# Sleep-Mode™ Two-State, Micropower Operational Amplifier

The MC33102 dual operational amplifier is an innovative design concept employing Sleep–Mode technology. Sleep–Mode amplifiers have two separate states, a sleepmode and an awakemode. In sleepmode, the amplifier is active and waiting for an input signal. When a signal is applied causing the amplifier to source or sink  $160~\mu A$  (typically) to the load, it will automatically switch to the awakemode which offers higher slew rate, gain bandwidth, and drive capability.

- Two States: "Sleepmode" (Micropower) and "Awakemode" (High Performance)
- Switches from Sleepmode to Awakemode in 4.0  $\mu$ s when Output Current Exceeds the Threshold Current ( $R_L = 600 \Omega$ )
- Independent Sleepmode Function for Each Op Amp
- Standard Pinouts No Additional Pins or Components Required
- Sleepmode State Can Be Used in the Low Current Idle State as a Fully Functional Micropower Amplifier
- Automatic Return to Sleepmode when Output Current Drops Below Threshold
- No Deadband/Crossover Distortion; as Low as 1.0 Hz in the Awakemode
- Drop-in Replacement for Many Other Dual Op Amps
- ESD Clamps on Inputs Increase Reliability without Affecting Device Operation

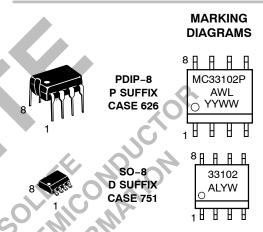
#### TYPICAL SLEEPMODE/AWAKEMODE PERFORMANCE

Characteristic	Sleepmode (Typical)	Awakemode (Typical)	Unit
Low Current Drain	45	750	μΑ
Low Input Offset Voltage	0.15	0.15	mV
High Output Current Capability	0.15	50	mA
Low T.C. of Input Offset Voltage	1.0	1.0	μV/°C
High Gain Bandwidth (@ 20 kHz)	0.33	4.6	MHz
High Slew Rate	0.16	1.7	V/μs
Low Noise (@ 1.0 kHz)	28	9.0	nV/√Hz



### **ON Semiconductor**

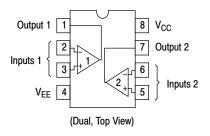
http://onsemi.com



A = Assembly Location

WL, L = Wafer Lot YY, Y = Year WW, W = Work Week

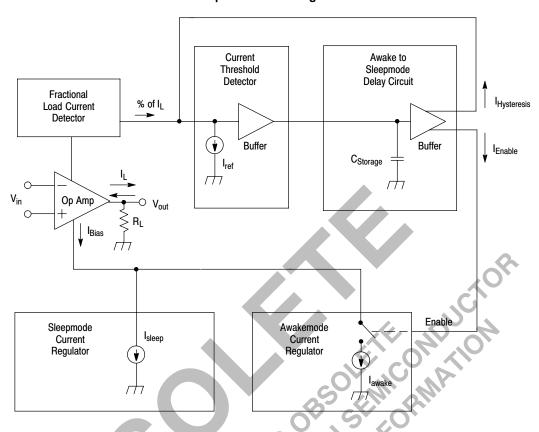
#### **PIN CONNECTIONS**



#### ORDERING INFORMATION

Device	Package	Shipping
MC33102D	SO-8	98 Units/Rail
MC33102DR2	SO-8	2500 Tape & Reel
MC33102P	PDIP-8	50 Units/Rail

#### **Simplified Block Diagram**



#### **MAXIMUM RATINGS**

Ratings	Symbol	Value	Unit
Supply Voltage (V <sub>CC</sub> to V <sub>EE</sub> )	Vs	+36	V
Input Differential Voltage Range Input Voltage Range	V <sub>IDR</sub> V <sub>IR</sub>	Note 1	V
Output Short Circuit Duration (Note 2)	t <sub>SC</sub>	Note 2	sec
Maximum Junction Temperature Storage Temperature	T <sub>J</sub> T <sub>stg</sub>	+150 -65 to +150	°C
Maximum Power Dissipation	P <sub>D</sub>	Note 2	mW

Either or both input voltages should not exceed V<sub>CC</sub> or V<sub>EE</sub>.
 Power dissipation must be considered to ensure maximum junction temperature (T<sub>J</sub>) is not exceeded (refer to Figure 1).

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Characteristics	Figure	Symbol	Min	Тур	Max	Unit
Input Offset Voltage ( $R_S = 50 \Omega$ , $V_{CM} = 0 V$ , $V_O = 0 V$ )	2	V <sub>IO</sub>				mV
Sleepmode						
$T_A = +25^{\circ}C$			_	0.15	2.0	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$			_	_	3.0	
Awakemode				0.45		
$T_A = +25^{\circ}C$			_	0.15	2.0	
$T_A = -40^\circ \text{ to } +85^\circ \text{C}$			-	-	3.0	
Input Offset Voltage Temperature Coefficient	3	$\Delta V_{IO}/\Delta T$				μV/°C
$(R_S = 50 \Omega, V_{CM} = 0 V, V_O = 0 V)$						
$T_A = -40^{\circ}$ to +85°C (Sleepmode and Awakemode)			_	1.0	_	
Input Bias Current (V <sub>CM</sub> = 0 V, V <sub>O</sub> = 0 V)	4, 6	I <sub>IB</sub>				nA
Sleepmode						
$T_A = +25^{\circ}C$			-	8.0	50	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$				-	60	
Awakemode						
$T_A = +25^{\circ}C$			-	100	500	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$			_	(	600	
Input Offset Current (V <sub>CM</sub> = 0 V, V <sub>O</sub> = 0 V)		I <sub>IO</sub>				nA
Sleepmode				'O'		
$T_A = +25^{\circ}C$				0.5	5.0	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$			A - 3	0 - 6	6.0	
Awakemode				, (O)	1	
$T_A = +25^{\circ}C$			-0	5.0	50	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$			1 .G	7	60	
Common Mode Input Voltage Range	5	Vice				V
$(\Delta V_{IO} = 5.0 \text{ mV}, V_O = 0 \text{ V})$	V 3	CION				
Sleepmode and Awakemode			-13	-14.8	_	
				+14.2	+13	
Large Signal Voltage Gain	7	Avoi				kV/V
Sleepmode (RL = 1.0 M $\Omega$ )		, VOL				,
$T_A = +25^{\circ}C$	$\cdot$		25	200	_	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$		1, 70	15	_	_	
Awakemode ( $V_O = \pm 10 \text{ V}, R_L = 600 \Omega$ )	. 1O					
$T_A = +25^{\circ}C$			50	700	_	
$T_A = -40^{\circ} \text{ to } +85^{\circ}\text{C}$		7	25	_	_	
Output Voltage Swing (V <sub>ID</sub> = ±1.0 V)	8, 9, 10					V
Sleepmode (V <sub>CC</sub> = +15 V, V <sub>EE</sub> = -15 V)						
$R_{L} = 1.0 \text{ M}\Omega$	7,	V <sub>O+</sub>	+13.5	+14.2	_	
		V <sub>O</sub> _	_	-14.2	-13.5	
Awakemode ( $V_{CC} = +15 \text{ V}, V_{EE} = -15 \text{ V}$ )						V
$R_{l} = 600 \Omega$		V <sub>O+</sub>	+12.5	+13.6	_	
$R_L = 600 \Omega$		V <sub>O</sub> -	_	-13.6	-12.5	
$R_L = 2.0 \text{ k}\Omega$		V <sub>O+</sub>	+13.3	+14	_	
$R_L = 2.0 \text{ k}\Omega$		V <sub>O</sub> -	_	-14	-13.3	
Awakemode ( $V_{CC} = +2.5 \text{ V}, V_{FF} = -2.5 \text{ V}$ )						
$R_L = 600 \Omega$		V <sub>O+</sub>	+1.1	+1.6	_	
$R_L = 600 \Omega$		V <sub>O</sub> -	-	-1.6	-1.1	
$R_L=1.0~M\Omega$ Awakemode ( $V_{CC}=+15~V,~V_{EE}=-15~V$ ) $R_L=600~\Omega$ $R_L=600~\Omega$ $R_L=2.0~k\Omega$ $R_L=2.0~k\Omega$ Awakemode ( $V_{CC}=+2.5~V,~V_{EE}=-2.5~V$ ) $R_L=600~\Omega$ $R_L=600~\Omega$ Common Mode Rejection ( $V_{CM}=\pm13~V$ )	11	CMR				dB
Sleepmode and Awakemode			80	90	-	
Power Supply Rejection (V <sub>CC</sub> /V <sub>EE</sub> = +15 V/-15 V,	12	PSR				dB
5.0 V/-15 V, +15 V/-5.0 V)			1			
3.0 V/-13 V, +13 V/-3.0 V)						

### **DC ELECTRICAL CHARACTERISTICS** $(V_{CC} = +15 \text{ V}, V_{EE} = -15 \text{ V}, T_A = 25^{\circ}\text{C}, \text{ unless otherwise noted.})$

13, 14	I <sub>TH1</sub>    I <sub>TH2</sub>	200 250	160 200	- -	μΑ
	I <sub>TH2</sub>				
			142 180	90 140	
15, 16	Isc	50	110	-	mA
17	I <sub>D</sub>	50			μΑ
			48 38	70 65	
		_	750	800	
MCE IS	REFOR				
ENTAI	3				
	17	17 I <sub>D</sub>	50 50 17 I <sub>D</sub>	50 110 50 110 17 I <sub>D</sub> 45 48 - 38	50 110 - 50 110 - 17 I <sub>D</sub> - 45 65 - 48 70 - 38 65

## AC ELECTRICAL CHARACTERISTICS $(V_{CC} = +15 \text{ V}, V_{EE} = -15 \text{ V}, T_A = 25^{\circ}\text{C}, \text{ unless otherwise noted.})$

Characteristics	Figure	Symbol	Min	Тур	Max	Unit
Slew Rate (V <sub>in</sub> = -5.0 V to +5.0 V, C <sub>L</sub> = 50 pF, A <sub>V</sub> = 1.0) Sleepmode (R <sub>L</sub> = 1.0 M $\Omega$ ) Awakemode (R <sub>L</sub> = 600 $\Omega$ )	18	SR	0.10 1.0	0.16 1.7	- -	V/µs
Gain Bandwidth Product Sleepmode (f = 10 kHz) Awakemode (f = 20 kHz)	19	GBW	0.25 3.5	0.33 4.6	- -	MHz
Sleepmode to Awakemode Transition Time $ \text{(A}_{CL} = 0.1,  \text{V}_{in} = 0  \text{V to } +5.0  \text{V)} $ $ \text{R}_{L} = 600  \Omega $ $ \text{R}_{L} = 10  \text{k}\Omega $	20, 21	t <sub>tr1</sub>	-	4.0 15	- -	μs
Awakemode to Sleepmode Transition Time	22	t <sub>tr2</sub>	_	1.5	_	sec
Unity Gain Frequency (Open Loop) Sleepmode (R <sub>L</sub> = 100 k $\Omega$ , C <sub>L</sub> = 0 pF) Awakemode (R <sub>L</sub> = 600 $\Omega$ , C <sub>L</sub> = 0 pF)		fu		200 2500	- O-	kHz
Gain Margin Sleepmode (R <sub>L</sub> = 100 k $\Omega$ , C <sub>L</sub> = 0 pF) Awakemode (R <sub>L</sub> = 600 $\Omega$ , C <sub>L</sub> = 0 pF)	23, 25	A <sub>M</sub>	- -	13 12	0	dB
Phase Margin Sleepmode (R <sub>L</sub> = 100 k $\Omega$ , C <sub>L</sub> = 0 pF) Awakemode (R <sub>L</sub> = 600 $\Omega$ , C <sub>L</sub> = 0 pF)	24, 26	$\varnothing_{M}$	( - O	60 60	<i>P</i> -	Degree s
Channel Separation (f = 100 Hz to 20 kHz) Sleepmode and Awakemode	29	CS		120	_	dB
Power Bandwidth (Awakemode) $(V_O = 10 V_{pp}, R_L = 100 kΩ, THD ≤ 1%)$		BW <sub>P</sub>	, O.	20	-	kHz
Total Harmonic Distortion ( $V_O$ = 2.0 $V_{pp}$ , $A_V$ = 1.0) Awakemode ( $R_L$ = 600 $\Omega$ ) f = 1.0 kHz f = 10 kHz f = 20 kHz	30	THD	-	0.005 0.016 0.031	- - -	%
DC Output Impedance ( $V_Q$ = 0 V, $A_V$ = 10, $I_Q$ = 10 $\mu$ A) Sleepmode Awakemode	31	R <sub>O</sub>		1.0 k 96	_ _	Ω
Differential Input Resistance (V <sub>CM</sub> = 0 V) Sleepmode Awakemode	MI	R <sub>in</sub>		1.3 0.17	- -	ΜΩ
Differential Input Capacitance (V <sub>CM</sub> = 0 V) Sleepmode Awakemode		C <sub>in</sub>		0.4 4.0	- -	pF
Equivalent Input Noise Voltage (f = 1.0 kHz, $R_S$ = 100 $\Omega$ ) Sleepmode Awakemode	32	e <sub>n</sub>		28 9.0	- -	nV/√Hz
Equivalent Input Noise Current (f = 1.0 kHz) Sleepmode Awakemode	33	i <sub>n</sub>	- -	0.01 0.05	- -	pA/√Hz

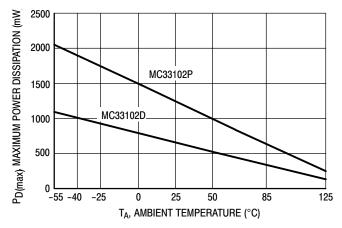


Figure 1. Maximum Power Dissipation versus Temperature

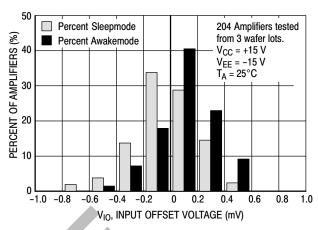


Figure 2. Distribution of Input Offset Voltage (MC33102D Package)

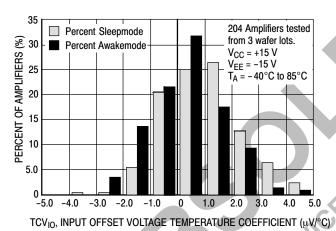


Figure 3. Input Offset Voltage Temperature Coefficient Distribution (MC33102D Package)

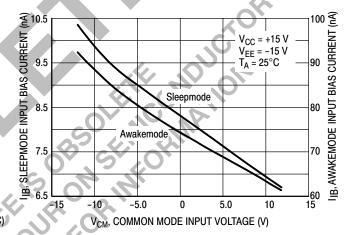


Figure 4. Input Bias Current versus Common Mode Input Voltage

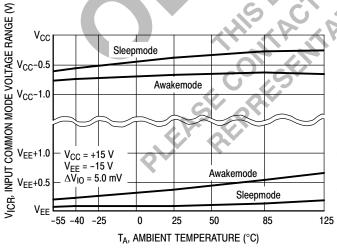


Figure 5. Input Common Mode Voltage Range versus Temperature

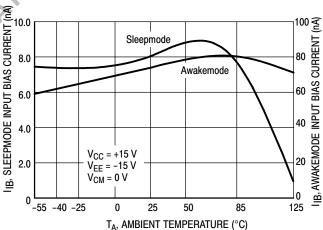


Figure 6. Input Bias Current versus Temperature

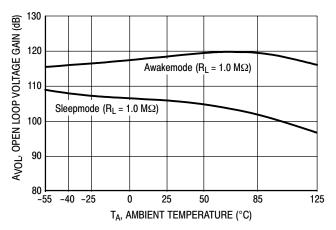
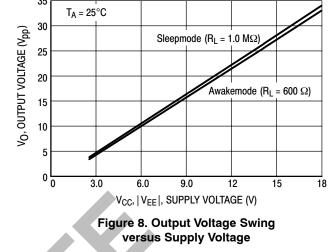


Figure 7. Open Loop Voltage Gain versus Temperature



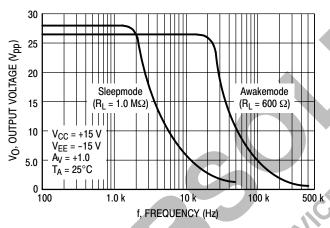


Figure 9. Output Voltage versus Frequency

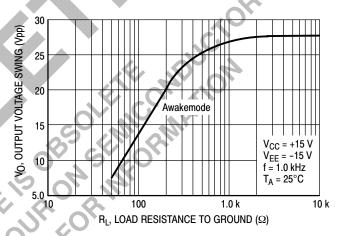


Figure 10. Maximum Peak-to-Peak Output
Voltage Swing versus Load Resistance

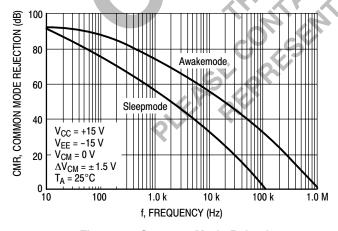


Figure 11. Common Mode Rejection versus Frequency

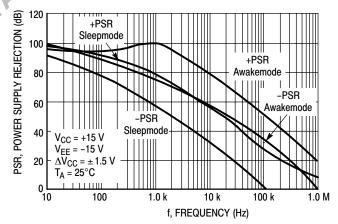


Figure 12. Power Supply Rejection versus Frequency

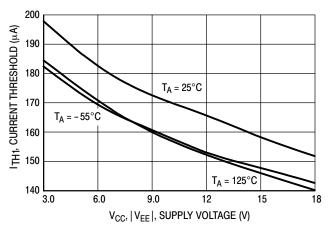


Figure 13. Sleepmode to Awakemode Current Threshold versus Supply Voltage

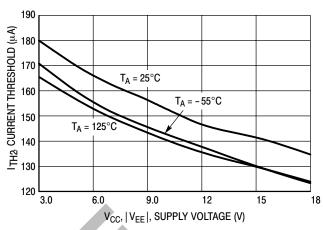


Figure 14. Awakemode to Sleepmode Current Threshold versus Supply Voltage

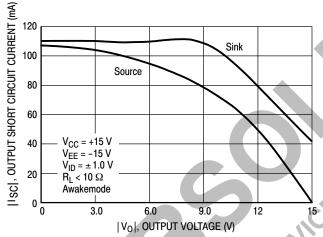


Figure 15. Output Short Circuit Current versus Output Voltage

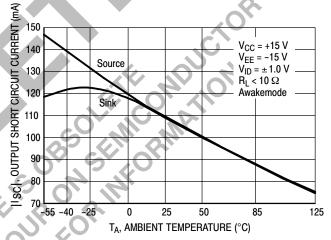


Figure 16. Output Short Circuit Current versus Temperature

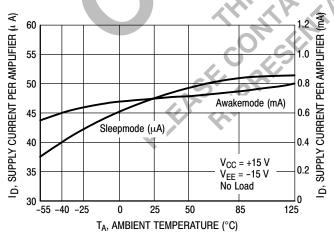


Figure 17. Power Supply Current Per Amplifier versus Temperature

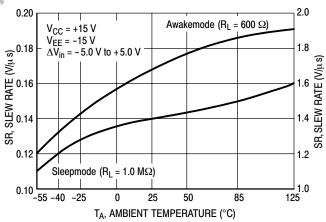


Figure 18. Slew Rate versus Temperature

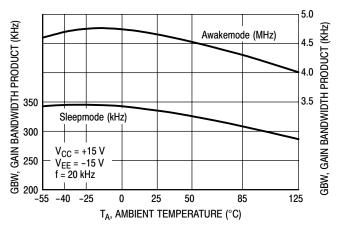


Figure 19. Gain Bandwidth Product versus Temperature

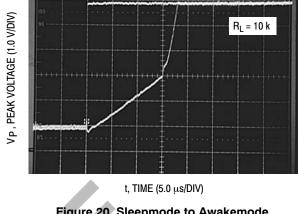


Figure 20. Sleepmode to Awakemode Transition Time

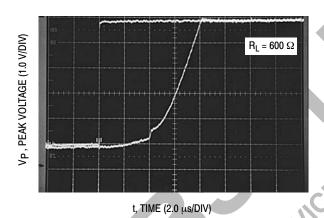


Figure 21. Sleepmode to Awakemode Transition Time

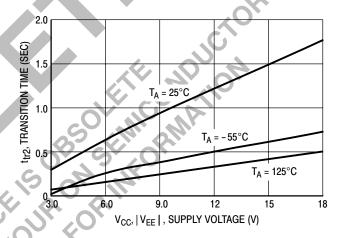


Figure 22. Awakemode to Sleepmode Transition Time versus Supply Voltage

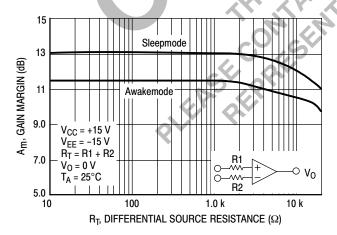


Figure 23. Gain Margin versus Differential Source Resistance

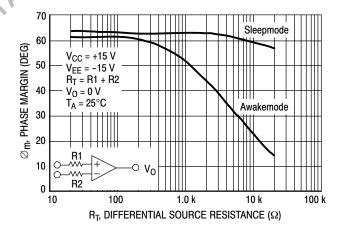


Figure 24. Phase Margin versus Differential Source Resistance

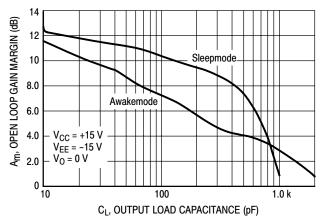


Figure 25. Open Loop Gain Margin versus
Output Load Capacitance

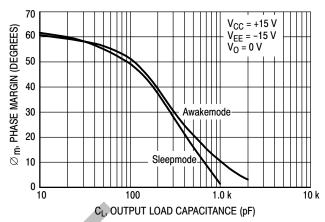


Figure 26. Phase Margin versus
Output Load Capacitance

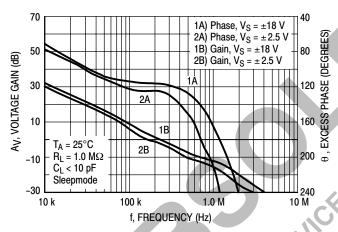


Figure 27. Sleepmode Voltage Gain and Phase versus Frequency

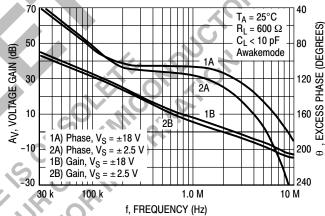


Figure 28. Awakemode Voltage Gain and Phase versus Frequency

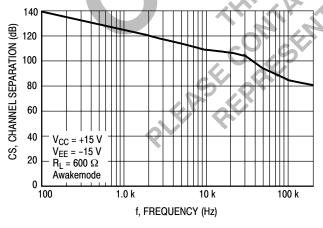


Figure 29. Channel Separation versus Frequency

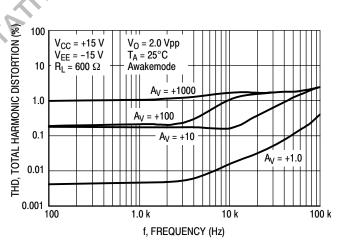


Figure 30. Total Harmonic Distortion versus Frequency

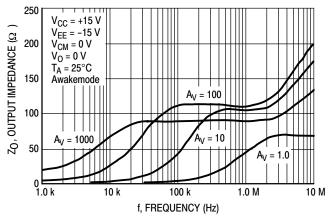


Figure 31. Awakemode Output Impedance versus Frequency

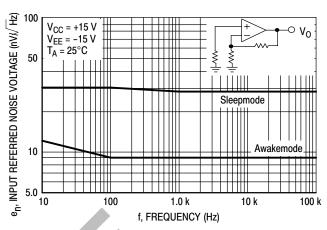
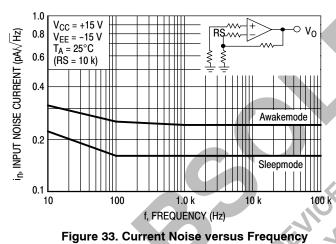


Figure 32. Input Referred Noise Voltage versus Frequency



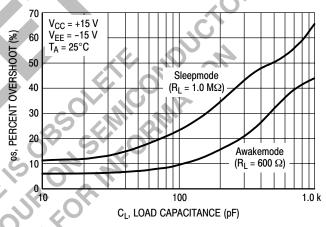


Figure 34. Percent Overshoot versus Load Capacitance

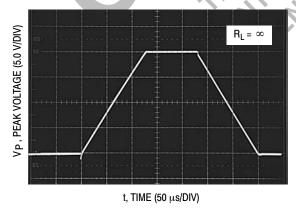


Figure 35. Sleepmode Large Signal **Transient Response** 

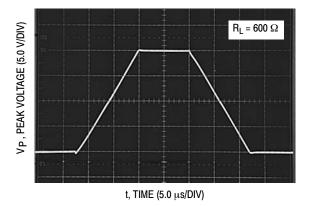


Figure 36. Awakemode Large Signal **Transient Response** 

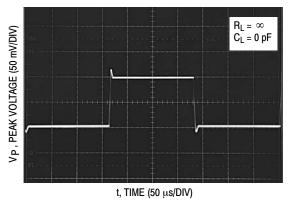


Figure 37. Sleepmode Small Signal Transient Response

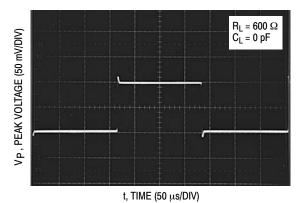


Figure 38. Awakemode Small Signal
Transient Response

#### **CIRCUIT INFORMATION**

The MC33102 was designed primarily for applications where high performance (which requires higher current drain) is required only part of the time. The two-state feature of this op amp enables it to conserve power during idle times, yet be powered up and ready for an input signal. Possible applications include laptop computers, automotive, cordless phones, baby monitors, and battery operated test equipment. Although most applications will require low power consumption, this device can be used in any application where better efficiency and higher performance is needed.

The Sleep-Mode<sup>TM</sup> amplifier has two states; a sleepmode and an awakemode. In the sleepmode state, the amplifier is active and functions as a typical micropower op amp. When a signal is applied to the amplifier causing it to source or sink sufficient current (see Figure 13), the amplifier will automatically switch to the awakemode. See Figures 20 and 21 for transition times with  $600~\Omega$  and  $10~k\Omega$  loads.

The awakemode uses higher drain current to provide a high slew rate, gain bandwidth, and output current capability. In the awakemode, this amplifier can drive 27 Vpp into a 600  $\Omega$  load with  $V_S = \pm 15$  V.

An internal delay circuit is used to prevent the amplifier from returning to the sleepmode at every zero crossing. This delay circuit also eliminates the crossover distortion commonly found in micropower amplifiers. This amplifier can process frequencies as low as 1.0 Hz without the amplifier returning to sleepmode, depending on the load.

The first stage PNP differential amplifier provides low noise performance in both the sleep and awake modes, and an all NPN output stage provides symmetrical source and sink AC frequency response.

## **APPLICATIONS INFORMATION**

The MC33102 will begin to function at power supply voltages as low as  $V_S = \pm 1.0 \, \mathrm{V}$  at room temperature. (At this voltage, the output voltage swing will be limited to a few hundred millivolts.) The input voltages must range between  $V_{CC}$  and  $V_{EE}$  supply voltages as shown in the maximum rating table. Specifically, allowing the input to go more negative than 0.3 V below  $V_{EE}$  may cause product damage. Also, exceeding the input common mode voltage range on either input may cause phase reversal, even if the inputs are between  $V_{CC}$  and  $V_{EE}$ .

When power is initially applied, the part may start to operate in the awakemode. This is because of the currents generated due to charging of internal capacitors. When this occurs and the sleepmode state is desired, the user will have to wait approximately 1.5 seconds before the device will switch back to the sleepmode. To prevent this from occurring, ramp the power supplies from 1.0 V to full supply. Notice that the device is more prone to switch into the awakemode when  $V_{\rm EE}$  is adjusted than with a similar change in  $V_{\rm CC}$ .

The amplifier is designed to switch from sleepmode to awakemode whenever the output current exceeds a preset current threshold ( $I_{TH}$ ) of approximately 160  $\mu$ A. As a result, the output switching threshold voltage ( $V_{ST}$ ) is controlled by the output loading resistance ( $R_L$ ). This loading can be a load resistor, feedback resistors, or both. Then:

$$V_{ST} = (160 \mu A) \times R_L$$

Large valued load resistors require a large output voltage to switch, but reduce unwanted transitions to the awakemode. For instance, in cases where the amplifier is connected with a large closed loop gain ( $A_{CL}$ ), the input offset voltage ( $V_{IO}$ ) is multiplied by the gain at the output and could produce an output voltage exceeding  $V_{ST}$  with no input signal applied.

Small values of  $R_L$  allow rapid transition to the awakemode because most of the transition time is consumed slewing in the sleepmode until  $V_{ST}$  is reached (see Figures 20, 21). The output switching threshold voltage  $V_{ST}$  is higher for larger

values of R<sub>L</sub>, requiring the amplifier to slew longer in the slower sleepmode state before switching to the awakemode.

The transition time  $(t_{tr1})$  required to switch from sleep to awake mode is:

$$t_{tr1} = t_D = I_{TH}(R_L/SR_{sleepmode})$$

Where:

 $t_D$  = Amplifier delay (< 1.0 µs)

 $I_{TH}$  = Output threshold current for more transition (160  $\mu$ A)

 $R_L$  = Load resistance

 $SR_{sleepmode}$  = Sleepmode slew rate (0.16 V/ $\mu$ s)

Although typically 160  $\mu$ A,  $I_{TH}$  varies with supply voltage and temperature. In general, any current loading on the output which causes a current greater than  $I_{TH}$  to flow will switch the amplifier into the awakemode. This includes transition currents such as those generated by charging load capacitances. In fact, the maximum capacitance that can be driven while attempting to remain in the sleepmode is approximately 1000 pF.

$$\begin{array}{ll} C_{L(max)} &= I_{TH}/SR_{sleepmode} \\ &= 160~\mu\text{A}/(0.16~\text{V/}\mu\text{s}) \\ &= 1000~\text{pF} \end{array}$$

Any electrical noise seen at the output of the MC33102 may also cause the device to transition to the awakemode. To

minimize this problem, a resistor may be added in series with the output of the device (inserted as close to the device as possible) to isolate the op amp from both parasitic and load capacitance.

The awakemode to sleepmode transition time is controlled by an internal delay circuit, which is necessary to prevent the amplifier from going to sleep during every zero crossing. This time is a function of supply voltage and temperature as shown in Figure 22.

Gain bandwidth product (GBW) in both modes is an important system design consideration when using a sleepmode amplifier. The amplifier has been designed to obtain the maximum GBW in both modes. "Smooth" AC transitions between modes with no noticeable change in the amplitude of the output voltage waveform will occur as long as the closed loop gains  $(A_{CL})$  in both modes are substantially equal at the frequency of operation. For smooth AC transitions:

Where:

A<sub>CLsleepmode</sub> = Closed loop gain in the sleepmode BW = The required system bandwidth or operating frequency

#### TESTING INFORMATION

To determine if the MC33102 is in the awakemode or the sleepmode, the power supply currents ( $I_D+$  and  $I_D-$ ) must be measured. When the magnitude of **either** power supply current exceeds 400  $\mu A$ , the device is in the awakemode. When the magnitudes of both supply currents are less than 400  $\mu A$ , the device is in the sleepmode. Since the total supply current is typically ten times higher in the awakemode than the sleepmode, the two states are easily distinguishable.

The measured value of  $I_D+$  equals the  $I_D$  of both devices (for a dual op amp) plus the output source current of device A and the output source current of device B. Similarly, the measured value of  $I_D-$  is equal to the  $I_D-$  of both devices plus

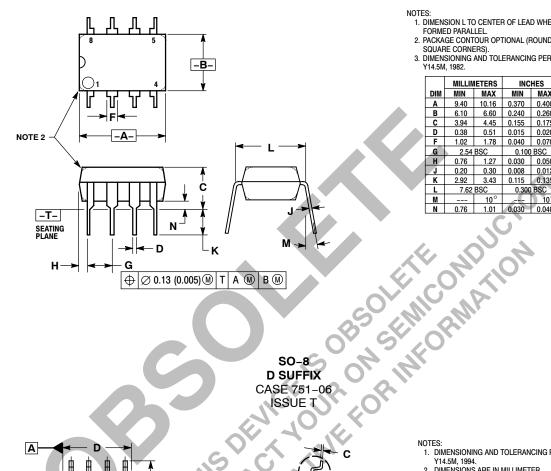
the output sink current of each device.  $I_{out}$  is the sum of the currents caused by both the feedback loop and load resistance. The total  $I_{out}$  needs to be subtracted from the measured  $I_D$  to obtain the correct  $I_D$  of the dual op amp.

An accurate way to measure the awakemode  $I_{out}$  current on automatic test equipment is to remove the  $I_{out}$  current on both Channel A and B. Then measure the  $I_D$  values before the device goes back to the sleepmode state. The transition will take typically 1.5 seconds with  $\pm 15$  V power supplies.

The large signal sleepmode testing in the characterization was accomplished with a 1.0 M $\Omega$  load resistor which ensured the device would remain in sleepmode despite large voltage swings.

#### PACKAGE DIMENSIONS

#### PDIP-8 **P SUFFIX** CASE 626-05 ISSUE K



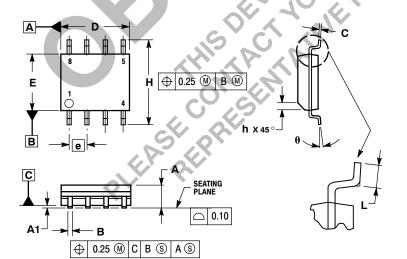
- NOTES:

  1. DIMENSION L TO CENTER OF LEAD WHEN FORMED PARALLEL.

  2. PACKAGE CONTOUR OPTIONAL (ROUND OR
  - SQUARE CORNERS)
  - 3. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.

	MILLIMETERS		INC	HES
DIM	MIN	MAX	MIN	MAX
Α	9.40	10.16	0.370	0.400
В	6.10	6.60	0.240	0.260
С	3.94	4.45	0.155	0.175
D	0.38	0.51	0.015	0.020
F.	1.02	1.78	0.040	0.070
G	2.54	BSC	0.100	BSC
H	0.76	1.27	0.030	0.050
7	0.20	0.30	0.008	0.012
K	2.92	3.43	0.115	0.135
L	7.62	BSC	0.300	BSC
M		10°		10°
N	0.76	1.01	0.030	0.040

# SO-8 D SUFFIX CASE 751-06 ISSUE T



- IOTES:
  1 DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.
  2 DIMENSIONS ARE IN MILLIMETER.
  3 DIMENSION D AND E DO NOT INCLUDE MOLD PROTECTION.
- PROTRUSION.

  4. MAXIMUM MOLD PROTRUSION 0.15 PER SIDE.
- 5. DIMENSION B DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.127 TOTAL IN EXCESS OF THE B DIMENSION AT MAXIMUM MATERIAL CONDITION.

	MILLIMETERS			
DIM	MIN	MAX		
Α	1.35	1.75		
A1	0.10	0.25		
В	0.35	0.49		
C	0.19	0.25		
D	4.80	5.00		
Е	3.80	4.00		
е	1.27	BSC		
H	5.80	6.20		
h	0.25	0.50		
L	0.40	1.25		
A	0 °	7 º		



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