no capacitive mode is detected. Frequency modulation is achieved via pin Cl .

## IC supply

Initially, the IC is supplied from $\mathrm{V}_{\text {in }}$ by the current through $R_{\text {RHV }}$. This current charges the supply capacitor CS9 via an internal diode. As soon as $\mathrm{V}_{\mathrm{Vs}}$ exceeds $\mathrm{V}_{\mathrm{Vs} \text { (start) }}$, the circuit starts oscillating. After the preheat phase is finished, pin RHV is connected to an internal resistor $\mathrm{R}_{\mathrm{i}(\mathrm{RHV}) \text {; prior }}$ to this, pin RHV is internally connected to pin VS. The voltage level at pin RHV thus drops from $\mathrm{V}_{\text {Vs }}+\mathrm{V}_{\text {diode }}$ to $\mathrm{I}_{\mathrm{RHV}} \times \mathrm{R}_{\mathrm{i}(\mathrm{RHV})}$. The capacitor CS9 at pin VS will now be charged via the snubber capacitor CS7. Excess charge is drained by an internal clamp that turns on at voltage $\mathrm{V}_{\mathrm{VS} \text { (clamp) }}$.

## Minimum gate-source voltage of T1 and T2

The high side driver is supplied via capacitor $\mathrm{C}_{\text {boot }}$. Capacitor $\mathrm{C}_{\text {boot }}$ is charged via the bootstrap switch during the on-periods of T2. The IC stops oscillating at a voltage level $\mathrm{V}_{\mathrm{VS}(\text { stop) })}$. Given a maximum charge consumption on the load at pin G 1 of $1 \mathrm{nC} / \mathrm{V}$, this safeguards the minimum drive voltages $\mathrm{V}_{(\mathrm{G} 1-\mathrm{S} 1)}$ for the high side driver; see Table 1.

Table 1 Minimum gate-source voltages

| FREQUENCY | VOLTAGE |
| :---: | :---: |
| $<75 \mathrm{kHz}$ | 8 V (min.) |
| 75 kHz to 85 kHz | 7 V (min.) |
| $\geq 85 \mathrm{kHz}$ | 6 V (min.) |

The drive voltage at G 2 will exceed the drive voltage of the high side driver.

## Frequency and change in frequency

At any point in time during oscillation, the circuit will operate between $f_{B}$ and $f_{s t a r t}$. Any change in frequency will be gradual, no steps in frequency will occur. Changes in frequency caused by a change in voltage at pin Cl show a rather-constant df/dt over the entire frequency range. The following rates are realised (at a frequency of 85 kHz and with a 100 nF capacitor connected to pin CI ):

- For any increase in frequency: df/dt is between 15 and $37.5 \mathrm{kHz} / \mathrm{ms}$
- During preheat and normal operation: df/dt for a decrease in frequency is between -6 and $-15 \mathrm{kHz} / \mathrm{ms}$
- During the ignition phase: $\mathrm{dt} / \mathrm{dt}$ for a decrease in frequency is between -150 and $-375 \mathrm{~Hz} / \mathrm{ms}$.


## Ground pins

Pin PGND is the ground reference of the IC with respect to the application. As an exception, pin SGND provides a local ground reference for the components connected to pins CP, CI, RREF and CF. For this purpose pins PGND and SGND are short-circuited internally. External connection of pins PGND and SGND is not preferred. The sum of currents flowing out of the pins CP, CI, RREF, CF and SGND must remain zero at any time.

## Charge coupling

Due to parasitic capacitive coupling to the high voltage circuitry, all pins are burdened with a repetitive charge injection. Given the typical application in Fig.7, pins RREF and CF are sensitive to this charge injection. For the rating $Q_{\text {couple }}$ a safe functional operation of the IC is guaranteed, independent of the current level. Charge coupling at current levels below $50 \mu \mathrm{~A}$ will not interfere with the accuracy of the $\mathrm{V}_{\mathrm{RS}(\text { cap })}$ and $\mathrm{V}_{\mathrm{RS} \text { (ctrl) }}$ levels. Charge coupling at current levels below $20 \mu \mathrm{~A}$ will not interfere with the accuracy of any parameter.

## 630 V driver IC for CFL and TL lamps

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## LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 60134); all voltages referenced to ground.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | MAX. | UNIT |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{V}_{\text {FS }}$ | high side floating supply voltage | operating | - | 570 | V |
|  |  | $\mathrm{t} \leq 0.5 \mathrm{~s}$ | - | 630 | V |
| $\mathrm{I}_{\text {VS(clamp) }}$ | clamp current | $\mathrm{t} \leq 0.5 \mathrm{~s}$ | - | 35 | mA |
| $\mathrm{~V}_{\mathrm{RS}}$ | input voltage pin RS |  | -2.5 | +2.5 | V |
|  |  | transient of 50 ns | -15.0 | +2.5 | V |
| SR | slew rate at pins S1, G1 and FS <br> (with respect to ground) |  | -4 | +4 | $\mathrm{~V} / \mathrm{ns}$ |
| P | power dissipation |  | - | 500 | mW |
| $\mathrm{~T}_{\text {amb }}$ | ambient temperature |  | -40 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}$ | junction temperature |  | -40 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {stg }}$ | storage temperature |  | -55 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{Q}_{\text {couple }}$ | charge coupling at pins RREF and CF | operating | -8 | +8 | pC |
| $\mathrm{V}_{\text {es }}$ | electrostatic handling voltage | human body model; note 1 | - | 3000 | V |
|  |  | machine model; note 2 | - | 300 | V |

## Notes

1. Human body model: all pins are 3000 V maximum, except pins FS, G1, S1 and VS which are 1500 V maximum and pin G2 which is 1000 V maximum.
2. Machine model: all pins are 300 V maximum, except pin G 2 which is 125 V maximum.

THERMAL CHARACTERISTICS

| SYMBOL | PARAMETER | CONDITIONS | VALUE | UNIT |
| :--- | :--- | :--- | :---: | :---: |
| $R_{\text {th(j-a) }}$ | thermal resistance from junction to ambient | in free air |  |  |
|  | SO14 |  | 100 | K/W |
|  | DIP14 |  | 60 | K/W |
| $\mathrm{R}_{\text {th(j-pin) }}$ | thermal resistance from junction to pcb | in free air | 50 | K/W |
|  | SO14 |  | 30 | K/W |

## QUALITY SPECIFICATION

In accordance with "SNW-FQ-611-E".

## CHARACTERISTICS

$\mathrm{V}_{\mathrm{VS}}=11 \mathrm{~V} ; \mathrm{V}_{\mathrm{FS}}-\mathrm{V}_{\mathrm{S} 1}=11 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; all voltages referenced to ground; see Fig.7; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| High voltage supply |  |  |  |  |  |  |
| IL | leakage current on high voltage pins | $\mathrm{V}_{\mathrm{FS}}, \mathrm{V}_{\mathrm{G} 1}$ and $\mathrm{V}_{\mathrm{S} 1}=630 \mathrm{~V}$ | - | - | 15 | $\mu \mathrm{A}$ |
| Start-up state |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{VS} \text { (reset) }}$ | reset voltage | T1 off; T2 on | 4.0 | 5.5 | 6.5 | V |
| $\mathrm{V}_{\text {VS(start) }}$ | oscillator start voltage |  | 11.35 | 11.95 | 12.55 | V |
| $\mathrm{V}_{\text {VS(stop) }}$ | oscillator stop voltage |  | 9.55 | 10.15 | 10.75 | V |
| $\mathrm{V}_{\mathrm{VS} \text { (hys) }}$ | supply voltage hysteresis |  | 1.5 | 1.8 | 2.0 | V |
| IVS(standby) | standby supply current at pin VS | $\mathrm{V}_{\text {Vs }}=11 \mathrm{~V}$; note 1 | 150 | 200 | 250 | $\mu \mathrm{A}$ |
| $\Delta \mathrm{V}_{\text {(RHV-VS) }}$ | voltage difference between pins RHV and VS | $\mathrm{I}_{\mathrm{RHV}}=1.0 \mathrm{~mA}$ | 0.7 | 0.8 | 1.0 | V |
| $\mathrm{V}_{\mathrm{VS} \text { (clamp-start) }}$ | clamp margin $\mathrm{V}_{\mathrm{VS} \text { (clamp) }}$ to $\mathrm{V}_{\mathrm{VS} \text { (start) }}$ | note 2 | 0.2 | 0.3 | 0.4 | V |
| IVs(clamp) | clamp current | $\mathrm{V}_{\mathrm{vs}}<17 \mathrm{~V}$ | - | 14 | 35 | mA |
| Preheat mode |  |  |  |  |  |  |
| $\mathrm{f}_{\text {start }}$ | starting frequency | $\mathrm{V}_{\mathrm{CI}}=0 \mathrm{~V}$ | 98 | 108 | 118 | kHz |
| $\mathrm{t}_{\mathrm{g}}$ | conducting time T1 and T2 | $\mathrm{f}_{\text {start }}=108 \mathrm{kHz}$ | - | 3.2 | - | $\mu \mathrm{s}$ |
| $\mathrm{I}_{\mathrm{Cl} \text { (charge) }}$ | charge current at pin Cl | $\mathrm{V}_{\mathrm{CI}}=1.5 \mathrm{~V} ; \mathrm{V}_{\mathrm{RS}}=-0.3 \mathrm{~V}$ | 38 | 44 | 50 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {CI (discharge) }}$ | discharge current at pin Cl | $\mathrm{V}_{\mathrm{CI}}=1.5 \mathrm{~V} ; \mathrm{V}_{\mathrm{RS}}=-0.9 \mathrm{~V}$ | 79 | 93 | 107 | $\mu \mathrm{A}$ |
| $\mathrm{t}_{\mathrm{ph}}$ | preheat time |  | 599 | 666 | 733 | ms |
| $\mathrm{I}_{\text {CP(charge) }}$ | charge current at pin CP | $\mathrm{V}_{\mathrm{CP}}=1 \mathrm{~V}$ | - | 6.0 | - | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {CP(discharge) }}$ | discharge current at pin CP | $\mathrm{V}_{\mathrm{CP}}=1 \mathrm{~V}$ | - | 5.95 | - | $\mu \mathrm{A}$ |
| $\Delta \mathrm{V}_{\mathrm{CP}(\mathrm{pk})}$ | peak voltage difference at pin CP | when timing | - | 2.5 | - | V |
| $\mathrm{V}_{\text {RS(ctrl) }}$ | control voltage at pin RS | note 3 | -636 | -600 | -564 | mV |

## Frequency sweep to ignition

| $\mathrm{I}_{\mathrm{Cl}(\text { charge })}$ | charge current at pin Cl | $\mathrm{V}_{\mathrm{CI}}=1.5 \mathrm{~V} ; \mathrm{f} \approx 85 \mathrm{kHz}$ | 0.8 | 1.0 | 1.2 | $\mu \mathrm{~A}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{f}_{\mathrm{B}}$ | bottom frequency | $\mathrm{V}_{\mathrm{CI}}$ at clamp level | - | 42.9 | - | kHz |
| $\mathrm{t}_{\text {ign }}$ | ignition time |  | - | 625 | - | ms |

## Normal operation

| $\mathrm{f}_{\mathrm{B}}$ | bottom frequency |  | 41.21 | 42.90 | 44.59 | kHz |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{t}_{\mathrm{g}}$ | conducting time T1 and T2 | $\mathrm{f}_{\mathrm{B}}=43 \mathrm{kHz}$ | - | 10.2 | - | $\mu \mathrm{s}$ |
| $\mathrm{t}_{\mathrm{no}}$ | non-overlap conductance time |  | 1.05 | 1.4 | 1.75 | $\mu \mathrm{~s}$ |
| $\mathrm{I}_{\text {tot }}$ | total supply current | $\mathrm{f}_{\mathrm{B}}=43 \mathrm{kHz} ;$ note 4 | 0.85 | 1.0 | 1.1 | mA |
| $\mathrm{~V}_{\mathrm{RS} \text { (cap) }}$ | capacitive mode control voltage | note 5 | 0 | 20 | 40 | mV |
| $\mathrm{V}_{\mathrm{RREF}}$ | reference voltage | note 6 | 2.425 | 2.5 | 2.575 | V |
| $\mathrm{~V}_{\mathrm{G} 1 \text { (on) }}$ | on voltage at pin G 1 | $\left\|\mathrm{I}_{\mathrm{G} 1}\right\|=1 \mathrm{~mA}$ | 10.5 | - | - | V |
| $\mathrm{V}_{\mathrm{G} 1 \text { (off) }}$ | off voltage at pin G 1 | $\left\|\mathrm{I}_{\mathrm{G} 1}\right\|=1 \mathrm{~mA}$ | - | - | 0.3 | V |
| $\mathrm{~V}_{\mathrm{G} 2 \text { (on) }}$ | on voltage at pin G 2 | $\left\|\mathrm{I}_{\mathrm{G} 2}\right\|=1 \mathrm{~mA}$ | 10.5 | - | - | V |
| $\mathrm{V}_{\mathrm{G} 2 \text { (off) }}$ | off voltage at pin G 2 | $\mathrm{I}_{\mathrm{G} 2} \mid=1 \mathrm{~mA}$ | - | - | 0.3 | V |
| $\mathrm{R}_{\mathrm{G} 1 \text { (on) }}$ | high side driver on resistance | $\mathrm{V}_{(\mathrm{G} 1-\mathrm{S} 1)}=3 \mathrm{~V} ;$ note 7 | 100 | 126 | 152 | $\Omega$ |


| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{R}_{\mathrm{G1} \text { (off) }}$ | high side driver off resistance | $\mathrm{V}_{(\mathrm{G} 1-\mathrm{S} 1)}=3 \mathrm{~V}$; note 7 | 60 | 75 | 90 | $\Omega$ |
| $\mathrm{R}_{\mathrm{G} 2 \text { (on) }}$ | low side driver on resistance | $\mathrm{V}_{\mathrm{G} 2}=3 \mathrm{~V}$; note 7 | 100 | 126 | 152 | $\Omega$ |
| $\mathrm{R}_{\mathrm{G} 2 \text { (off) }}$ | low side driver off resistance | $\mathrm{V}_{\mathrm{G} 2}=3 \mathrm{~V}$; note 7 | 60 | 75 | 90 | $\Omega$ |
| $\mathrm{V}_{\text {drop }}$ | voltage drop at bootstrap switch | $\mathrm{I}_{\text {FS }}=5 \mathrm{~mA}$ | 0.6 | 1.0 | 1.4 | V |
| Feed-forward |  |  |  |  |  |  |
| $\mathrm{R}_{\mathrm{i} \text { (RHV) }}$ | input resistance at pin RHV |  | 1.54 | 2.2 | 2.86 | k $\Omega$ |
| $\mathrm{I}_{\text {( } \mathrm{RHV})}$ | operating range of input current at pin RHV | note 8 | 0 | - | 1000 | $\mu \mathrm{A}$ |
| fff | feed-forward frequency | $\mathrm{I}_{\mathrm{RHV}}=0.75 \mathrm{~mA}$ | 60.4 | 63.6 | 66.15 | kHz |
|  |  | $\mathrm{I}_{\mathrm{RHV}}=1 \mathrm{~mA}$ | 80.3 | 84.5 | 88.2 | kHz |
| $\mathrm{SYM}_{\mathrm{ff}}$ | symmetry | $\mathrm{I}_{\mathrm{RHV}}=1 \mathrm{~mA}$; note 9 | 0.9 | 1.0 | 1.1 |  |
| RR | ripple rejection | $\mathrm{f}_{\mathrm{Vin}}=100 \mathrm{~Hz}$ | - | 6 | - | dB |
| $\mathrm{R}_{\mathrm{CP} \text { (sw) }}$ | CP switch series resistance | $\mathrm{I}_{\mathrm{CP}}=100 \mu \mathrm{~A}$ | 0.75 | 1.5 | 2.25 | $\mathrm{k} \Omega$ |
| $\mathrm{R}_{\mathrm{AV}}$ | averaging resistor | $\mathrm{I}_{\mathrm{CP}}=10 \mu \mathrm{~A}$ | 22.4 | 32 | 41.6 | k $\Omega$ |

## Notes

1. The start-up supply current is specified in a temperature ( $\mathrm{T}_{\mathrm{vj}}$ ) range of 0 to $125^{\circ} \mathrm{C}$. For $\mathrm{T}_{\mathrm{vj}}<0$ and $\mathrm{T}_{\mathrm{vj}}>125^{\circ} \mathrm{C}$ the start-up supply current is $<350 \mu \mathrm{~A}$.
2. The clamp margin is defined as the voltage difference between turn-on of the clamp and start of oscillation. The clamp is in the off-state at start of oscillation.
3. Data sampling of $\mathrm{V}_{\mathrm{RS}(\text { ctrl) }}$ is performed at the end of conduction of T 2 .
4. The total supply current is specified in a temperature ( $\mathrm{T}_{\mathrm{vj}}$ ) range of -20 to $+125^{\circ} \mathrm{C}$. For $\mathrm{T}_{\mathrm{vj}}<-20$ and $\mathrm{T}_{\mathrm{vj}}>125^{\circ} \mathrm{C}$ the total supply current is $<1.5 \mathrm{~mA}$.
5. Data sampling of $\mathrm{V}_{\mathrm{RS} \text { (cap) }}$ is performed at the start of conduction of T 2 .
6. Within the allowed range of $R_{\text {RREF }}$, defined as $30 \mathrm{k} \Omega \pm 10 \%$.
7. Typical values for the on and off resistances at $\mathrm{T}_{\mathrm{vj}}=87.5^{\circ} \mathrm{C}$ are: $\mathrm{R}_{\mathrm{G} 2 \text { (on) }}$ and $\mathrm{R}_{\mathrm{G} 1 \text { (on) }}=164 \Omega, \mathrm{R}_{\mathrm{G} 2 \text { (off) }}$ and $R_{G 1 \text { (off) }}=100 \Omega$.
8. The input current at pin RHV may increase to $1600 \mu \mathrm{~A}$ during voltage transient at $\mathrm{V}_{\mathrm{in} \text {. }}$. Only for currents $\mathrm{I}_{\mathrm{RHV}}$ beyond approximately $550 \mu \mathrm{~A}$ is the oscillator frequency proportional to $I_{\mathrm{RHV}}$.
9. The symmetry $\mathrm{SYM}_{\mathrm{ff}}$ is calculated from the quotient $\mathrm{SYM}_{\mathrm{ff}}=\mathrm{T} 1_{\text {tot }} / T 2_{\text {tot }}$, with $\mathrm{T}_{\text {tot }}$ the time between turn-off of G 2 and turn-off of G1, and $\mathrm{T}_{\text {tot }}$ the time between turn-off of G 1 and turn-off of G 2 .

## 630 V driver IC for CFL and TL lamps

## DESIGN EQUATIONS

- Bottom frequency: $\mathrm{f}_{\mathrm{B}}=\frac{1}{2 \times\left\{\left[\left(\mathrm{C}_{\mathrm{CF}}+\mathrm{C}_{\mathrm{par}}\right) \times\left(\mathrm{X} 1 \times \mathrm{R}_{\mathrm{RREF}}-\mathrm{R}_{\mathrm{int}}\right)\right]+\tau\right\}}$
- Feed-forward frequency: $\mathrm{f}_{\mathrm{ff}}=\frac{1}{2 \times\left\{\left[\left(\mathrm{C}_{\mathrm{CF}}+\mathrm{C}_{\mathrm{par}}\right) \times\left(\frac{\mathrm{X} 2 \times \mathrm{V}_{\mathrm{RREF}}}{\mathrm{I}_{\mathrm{i}(\mathrm{RHV})}}-\mathrm{R}_{\mathrm{int}}\right)\right]+\tau\right\}}$

Where:

- X1 = 3.68
$-\mathrm{X} 2=22.28$
- $\tau=0.4 \mu \mathrm{~s}$
$-\mathrm{R}_{\mathrm{int}}=3 \mathrm{k} \Omega$
$-\mathrm{C}_{\mathrm{par}}=4.7 \mathrm{pF}$
- Operating frequency is the maximum of $\mathrm{f}_{\mathrm{B}}, \mathrm{f}_{\mathrm{ff}}$ or $\mathrm{f}_{\mathrm{cm}}$ Where:
- $f_{B}=$ bottom frequency
- $\mathrm{f}_{\mathrm{ff}}=$ feed-forward frequency
- $f_{c m}=$ frequency due to capacitive mode detection
- Preheat time: $\mathrm{t}_{\mathrm{ph}}=\frac{\mathrm{C}_{\mathrm{CP}}}{150 \mathrm{nF}} \times \frac{R_{\mathrm{RREF}}}{30 \mathrm{k} \Omega}$
- Ignition time: $\mathrm{t}_{\mathrm{ign}}=\frac{15}{16} \times \mathrm{t}_{\mathrm{ph}}$
- Non-overlap time: $\mathrm{t}_{\mathrm{no}}=1.4 \mu \mathrm{~s} \times \frac{\mathrm{R}_{\mathrm{RREF}}}{30 \mathrm{k} \Omega}$


## APPLICATION INFORMATION



Fig. 7 Application diagram.

## PACKAGE OUTLINES



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

| UNIT | $\underset{\max }{\mathrm{A}}$ | $\mathrm{A}_{1}$ | $\mathrm{A}_{2}$ | $\mathrm{A}_{3}$ | $\mathrm{b}_{\mathrm{p}}$ | c | $D^{(1)}$ | $E^{(1)}$ | e | $\mathrm{H}_{\mathrm{E}}$ | L | $\mathrm{L}_{\mathrm{p}}$ | Q | v | w | y | $\mathrm{Z}^{(1)}$ | $\theta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 1.75 | $\begin{aligned} & 0.25 \\ & 0.10 \end{aligned}$ | $\begin{aligned} & 1.45 \\ & 1.25 \end{aligned}$ | 0.25 | $\begin{aligned} & 0.49 \\ & 0.36 \end{aligned}$ | $\begin{aligned} & 0.25 \\ & 0.19 \end{aligned}$ | $\begin{aligned} & 8.75 \\ & 8.55 \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 3.8 \end{aligned}$ | 1.27 | $\begin{aligned} & 6.2 \\ & 5.8 \end{aligned}$ | 1.05 | $\begin{aligned} & 1.0 \\ & 0.4 \end{aligned}$ | $\begin{aligned} & 0.7 \\ & 0.6 \end{aligned}$ | 0.25 | 0.25 | 0.1 | $\begin{aligned} & 0.7 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 8^{\circ} \\ & 0^{\circ} \end{aligned}$ |
| inches | 0.069 | $\begin{aligned} & 0.010 \\ & 0.004 \end{aligned}$ | $\begin{aligned} & 0.057 \\ & 0.049 \end{aligned}$ | 0.01 | $\begin{aligned} & 0.019 \\ & 0.014 \end{aligned}$ | $\left.\begin{array}{\|l\|} 0.0100 \\ 0.0075 \end{array} \right\rvert\,$ | $\begin{aligned} & 0.35 \\ & 0.34 \end{aligned}$ | $\begin{aligned} & 0.16 \\ & 0.15 \end{aligned}$ | 0.050 | $\begin{aligned} & 0.244 \\ & 0.228 \end{aligned}$ | 0.041 | $\begin{aligned} & 0.039 \\ & 0.016 \end{aligned}$ | $\begin{aligned} & 0.028 \\ & 0.024 \end{aligned}$ | 0.01 | 0.01 | 0.004 | $\begin{aligned} & 0.028 \\ & 0.012 \end{aligned}$ |  |

Note

1. Plastic or metal protrusions of 0.15 mm maximum per side are not included.

| OUTLINE <br> VERSION | REFERENCES |  |  |  | EUROPEAN <br> PROJECTION | ISSUE DATE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IEC | JEDEC | EIAJ |  |  |  |
| SOT108-1 | $076 E 06$ | MS-012 |  |  | $-99-12-27$ |  |



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

| UNIT | $\underset{\max .}{A}$ | $\mathrm{A}_{1}$ min. | $\underset{\mathrm{A}_{2}}{ }$ max. | b | $\mathrm{b}_{1}$ | c | $D^{(1)}$ | $E^{(1)}$ | e | $\mathrm{e}_{1}$ | L | $\mathrm{M}_{\mathrm{E}}$ | $\mathbf{M}_{\mathbf{H}}$ | w | $\underset{\max }{\mathrm{Z}^{(1)}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 4.2 | 0.51 | 3.2 | $\begin{aligned} & 1.73 \\ & 1.13 \end{aligned}$ | $\begin{aligned} & 0.53 \\ & 0.38 \end{aligned}$ | $\begin{aligned} & 0.36 \\ & 0.23 \end{aligned}$ | $\begin{aligned} & 19.50 \\ & 18.55 \end{aligned}$ | $\begin{aligned} & 6.48 \\ & 6.20 \end{aligned}$ | 2.54 | 7.62 | $\begin{aligned} & 3.60 \\ & 3.05 \end{aligned}$ | $\begin{aligned} & 8.25 \\ & 7.80 \end{aligned}$ | $\begin{gathered} 10.0 \\ 8.3 \end{gathered}$ | 0.254 | 2.2 |
| inches | 0.17 | 0.020 | 0.13 | $\begin{aligned} & 0.068 \\ & 0.044 \end{aligned}$ | $\begin{aligned} & 0.021 \\ & 0.015 \end{aligned}$ | $\begin{aligned} & 0.014 \\ & 0.009 \end{aligned}$ | $\begin{aligned} & \hline 0.77 \\ & 0.73 \end{aligned}$ | $\begin{aligned} & 0.26 \\ & 0.24 \end{aligned}$ | 0.10 | 0.30 | $\begin{aligned} & \hline 0.14 \\ & 0.12 \end{aligned}$ | $\begin{aligned} & 0.32 \\ & 0.31 \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.33 \end{aligned}$ | 0.01 | 0.087 |

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

| OUTLINE <br> VERSION | REFERENCES |  |  |  | EUROPEAN <br> PROJECTION | ISSUE DATE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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| SOT27-1 | $050 G 04$ | MO-001 | SC-501-14 |  | - |  |

## SOLDERING

## Introduction

This text gives a very brief insight to a complex technology. A more in-depth account of soldering ICs can be found in our "Data Handbook IC26; Integrated Circuit Packages" (document order number 9398652 90011).

There is no soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and surface mount components are mixed on one printed-circuit board. Wave soldering can still be used for certain surface mount ICs, but it is not suitable for fine pitch SMDs. In these situations reflow soldering is recommended.

## Through-hole mount packages

## Soldering by dipping or by solder wave

The maximum permissible temperature of the solder is $260^{\circ} \mathrm{C}$; solder at this temperature must not be in contact with the joints for more than 5 seconds. The total contact time of successive solder waves must not exceed 5 seconds.

The device may be mounted up to the seating plane, but the temperature of the plastic body must not exceed the specified maximum storage temperature ( $\mathrm{T}_{\text {stg(max) }}$ ). If the printed-circuit board has been pre-heated, forced cooling may be necessary immediately after soldering to keep the temperature within the permissible limit.

## Manual soldering

Apply the soldering iron ( 24 V or less) to the lead(s) of the package, either below the seating plane or not more than 2 mm above it. If the temperature of the soldering iron bit is less than $300^{\circ} \mathrm{C}$ it may remain in contact for up to 10 seconds. If the bit temperature is between 300 and $400^{\circ} \mathrm{C}$, contact may be up to 5 seconds.

## Surface mount packages

## Reflow soldering

Reflow soldering requires solder paste (a suspension of fine solder particles, flux and binding agent) to be applied to the printed-circuit board by screen printing, stencilling or pressure-syringe dispensing before package placement.

Several methods exist for reflowing; for example, convection or convection/infrared heating in a conveyor type oven. Throughput times (preheating, soldering and cooling) vary between 100 and 200 seconds depending on heating method.

Typical reflow peak temperatures range from 215 to $250^{\circ} \mathrm{C}$. The top-surface temperature of the packages should preferable be kept below $220^{\circ} \mathrm{C}$ for thick/large packages, and below $235^{\circ} \mathrm{C}$ for small/thin packages.

## Wave soldering

Conventional single wave soldering is not recommended for surface mount devices (SMDs) or printed-circuit boards with a high component density, as solder bridging and non-wetting can present major problems.

To overcome these problems the double-wave soldering method was specifically developed.
If wave soldering is used the following conditions must be observed for optimal results:

- Use a double-wave soldering method comprising a turbulent wave with high upward pressure followed by a smooth laminar wave.
- For packages with leads on two sides and a pitch (e):
- larger than or equal to 1.27 mm , the footprint longitudinal axis is preferred to be parallel to the transport direction of the printed-circuit board;
- smaller than 1.27 mm , the footprint longitudinal axis must be parallel to the transport direction of the printed-circuit board.
The footprint must incorporate solder thieves at the downstream end.
- For packages with leads on four sides, the footprint must be placed at a $45^{\circ}$ angle to the transport direction of the printed-circuit board. The footprint must incorporate solder thieves downstream and at the side corners.

During placement and before soldering, the package must be fixed with a droplet of adhesive. The adhesive can be applied by screen printing, pin transfer or syringe dispensing. The package can be soldered after the adhesive is cured.

Typical dwell time is 4 seconds at $250^{\circ} \mathrm{C}$.
A mildly-activated flux will eliminate the need for removal of corrosive residues in most applications.

## MANUAL SOLDERING

Fix the component by first soldering two diagonally-opposite end leads. Use a low voltage ( 24 V or less) soldering iron applied to the flat part of the lead. Contact time must be limited to 10 seconds at up to $300^{\circ} \mathrm{C}$. When using a dedicated tool, all other leads can be soldered in one operation within 2 to 5 seconds between 270 and $320^{\circ} \mathrm{C}$.

Suitability of IC packages for wave, reflow and dipping soldering methods

| MOUNTING | PACKAGE ${ }^{(1)}$ | SOLDERING METHOD |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | WAVE | REFLOW ${ }^{(2)}$ | DIPPING |
| Through-hole mount | DBS, DIP, HDIP, SDIP, SIL | suitable ${ }^{(3)}$ | - | suitable |
| Surface mount | BGA, LBGA, LFBGA, SQFP, TFBGA, VFBGA <br> HBCC, HBGA, HLQFP, HSQFP, HSOP, <br> HTQFP, HTSSOP, HVQFN, HVSON, SMS <br> PLCC ${ }^{(5)}$, SO, SOJ <br> LQFP, QFP, TQFP <br> SSOP, TSSOP, VSO | not suitable <br> not suitable ${ }^{(4)}$ <br> suitable <br> not recommended ${ }^{(5)(6)}$ <br> not recommended ${ }^{(7)}$ | suitable <br> suitable <br> suitable <br> suitable <br> suitable | $-$ |

## Notes

1. For more detailed information on the BGA packages refer to the "(LF)BGA Application Note" (AN01026); order a copy from your Philips Semiconductors sales office.
2. All surface mount (SMD) packages are moisture sensitive. Depending upon the moisture content, the maximum temperature (with respect to time) and body size of the package, there is a risk that internal or external package cracks may occur due to vaporization of the moisture in them (the so called popcorn effect). For details, refer to the Drypack information in the "Data Handbook IC26; Integrated Circuit Packages; Section: Packing Methods".
3. For SDIP packages, the longitudinal axis must be parallel to the transport direction of the printed-circuit board.
4. These packages are not suitable for wave soldering. On versions with the heatsink on the bottom side, the solder cannot penetrate between the printed-circuit board and the heatsink. On versions with the heatsink on the top side, the solder might be deposited on the heatsink surface.
5. If wave soldering is considered, then the package must be placed at a $45^{\circ}$ angle to the solder wave direction. The package footprint must incorporate solder thieves downstream and at the side corners.
6. Wave soldering is suitable for LQFP, QFP and TQFP packages with a pitch (e) larger than 0.8 mm ; it is definitely not suitable for packages with a pitch (e) equal to or smaller than 0.65 mm .
7. Wave soldering is suitable for SSOP and TSSOP packages with a pitch (e) equal to or larger than 0.65 mm ; it is definitely not suitable for packages with a pitch (e) equal to or smaller than 0.5 mm .

## DATA SHEET STATUS

| DATA SHEET STATUS ${ }^{(1)}$ | PRODUCT <br> STATUS |  |
| :--- | :--- | :--- |
| Objective data | Development | DEFINITIONS |
| Preliminary data | This data sheet contains data from the objective specification for product <br> development. Philips Semiconductors reserves the right to change the <br> specification in any manner without notice. |  |
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## Notes

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## NOTES

## NOTES

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