

PA84 • PA84A • PA84S

HTTP://WWW.APEXMICROTECH.COM (800) 546-APEX (800) 546-2739

FEATURES

- HIGH SLEW RATE $200V/\mu s$
- FAST SETTLING TIME .1% in 1µs (PA84S)
- FULLY PROTECTED INPUT Up to ±150v
- LOW BIAS CURRENT, LOW NOISE FET Input
- WIDE SUPPLY RANGE ±15V to ±150V

APPLICATIONS

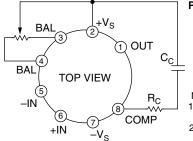
- HIGH VOLTAGE INSTRUMENTATION
- ELECTROSTATIC TRANSDUCERS & DEFLECTION
- PROGRAMMABLE POWER SUPPLIES UP TO 290V
- ANALOG SIMULATORS

DESCRIPTION

The PA84 is a high voltage operational amplifier designed for output voltage swings up to ±145V with a dual supply or 290V with a single supply. Two versions are available. The new PA84S, fast settling amplifier can absorb differential input overvoltages up to $\pm 50 \mbox{V}$ while the established PA84 and PA84A can handle differential input overvoltages of up to ±300V. Both versions are protected against common mode transients and overvoltages up to the supply rails. High accuracy is achieved with a cascode input circuit configuration. All internal biasing is referenced to a zener diode fed by a FET constant current source. As a result, the PA84 features an unprecedented supply range and excellent supply rejection. The output stage is biasedon for linear operation. External phase compensation allows for user flexibility in obtaining the maximum slew rate. Fixed current limits protect these amplifiers against shorts to common at supply voltages up to 150V. For operation into inductive loads, two external flyback pulse protection diodes are recommended. With the exception of PA84S, a built-in thermal shutoff circuit prevents destructive overheating. However, a heatsink may be necessary to maintain the proper case temperature under normal operating conditions.

This hybrid integrated circuit utilizes a beryllia (BeO) substrate, thick film resistors, ceramic capacitors and semiconductor chips to maximize reliability, minimize size and give top performance. Ultrasonically bonded aluminum wires provide reliable interconnections at all operating temperatures. The 8-pin TO-3 package is hermetically sealed and electrically isolated. The use of compressible thermal isolation washers and/or improper mounting torque will void the product warranty. Please see "General Operating Considerations".

EXTERNAL CONNECTION



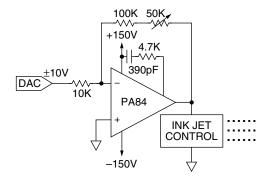
PHASE COMPENSATION

GAIN	C^{C}	R_{C}
1 10 100 1000	10nF 500pF 50pF none	$\begin{array}{c} 200\Omega\\ 2K\Omega\\ 20K\Omega\\ \text{none} \end{array}$

NOTES:

- Phase Compensation required for safe operation.
- 2. Input offset trimpot optional. Recommended value $100 K\Omega$.

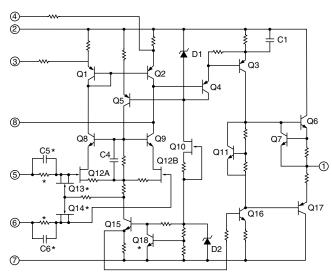




TYPICAL APPLICATION

The PA84 is ideally suited to driving ink jet control units (often a piezo electric device) which require precise pulse shape control to deposit crisp clear date or lot code information on product containers. The external compensation network has been optimized to match the gain setting of the circuit and the complex impedance of the ink jet control unit. The combination of speed and high voltage capabilities of the PA84 form ink droplets of uniform volume at high production rates to enhance the value of the printer.

EQUIVALENT SCHEMATIC



* NOTE: Not used for PA84S

300V

17.5W

±300V ±50V

300°C 200°C

Internally Limited

PA84 • PA84A • PA84S

ABSOLUTE MAXIMUM RATINGS

SUPPLY VOLTAGE, +V_S to -V_S OUTPUT CURRENT, within SOA POWER DISSIPATION, internal at $T_{\rm C}$ = $25^{\circ}C^2$

INPUT VOLTAGE, differential PA84/PA84A¹ INPUT VOLTAGE, differential PA84S INPUT VOLTAGE, common mode1

TEMPERATURE, pins for 10s max (solder) TEMPERATURE, junction²

TEMPERATURE RANGE, storage -65 to +150°C OPERATING TEMPERATURE RANGE, case -55 to +125°C

SPECIFICATIONS		P	A84/PA84	18		PA84A		
PARAMETER	TEST CONDITIONS 3	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
INPUT								
OFFSET VOLTAGE, initial OFFSET VOLTAGE, vs. temperature OFFSET VOLTAGE, vs. supply OFFSET VOLTAGE, vs. time	$ \begin{array}{l} T_{C} = 25^{\circ}C \\ T_{C} = -25^{\circ} \text{ to } +85^{\circ}C \\ T_{C} = 25^{\circ}C \\ T_{C} = 25^{\circ}C \end{array} $		±1.5 ±10 ±.5 ±75	±3 ±25		±.5 ±5 ±.2 *	±1 ±10	mV μV/°C μV/V μV/√kh
BIAS CURRENT, initial⁴	$T_C = 25^{\circ}C$		5	50		3	10	, bY
BIAS CURRENT, vs. supply OFFSET CURRENT, initial ⁴ OFFSET CURRENT, vs. supply INPUT IMPEDANCE, DC INPUT CAPACITANCE COMMON MODE VOLTAGE RANGE ⁵ COMMON MODE REJECTION, DC	$\begin{split} T_{\text{C}} &= 25^{\circ}\text{C} \\ T_{\text{C}} &= 25^{\circ}\text{C} \\ T_{\text{C}} &= 25^{\circ}\text{C} \\ T_{\text{C}} &= 25^{\circ}\text{C} \\ T_{\text{C}} &= -25^{\circ}\text{ to } +85^{\circ}\text{C} \\ T_{\text{C}} &= -25^{\circ}\text{ to } +85^{\circ}\text{C} \\ T_{\text{C}} &= -25^{\circ}\text{ to } +85^{\circ}\text{C} \end{split}$	±V _S -10	.01 ±2.5 ±.01 10 ¹¹ 6 ±V _S -8.5 130	±50	*	±1.5 * * * * *	±10	pA/V pA pA/V Ω pF V dB
GAIN								
OPEN LOOP GAIN at 10Hz OPEN LOOP GAIN at 10Hz. GAIN BANDWIDTH PRODUCT@ 1MHz POWER BANDWIDTH, high gain POWER BANDWIDTH, low gain	$ \begin{array}{l} T_{\text{C}} = 25^{\circ}\text{C}, R_{\text{L}} = \infty \\ T_{\text{C}} = 25^{\circ}\text{C}, R_{\text{L}} = 3.5\text{K}\Omega \\ T_{\text{C}} = 25^{\circ}\text{C}, R_{\text{L}} = 3.5\text{K}\Omega, R_{\text{C}} = 20\text{K}\Omega \\ T_{\text{C}} = 25^{\circ}\text{C}, R_{\text{L}} = 3.5\text{K}\Omega, R_{\text{C}} = 20\text{K}\Omega \\ T_{\text{C}} = 25^{\circ}\text{C}, R_{\text{L}} = 3.5\text{K}\Omega, R_{\text{C}} = 20\text{K}\Omega \\ \end{array} $	100	120 118 75 250 120		* 180	* * * *		dB dB MHz kHz kHz
OUTPUT								
VOLTAGE SWING ⁵ VOLTAGE SWING ⁵ CURRENT, peak CURRENT, short circuit SLEW RATE, high gain	$ \begin{array}{l} T_{\text{C}} = 25^{\circ}\text{C}, \ I_{\text{O}} = \pm 40\text{mA} \\ T_{\text{C}} = -25^{\circ}\text{ to } +85^{\circ}\text{C}, \ I_{\text{O}} = \pm 15\text{mA} \\ T_{\text{C}} = 25^{\circ}\text{C} \\ T_{\text{C}} = 25^{\circ}\text{C} \\ T_{\text{C}} = 25^{\circ}\text{C}, \ R_{\text{L}} = 3.5\text{K}\Omega, \ R_{\text{C}} = 20\text{K}\Omega \end{array} $	±V _S -7 ±V _S -5 40	±V _S -3 ±V _S -2		* * 150	* * *		V V mA mA V/μs
SLEW RATE, low gain SETTLING TIME .01% at gain = 100	$T_c = 25$ °C, $R_L = 3.5$ KΩ, $R_c = 2$ KΩ $T_c = 25$ °C, $R_L = 3.5$ KΩ PA84S	 	125 2			_ * +		<u>V/μs</u> μs
SETTLING TIME .1% at gain = 100	$R_C = 20K\Omega$, $V_{IN} = 2V$ step ONLY	ļ <u> </u>	1					<u>μ</u> s
SETTLING TIME .01% at gain = 100 SETTLING TIME .1% at gain = 100	$T_{c} = 25^{\circ}C, R_{L} = 3.5K\Omega$ PA84/84A $R_{c} = 20K\Omega, V_{IN} = 2V \text{ step}$		20 12			20 12		μs μs
POWER SUPPLY								
VOLTAGE CURRENT, quiescent	$T_{c} = -55^{\circ}C \text{ to } +125^{\circ}C$ $T_{c} = 25^{\circ}C$	±15	5.5	±150 7.5	*	*	*	V mA
THERMAL								
RESISTANCE, AC, junction to case ⁶ RESISTANCE, DC, junction to case RESISTANCE, case to air TEMPERATURE RANGE, case	$\begin{array}{l} T_{\text{C}} = -55^{\circ}\text{C to} + 125^{\circ}\text{C, F} > 60\text{Hz} \\ T_{\text{C}} = -55^{\circ}\text{C to} + 125^{\circ}\text{C, F} < 60\text{Hz} \\ T_{\text{C}} = -55^{\circ}\text{C to} + 125^{\circ}\text{C} \\ \text{Meets full range specifications} \end{array}$	-25	3.8 6 30	6.5 +85	*	* *	*	°C/W °C/W °C

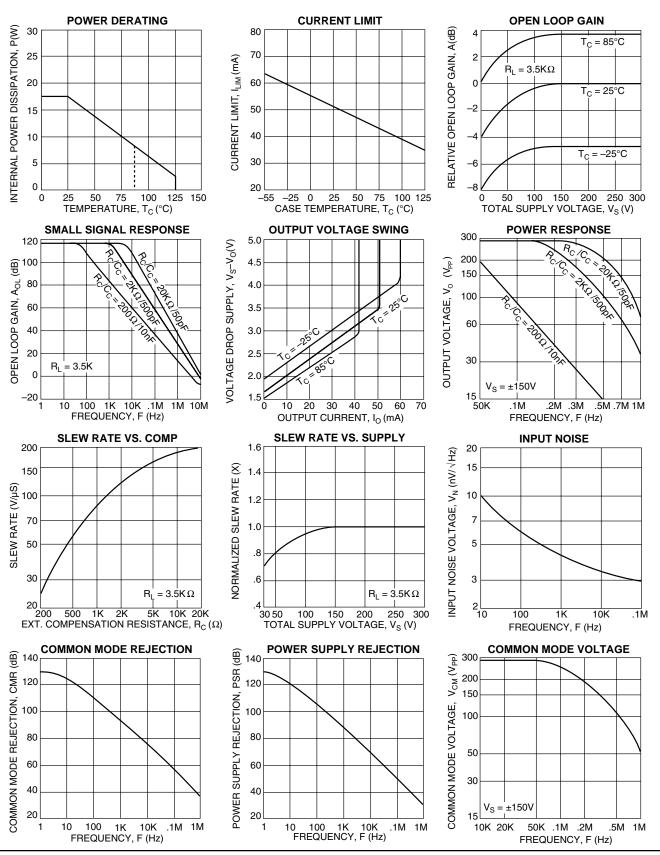
NOTES:

- The specification of PA84A is identical to the specification for PA84/PA84S in applicable column to the left.
- Signal slew rates at pins 5 and 6 must be limited to less than 1V/ns to avoid damage. When faster waveforms are unavoidable, 1. resistors in series with those pins, limiting current to 150mA will protect the amplifier from damage.
- Long term operation at the maximum junction temperature will result in reduced product life. Derate internal power dissipation to achieve high MTTF.
- The power supply voltage for all tests is ± 150 V, unless otherwise noted as a test condition.
- 4. Doubles for every 10°C of temperature increase.
- +V_s and -V_s denote the positive and negative power supply rail respectively.
- Rating applies if the output current alternates between both output transistors at a rate faster than 60Hz.

CAUTION

The internal substrate contains beryllia (BeO). Do not break the seal. If accidentally broken, do not crush, machine, or subject to temperatures in excess of 850°C to avoid generating toxic fumes.

PA84 • PA84A • PA84S



PA84 • PA84A • PA84S

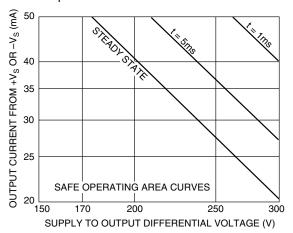
GENERAL

Please read the "General Operating Considerations" section, which covers stability, supplies, heatsinking, mounting, current limit, SOA interpretation, and specification interpretation. Additional information can be found in the application notes. For information on the package outline, heatsinks, and mounting hardware, consult the "Accessory and Package Mechanical Data" section of the handbook.

SAFE OPERATING AREA (SOA)

The bipolar output stage of this high voltage operational amplifier has two output limitations:

- The internal current limit which limits maximum available output current.
- The second breakdown effect, which occurs whenever the simultaneous collector current and collector-emitter voltage exceeds specified limits.



The SOA curves combine the effect of these limits. For a given application, the direction and magnitude of the output current should be calculated or measured and checked against the SOA curves. This is simple for resistive loads but more complex for reactive and EMF generating loads. However, the following guidelines may save extensive analytical efforts:

1. The following capacitive and inductive loads are safe:

$\pm V_S$	C(MAX)	L(MAX)
150V	1.2μF	.7H
125V	6.0μF	25H
100V	12μF	90H
75V	ALL	ALL

- 2. Short circuits to ground are safe with dual supplies up to $\pm 150 \text{V}$ or single supplies up to 150V.
- 3. Short circuits to the supply rails are safe with total supply voltages up to 150V (i.e. ± 75 V).

THERMAL SHUTDOWN PROTECTION

PA84S does not have this feature.

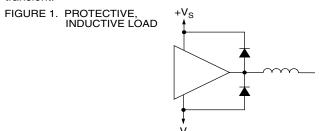
The thermal protection circuit shuts off the amplifier when the substrate temperature exceeds approximately 150°C. This allows heatsink selection to be based on normal operating conditions while protecting the amplifier against excessive junction temperatures during temporary fault conditions.

Thermal protection is a fairly slow-acting circuit and therefore does not protect the amplifier against transient SOA violations (areas outside of the $T_{\rm c}=25^{\circ}{\rm C}$ boundary). It is designed to protect against short-term fault conditions that result in high power dissipation within the amplifier. If the conditions that cause thermal shutdown are not removed, the amplifier will oscillate in and out of shutdown. This will result in high peak power stresses, will destroy signal integrity, and reduce the reliability of the device.

OUTPUT PROTECTION

Two external diodes as shown in Figure 2, are required to protect these amplifiers against flyback (kickback) pulses exceeding the supply voltages of the amplifier when driving inductive loads. For component selection, these external diodes must be very quick, such as ultra fast recovery diodes with no more than 200 nanoseconds of reverse recovery time. Be sure the diode voltage rating is greater than the total of both supplies. The diode will turn on to divert the flyback energy into the supply rails thus protecting the output transistors from destruction due to reverse bias.

A note of caution about the supply. The energy of the flyback pulse must be absorbed by the power supply. As a result, a transient will be superimposed on the supply voltage, the magnitude of the transient being a function of its transient impedance and current sinking capability. If the supply voltage plus transient exceeds the maximum supply rating or if the AC impedance of the supply is unknown, it is best to clamp the output and the supply with a zener diode to absorb the transient.



STABILITY

Due to its large bandwidth the PA84 is more likely to oscillate than lower bandwidth Power Operational Amplifiers such as the PA83 or PA08. To prevent oscillations, a reasonable phase margin must be maintained by:

- 1. Selection of the proper phase compensation capacitor and resistor. Use the values given in the table under external connections and interpolate if necessary. The phase margin can be increased by using a large capacitor and a smaller resistor than the slew rate optimized values listed in the table. The compensation capacitor may be connected to common (in lieu of +V_s) if the positive supply is properly bypassed to common. Because the voltage at pin 8 is only a few volts below the positive supply, this ground connection requires the use of a high voltage capacitor.
- 2. Keeping the external sumpoint stray capacitance to ground at a minimum and the sumpoint load resistance (input and feedback resistors in parallel) below 500Ω . Larger sumpoint load resistance can be used with increased phase compensation (see 1 above).
- Connecting the amplifier case to a local AC common thus preventing it from acting as an antenna.





PA84M

HTTP://WWW.APEXMICROTECH.COM (800) 546-APEX (800) 546-2739

1 Input Offset Voltage V_{OS} $25^{\circ}C$ $\pm 150V$ $V_{IN} = 0$, $A_{V} = 100$ 1 Input Offset Voltage V_{OS} $25^{\circ}C$ $\pm 15V$ $V_{IN} = 0$, $A_{V} = 100$ 1 Input Bias Current, +IN $+I_{B}$ $25^{\circ}C$ $\pm 150V$ $V_{IN} = 0$	5.5 mA 3 mV 5.7 mV 50 pA 50 pA 50 pA 50 pA
1 Input Offset Voltage V_{OS} 25° C $\pm 15V$ $V_{IN} = 0$, $A_{V} = 100$ 1 Input Bias Current, +IN $+I_{B}$ 25° C $\pm 150V$ $V_{IN} = 0$	mV pA pA pA pA pA5 mA
1 Input Bias Current, +IN $+I_B$ $25^{\circ}C$ $\pm 150V$ $V_{IN} = 0$	50 pA 50 pA 50 pA 50 mA
	50 pA 50 pA .5 mA
	50 pA 1.5 mA
1 Input Bias Current, –IN $-I_B$ 25° C ± 150 V $V_{IN} = 0$.5 mA
1 Input Offset Current I_{OS} $25^{\circ}C$ $\pm 150V$ $V_{IN} = 0$	
3 Quiescent Current I_Q $-55^{\circ}C$ $\pm 150V$ $V_{IN} = 0$, $A_V = 100$	5 mV
3 Input Offset Voltage $V_{OS} = -55^{\circ}C = \pm 150V = V_{IN} = 0$, $A_{V} = 100$	
	7.7 mV
, , , , , , , , , , , , , , , , , , , ,	50 pA
	50 pA
	50 pA
2 Quiescent Current I_Q 125°C $\pm 150V$ $V_{IN} = 0$, $A_V = 100$.5 mA
	.5 mV
	.2 mV
, , , , , , , , , , , , , , , , , , , ,	0 nA
	0 nA
	0 nA
4 Output Voltage, $I_0 = 40 \text{mA}$ V_0 25°C $\pm 47 \text{V}$ $R_L = 1 \text{K}$ 40	V
4 Output Voltage, $I_0 = 28.6 \text{mA}$ $V_0 = 25^{\circ}\text{C} = \pm 150 \text{V}$ $R_L = 5 \text{K}$ 143	V
4 Output Voltage, $I_0 = 15 \text{mA}$ $V_0 = 25^{\circ}\text{C} \pm 80 \text{V}$ $R_L = 5 \text{K}$ 75	V
	70 mA
4 Stability/Noise E_N $25^{\circ}C$ $\pm 150V$ $R_L = 5K$, $A_V = 1$, $C_L = 10nF$	1 mV
	00 V/μs
4 Open Loop Gain A_{OL} 25° C ± 150 V $R_{L} = 5$ k, $F = 10$ Hz 100	dB
4 Common Mode Rejection CMR 25° C ± 32.5 V $R_L = 5$ k, $F = DC$, $V_{CM} = \pm 22.5$ V 90	dB
6 Output Voltage, $I_0 = 40 \text{mA}$ $V_0 = -55 ^{\circ}\text{C}$ $\pm 47 \text{V}$ $R_L = 1 \text{K}$ 40	V
6 Output Voltage, $I_0 = 28.6 \text{mA}$ $V_0 = -55^{\circ}\text{C}$ $\pm 150 \text{V}$ $R_L = 5 \text{K}$ 143	V
6 Output Voltage, $I_0 = 15 \text{mA}$ $V_0 = -55^{\circ}\text{C}$ $\pm 80 \text{V}$ $R_L = 5 \text{K}$ 75	V
6 Stability/Noise $E_N = -55^{\circ}C = \pm 150V$ $R_L = 5K$, $A_V = 1$, $C_L = 10nF$	1 mV
	00 V/μs
6 Open Loop Gain $A_{OL} = -55^{\circ}C \pm 150V$ $R_{L} = 5K$, $F = 10Hz$ 100	dΒ
6 Common Mode Rejection CMR -55° C ± 32.5 V $R_L = 5k$, $F = DC$, $V_{CM} = \pm 22.5$ V 90	dB
5 Output Voltage, $I_0 = 30 \text{mA}$ V_0 125°C $\pm 37 \text{V}$ $R_L = 1 \text{K}$ 30	V
5 Output Voltage, $I_0 = 28.6 \text{mA}$ V_0 125°C $\pm 150 \text{V}$ $R_L = 5 \text{K}$ 143	V
5 Output Voltage, $I_0 = 15\text{mA}$ V_0 125°C $\pm 80\text{V}$ $R_L = 5\text{K}$ 75	V
5 Stability/Noise E_N 125°C ±150V $R_L = 5$, $A_V = 1$, $C_L = 10$ nF	1 mV
	00 V/μs
5 Open Loop Gain $A_{OL} = 125^{\circ}\text{C} + 150^{\circ}\text{C} + 150^{\circ}\text{C} = 36\text{Hz}$ 100	dB
5 Common Mode Rejection CMR 125° C ± 32.5 V $R_1 = 5$ k, $F = DC$, $V_{CM} = \pm 22.5$ V 90	dB

BURN IN CIRCUIT $\begin{array}{c} 100K\Omega \\ +50V \\ \\ ** & 1 \end{array}$

- These components are used to stabilize device due to poor high frequency characteristics of burn in board.
- Input signals are calculated to result in internal power dissipation of approximately 2.1W at case temperature = 125°C.