## Data Sheet

## FEATURES

Input start-up voltage range: $\mathbf{2 . 1 5} \mathbf{V}$ to 6.50 V
Operates down to 2.00 V voltage
Ultralow 180 nA quiescent current with no load
Selectable output voltage of 1.2 V to 3.6 V or 0.8 V to 5.0 V
$\pm 1.5 \%$ output accuracy over full temperature range in

## PWM mode

Selectable hysteresis mode or PWM operation mode
Output current
Up to 50 mA in hysteresis mode
Up to $\mathbf{5 0 0}$ mA in PWM mode
VOUTOK flag monitors the output voltage
100\% duty cycle operation mode
2 MHz switching frequency with optional synchronization input from 1.2 MHz to 2.5 MHz
QOD option
UVLO, OCP, and TSD protection
9-ball, $1.65 \mathrm{~mm} \times 1.87 \mathrm{~mm}$ WLCSP
$-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ junction temperature

## APPLICATIONS

Energy (gas and water) metering
Portable and battery-powered equipment
Medical applications
Keep-alive power supplies

## GENERAL DESCRIPTION

The ADP5301 is a high efficiency, ultralow quiescent current step-down regulator that draws only a 180 nA quiescent current to regulate the output at no load.
The ADP5301 runs from an input startup voltage range of 2.15 V to 6.50 V , allowing the use of multiple alkaline/ NiMH , Li-Ion cells, or other power sources. The output voltage is selectable from 0.8 V to 5.0 V by an external VID resistor and factory fuse. The total solution requires only four tiny external components.

The ADP5301 can operate between hysteresis mode and PWM mode via the SYNC/MODE pin. The regulator in hysteresis mode achieves excellent efficiency at a power of less than 1 mW and provides up to 50 mA of output current. The regulator in PWM mode produces a lower output ripple and supplies up to 500 mA of output current. The flexible configuration capability during operation of the device enables very efficient power management to meet both the longest battery life and low system noise requirements.

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12/15-Rev. 0 to Rev. A
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6/15-Revision 0: Initial Version

FUNCTIONAL BLOCK DIAGRAM


Figure 2.

## SPECIFICATIONS

$\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=2.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ for minimum and maximum specifications, and $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ for typical specifications, unless otherwise noted.

Table 1.


| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SW PIN <br> High-Side Power FET On Resistance Low-Side Power FET On Resistance Current-Limit in PWM Mode Peak Current in Hysteresis Mode Minimum On Time | RDS (ON) H <br> RDS (ON) L <br> llim_pwm <br> llim_hys <br> tmin_on | 800 | $\begin{aligned} & 324 \\ & 196 \\ & 1000 \\ & 265 \\ & 40 \end{aligned}$ | $\begin{aligned} & 470 \\ & 320 \\ & 1200 \\ & 70 \end{aligned}$ | $\mathrm{m} \Omega$ <br> $\mathrm{m} \Omega$ <br> mA <br> mA <br> ns | Pin to pin measurement <br> Pin to pin measurement <br> SYNC/MODE = high <br> SYNC/MODE = low |
| VOUTOK PIN <br> Monitor Threshold <br> Monitor Hysteresis <br> Monitor Rising Delay <br> Monitor Falling Delay <br> Leakage Current <br> Output Low Voltage | Voutok (RISE) <br> Voutok (HYS) <br> tvoutok_RISE <br> tvoutok_fall <br> Ivoutok_leakage <br> Voutok_Low | 87 | $\begin{aligned} & 90 \\ & 3 \\ & 40 \\ & 10 \\ & 0.1 \\ & 50 \end{aligned}$ | 93 <br> 1 <br> 80 | \% <br> \% <br> $\mu \mathrm{s}$ <br> $\mu \mathrm{S}$ <br> $\mu \mathrm{A}$ <br> mV | $\mathrm{I}_{\text {voutok }}=100 \mu \mathrm{~A}$ |
| SOFT START Default Soft Start Time Start-Up Delay | tss <br> tstart_delay |  | $\begin{aligned} & 350 \\ & 2 \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ms} \end{aligned}$ | Factory trim, 1 bit ( $350 \mu \mathrm{~s}$ and $2800 \mu \mathrm{~s}$ ) <br> Delay from the EN pin being pulled high |
| Cout DISCHARGE SWITCH ON RESISTANCE | R DIS |  | 290 |  | $\Omega$ |  |
| THERMAL SHUTDOWN <br> Threshold Hysteresis | Tshin Thys |  | $\begin{aligned} & 142 \\ & 127 \end{aligned}$ |  | $\begin{aligned} & { }^{\circ} \mathrm{C} \\ & { }^{\circ} \mathrm{C} \end{aligned}$ |  |

## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :--- | :--- |
| PVIN to PGND | -0.3 V to +7 V |
| SW to PGND | -0.3 V to $\mathrm{PVIN}+0.3 \mathrm{~V}$ |
| FB to AGND | -0.3 V to +7 V |
| VID to AGND | -0.3 V to +7 V |
| EN to AGND | -0.3 V to +7 V |
| VOUTOK to AGND | -0.3 V to +7 V |
| SYNC/MODE to AGND | -0.3 V to +7 V |
| PGND to AGND | -0.3 V to +0.3 V |
| Storage Temperate Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operational Junction Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for the worst case conditions, that is, a device soldered in a circuit board for surface-mount packages.

Table 3. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | Unit |
| :--- | :--- | :--- |
| 9-Ball WLCSP | 132 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

ESD CAUTION

| ESD (electrostatic discharge) sensitive device. |
| :--- | :--- |
| Charged devices and circuit boards can discharge |
| without detection. Although this product features |
| patented or proprietary protection circuitry, damage |
| may occur on devices subjected to high energy ESD. |
| Therefore, proper ESD precautions should be taken to |
| avoid performance degradation or loss of functionality. |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

| (́Ál | (ÁA2) | (́A3) |
| :---: | :---: | :---: |
| sw | pVİ | EN |
|  | ADP5301 |  |
| (́Bi) | (́B2) | (́вз) |
| PGND | AGND | SYNCI |
|  |  |  |
| (́Ci) | (́C2) | (́Cs) |
| voutok | FB | VID |

Figure 3. Pin Configuration (Top View)
Table 4. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| A1 | SW | Switching Node Output for the Regulator. |
| A2 | PVIN | Power Input for the Regulator. |
| A3 | EN | Enable Input for the Regulator. Set this pin to logic low to disable the regulator. |
| B1 | PGND | Power Ground. |
| B2 | AGND | Analog Ground. |
| B3 | SYNC/MODE | Synchronization Input Pin (SYNC). To synchronize the switching frequency of the device to an external <br> clock, connect this pin to an external clock with a frequency from 1.2 MHz to 2.5 MHz. |
|  |  | PWM or Hysteresis Mode Selection Pin (MODE). When this pin is logic high, the regulator operates in PWM <br> mode. When this pin is logic low, the regulator operates in hysteresis mode. |
| C1 | VOUTOK | Output Power-Good Signal. This open-drain output is the power-good signal for the output voltage. <br> C2 |
| C3 | FB | Vid |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {out }}=2.5 \mathrm{~V}, \mathrm{~L}=2.2 \mu \mathrm{H}, \mathrm{C}_{\text {IN }}=\mathrm{Cout}=10 \mu \mathrm{~F}, \mathrm{f}_{\text {sw }}=2 \mathrm{MHz}, \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 4. Hysteresis Efficiency vs. Load Current, Vout $=1.2 \mathrm{~V}$


Figure 5. Hysteresis Efficiency vs. Load Current, Vout $=1.8 \mathrm{~V}$


Figure 6. Hysteresis Efficiency vs. Load Current, Vout $=3.3 \mathrm{~V}$


Figure 7. Hysteresis Efficiency vs. Load Current, Vout $=1.5 \mathrm{~V}$


Figure 8. Hysteresis Efficiency vs. Load Current, Vout $=2.5 \mathrm{~V}$


Figure 9. PWM Efficiency vs. Load Current, Vout =1.2 V


Figure 10. PWM Efficiency vs. Load Current, Vout $=1.5 \mathrm{~V}$


Figure 11. PWM Efficiency vs. Load Current, Vout $=2.5 \mathrm{~V}$


Figure 12. Shutdown Current vs. $V_{I N}, E N=$ Low


Figure 13. PWM Efficiency vs. Load Current, Vout $=1.8 \mathrm{~V}$


Figure 14. PWM Efficiency vs. Load Current, Vout $=3.3 \mathrm{~V}$


Figure 15. Hysteresis Quiescent Current vs. $V_{I N}, S Y N C / M O D E=$ Low


Figure 16. Feedback Voltage vs. Temperature, PWM Mode


Figure 17. High-Side RDS (оN) н VS. VIN


Figure 18. Peak Current Limit vs. Temperature


Figure 19. Feedback Voltage vs. Temperature, Hysteresis Mode


Figure 20. Low-Side RDS(ON)L vs. VIN


Figure 21. Peak Current Limit vs. Vin


Figure 22. UVLO Threshold, Rising and Falling vs. Temperature


Figure 23. Steady Waveform of Hysteresis Mode, $I_{\text {LOAD }}=1 \mathrm{~mA}$
(IL is the Inductor Current)


Figure 24. Soft Start, $I_{\text {LOAD }}=300 \mathrm{~mA}$


Figure 25. Switching Frequency vs. $V_{\text {IN }}$


Figure 26. Steady Waveform of PWM Mode, $I_{\text {LOAD }}=300 \mathrm{~mA}$


Figure 27. Soft Start with Precharge Function


Figure 28. Load Transient of Hysteresis Mode, I LOAD from 0 mA to 50 mA


Figure 29. Line Transient of Hysteresis Mode, $I_{L O A D}=10 \mu \mathrm{~A}, \mathrm{~V}_{\mathbb{I N}}$ from 2.5 V to 6 V


Figure 30. Input Voltage Ramp Up and Ramp Down in Hysteresis Mode


Figure 31. Load Transient of PWM Mode, I LOAD from 125 mA to 375 mA


Figure 32. Line Transient of PWM Mode, $I_{\text {LOAD }}=500 \mathrm{~mA}, \mathrm{~V}_{\mathbb{I}}$ from 2.5 V to 6 V


Figure 33. VOUTOK Function


Figure 34. Output Short Protection


Figure 35. Synchronized to 2.5 MHz


Figure 36. Output Short Recovery


Figure 37. Quick Output Discharge Function

## THEORY OF OPERATION

The ADP5301 is a high efficiency, ultralow quiescent current step-down regulator in a 9-ball WLCSP to meet demanding performance and board space requirements. The device enables direct connection to the wide input voltage range of 2.15 V to 6.50 V , allowing the use of multiple alkaline/ NiMH or Li-Ion cells and other power sources.

## BUCK REGULATOR OPERATION MODES PWM Mode

In PWM mode, the buck regulator in the ADP5301 operates at a fixed frequency that is set by an internal oscillator. At the start of each oscillator cycle, the high-side MOSFET switch turns on and sends a positive voltage across the inductor. The inductor current increases until the current sense signal exceeds the peak inductor current threshold, which turns off the high-side MOSFET switch. This threshold is set by the error amplifier output. During the highside MOSFET off time, the inductor current decreases through the low-side MOSFET until the next oscillator clock pulse starts a new cycle.

## Hysteresis Mode

In hysteresis mode, the buck regulator in the ADP5301 charges the output voltage slightly higher than its nominal output voltage with PWM pulses by regulating the constant peak inductor current. When the output voltage increases until the output sense signal exceeds the hysteresis upper threshold, the regulator enters standby mode. In standby mode, the high-side and low-side MOSFETs and a majority of the circuitry are disabled to allow a low quiescent current as well as high efficiency performance.

During standby mode, the output capacitor supplies energy into the load and the output voltage decreases until it falls below the hysteresis comparator lower threshold. The buck regulator wakes up and generates the PWM pulses to charge the output again.
Because the output voltage occasionally enters standby mode and then recovers, the output voltage ripple in hysteresis mode is larger than the ripple in PWM mode.

## Mode Selection

The ADP5301 includes the SYNC/MODE pin to allow flexible configuration in hysteresis mode or PWM mode.
When a logic high level is applied to the SYNC/MODE pin, the buck regulator is forced to operate in PWM mode. In PWM mode, the regulator can supply up to 500 mA of output current. The regulator can provide lower output ripple and output noise in PWM mode, which is useful for noise sensitive applications.
When a logic low level is applied to the SYNC/MODE pin, the buck regulator is forced to operate in hysteresis mode. In hysteresis mode, the regulator draws only 180 nA of quiescent current typical to regulate the output under zero load, which allows the regulator to act as a keep-alive power supply in a battery-powered system. In hysteresis mode, the regulator supplies up to 50 mA of output current with a relatively large output ripple compared to PWM mode.

The user can alternate between hysteresis mode and PWM mode during operation. The flexible configuration capability during operation of the device enables efficient power management to meet high efficiency and low output ripple requirements when the system switches between active mode and standby mode.

## OSCILLATOR AND SYNCHRONIZATION

The ADP5301 operates at a 2 MHz switching frequency typical in PWM operation mode.
The switching frequency of the ADP5301 can be synchronized to an external clock with a frequency range from 1.2 MHz to 2.5 MHz. The ADP5301 automatically detects the presence of an external clock applied to the SYNC/MODE pin, and the switching frequency transitions to the frequency of the external clock. When the external clock signal stops, the device automatically switches back to the internal clock.

## ADJUSTABLE AND FIXED OUTPUT VOLTAGES

The ADP5301 provides adjustable output voltage settings by connecting one resistor through the VID pin to AGND. The VID detection circuitry works in the start-up period, and the voltage ID code is sampled and held into the internal register and does not change until the next power recycle. Furthermore, the ADP5301 provides a fixed output voltage programmed via the factory fuse. In this condition, connect the VID pin to the PVIN pin.
For the output voltage settings, the feedback resistor divider is built into the ADP5301, and the feedback pin (FB) must be tied directly to the output. An ultralow power voltage reference and an integrated high impedance ( $50 \mathrm{M} \Omega$ typical) feedback divider network contribute to the low quiescent current. Table 5 lists the output voltage options by the VID pin configurations.

Table 5. Output Voltage (Vout) Options Using the VID Pin

| VID Configuration | $\mathrm{V}_{\text {out }}(\mathrm{V})$ |  |
| :---: | :---: | :---: |
|  | Factory Option 0 | Factory Option 1 |
| Short to Ground | 3.0 | 3.1 |
| Short to PVIN | 2.5 | 1.3 |
| Rvid $=499 \mathrm{k} \Omega$ | 3.6 | 5.0 |
| $\mathrm{Rvid}=316 \mathrm{k} \Omega$ | 3.3 | 4.5 |
| Rvid $=226 \mathrm{k} \Omega$ | 2.9 | 4.2 |
| $\mathrm{R}_{\mathrm{viD}}=174 \mathrm{k} \Omega$ | 2.8 | 3.9 |
| $\mathrm{Rvid}=127 \mathrm{k} \Omega$ | 2.7 | 3.4 |
| Rvid $=97.6 \mathrm{k} \Omega$ | 2.6 | 3.2 |
| Rvid $=76.8 \mathrm{k} \Omega$ | 2.4 | 1.9 |
| RYID $=56.2 \mathrm{k} \Omega$ | 2.3 | 1.7 |
| $\mathrm{R}_{\mathrm{vid}}=43 \mathrm{k} \Omega$ | 2.2 | 1.6 |
| Rvid $=32.4 \mathrm{k} \Omega$ | 2.1 | 1.4 |
| Rvid $=25.5 \mathrm{k} \Omega$ | 2.0 | 1.1 |
| $\mathrm{R}_{\mathrm{VID}}=19.6 \mathrm{k} \Omega$ | 1.8 | 1.0 |
| Rvid $=15 \mathrm{k} \Omega$ | 1.5 | 0.9 |
| RVID $=11.8 \mathrm{k} \Omega$ | 1.2 | 0.8 |

## UNDERVOLTAGE LOCKOUT (UVLO)

The undervoltage lockout circuitry monitors the input voltage level on the PVIN pin. If input voltage falls below 2.00 V (typical), the regulator turns off. After the input voltage rises above 2.06 V (typical), the soft start period is initiated, and the regulator is enabled when the EN pin is high.

## ENABLE/DISABLE

The ADP5301 includes a separate enable pin (EN). A logic high in the EN pin starts the regulator. Due to the low quiescent current design, it is typical for the regulator to start switching after a delay of a few milliseconds from the EN pin being pulled high.
A logic low on the EN pin immediately disables the regulator and brings the regulator into extremely low current consumption.

## CURRENT LIMIT

The buck regulator in the ADP5301 has protection circuitry that limits the direction and the amount of current to a certain level that flows through the high-side MOSFET and the low-side MOSFET in cycle-by-cycle mode. The positive current limit on the high-side MOSFET limits the amount of current that can flow from the input to the output. The negative current limit on the low-side MOSFET prevents the inductor current from reversing direction and flowing out of the load.

## SHORT-CIRCUIT PROTECTION

The buck regulator in ADP5301 includes frequency foldback to prevent current runaway on a hard short. When the output voltage at the FB pin falls below 0.3 V typical, indicating the possibility of a hard short at the output, the switching frequency (in PWM mode) is reduced to one-fourth of the internal oscillator frequency. The reduction in the switching frequency allows more time for the inductor to discharge, preventing a runaway of output current.

## SOFT START

The ADP5301 has an internal soft start function that ramps up the output voltage in a controlled manner upon startup, thereby limiting the inrush current. This feature prevents possible input voltage drops when a battery or a high impedance power source is connected to the input of the device. The default typical soft start time is $350 \mu$ s for the regulator.
A different soft start time ( $2800 \mu \mathrm{~s}$ ) can be programmed for ADP5301 by the factory fuse.

## STARTUP WITH A PRECHARGED OUTPUT

The buck regulator in the ADP5301 includes a precharged start-up feature to protect the low-side MOSFET from damage during startup. If the output voltage is precharged before the regulator turns on, the regulator prevents reverse inductor current-which discharges the output capacitor-until the internal soft start reference voltage exceeds the precharged voltage on the feedback pin.

## 100\% DUTY CYCLE OPERATION

When the input voltage approaches the output voltage, the ADP5301 stops switching and enters $100 \%$ duty cycle operation. It connects the output via the inductor and the internal high-side power switch to the input. When the input voltage is charged again and the required duty cycle falls to $95 \%$ typical, the buck immediately restarts switching and regulation without allowing overshoot on the output voltage. In hysteresis mode, the ADP5301 draws an ultralow quiescent current of only 570 nA typical during $100 \%$ duty cycle operation

## ACTIVE DISCHARGE

The ADP5301 integrates an optional, factory programmable discharge switch from the switching node to ground. This switch turns on when its associated regulator is disabled, which helps discharge the output capacitor quickly. The typical value of the discharge switch is $290 \Omega$ for the regulator.
By default, the discharge function is not enabled. The active discharge function can be enabled by the factory fuse.

## VOUTOK FUNCTION

The ADP5301 includes an open-drain power-good output (VOUTOK pin) that is active high when the buck regulator is operating normally. By default, the VOUTOK pin monitors the output voltage. A logic high on the VOUTOK pin indicates that the regulated output voltage of the buck regulator is above $90 \%$ (typical) of its nominal output. When the regulated output voltage of the buck regulator falls below $87 \%$ (typical) of its nominal output for a delay time greater than approximately $10 \mu \mathrm{~s}$, the VOUTOK pin goes low.

## THERMAL SHUTDOWN

If the ADP5301 junction temperature exceeds $142^{\circ} \mathrm{C}$, the thermal shutdown circuit turns off the IC except for the internal linear regulator. Extreme junction temperatures can be the result of high current operation, poor circuit board design, or high ambient temperature. A $15^{\circ} \mathrm{C}$ hysteresis is included so that the ADP5301 does not return to operation after thermal shutdown until the junction temperature falls below $127^{\circ} \mathrm{C}$. When the device exits thermal shutdown, a soft start is initiated for the buck regulator.

## ADP5301

## APPLICATIONS INFORMATION

This section describes the external components selection for the ADP5301. A typical application circuit is shown in Figure 38.


Figure 38. Typical Application Circuit

## EXTERNAL COMPONENT SELECTION

The ADP5301 is optimized for operation with a $2.2 \mu \mathrm{H}$ inductor and $10 \mu \mathrm{~F}$ output capacitors for various output voltages using the closed-loop compensation and adaptive slope compensation circuits. The selection of components depends on the efficiency, the load current transient, and other application requirements. The trade-offs among performance parameters, such as efficiency and transient response, are made by varying the choice of external components.

## SELECTING THE INDUCTOR

The high switching frequency of the ADP5301 allows the use of small surface-mount power inductors. The dc resistance (DCR) value of the selected inductor affects efficiency. In addition, it is recommended to select a multilayer inductor rather than a magnetic iron inductor because the high switching frequency increases the core temperature rise and enlarges the core loss.

A minimum requirement of the dc current rating of the inductor is for it to be equal to the maximum load current plus half of the inductor current ripple $\left(\Delta \mathrm{I}_{\mathrm{L}}\right)$, as shown by the following equations:

$$
\begin{aligned}
& \Delta I_{L}=V_{O U T}+\left(\frac{1-\frac{V_{O U T}}{V_{I N}}}{L \times f_{S W}}\right) \\
& I_{P K}=I_{L O A D(M A X)}+\left(\frac{\Delta I_{L}}{2}\right)
\end{aligned}
$$

Use the inductor series from different vendors shown in Table 6.

## OUTPUT CAPACITOR

Output capacitance is required to minimize the voltage overshoot, the voltage undershoot, and the ripple voltage present on the output. Capacitors with low equivalent series resistance (ESR) values produce the lowest output ripple. Furthermore, use capacitors such as X5R and X7R dielectric capacitors. Do not use Y5V and Z5U capacitors, which are unsuitable choices due to their large capacitance variation over temperature and their dc bias voltage changes. Because ESR is important, select the capacitor using the following equation:

$$
E S R_{\text {COUT }} \leq \frac{V_{\text {RIPPLE }}}{\Delta I_{L}}
$$

where:
$E S R_{\text {cout }}$ is the ESR of the chosen capacitor.
$V_{\text {RIPPLE }}$ is the peak-to-peak output voltage ripple.
Increasing the output capacitor value has no effect on stability and may reduce output ripple and enhance load transient response. When choosing the output capacitor value, it is important to account for the loss of capacitance due to output voltage dc bias.
Use the capacitor series from different vendors shown in Table 7.

Table 6. Recommended Inductors

| Vendor | Model | Inductance $(\boldsymbol{\mu H})$ | Dimensions $(\mathbf{m m})$ | DCR $(\mathbf{m} \boldsymbol{\Omega})$ | I $_{\text {SAT }}{ }^{\mathbf{1}}(\mathbf{A})$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| TDK | MLP2016V2R2MTOS1 | 2.2 | $2.0 \times 1.6 \times 0.85$ | 280 | 1.0 |
| Wurth | 74479889222 | 2.2 | $2.5 \times 2.0 \times 1.2$ | 250 | 1.7 |
| Coilcraft | LPS3314-222MR | 2.2 | $3.3 \times 3.3 \times 1.3$ | 100 | 1.5 |

${ }^{1} I_{\text {SAT }}$ is the dc current at which the inductance drops $30 \%$ (typical) from its value without current.

Table 7. Input and Output Capacitors

| Vendor | Model | Capacitance $(\boldsymbol{\mu F})$ | Size |
| :--- | :--- | :--- | :--- |
| Murata | GRM188D71A106MA73 | 10 | 0603 |
| Murata | GRM21BR71A106KE51 | 10 | 0805 |
| Murata | GRM31CR71A106KA01 | 10 | 1206 |

## INPUT CAPACITOR

An input capacitor is required to reduce the input voltage ripple, input ripple current, and source impedance. Place the input capacitor as close as possible to the PVIN pin. A low ESR X7R or X5R capacitor is highly recommended to minimize the input voltage ripple. Use the following equation to determine the rms input current:

$$
I_{R M S} \geq I_{\text {LOAD }(M A X)} \sqrt{\frac{V_{\text {OUT }}\left(V_{I N}-V_{O U T}\right)}{V_{I N}}}
$$

For most applications, a $10 \mu \mathrm{~F}$ capacitor is sufficient. The input capacitor can be increased without any limit for better input voltage filtering.

## EFFICIENCY

Efficiency is the ratio of output power to input power. The high efficiency of the ADP5301 has two distinct advantages. First, only a small amount of power is lost in the dc-to-dc converter package, which in turn reduces thermal constraints. Second, the high efficiency delivers the maximum output power for the given input power, thereby extending battery life in portable applications.

## Power Switch Conduction Losses

Power switch dc conduction losses are caused by the flow of output current through the high-side P-channel power switch and the low-side N -channel synchronous rectifier, which have internal resistances ( $\mathrm{R}_{\mathrm{DS} \text { (ON) }}$ ) associated with them. The amount of power loss is approximated by

$$
P_{S W_{-C O N D}}=\left(R_{D S(O N) H} \times D+R_{D S(O N) L} \times(1-D)\right) \times I_{O U T}{ }^{2}
$$

where:

$$
D=\frac{V_{O U T}}{V_{I N}}
$$

The internal resistance of the power switches increases with temperature and with the input voltage decrease.

## Inductor Losses

Inductor conduction losses are caused by the flow of current through the inductor, which has an internal DCR associated with it. Larger size inductors have smaller DCR, which can decrease inductor conduction losses. Inductor core losses relate to the magnetic permeability of the core material. Because the ADP5301 is a high switching frequency dc-to-dc regulator, shielded ferrite core material is recommended because of its low core losses and low electromagnetic interference (EMI).

To estimate the total amount of power lost in the inductor, use the following equation:

$$
P_{L}=D C R \times I_{\text {out }}{ }^{2}+\text { Core Losses }
$$

## Driver Losses

Driver losses are associated with the current drawn by the driver to turn on and turn off the power devices at the switching frequency. Each time a power device gate is turned on and turned off, the driver transfers a charge from the input supply to the gate, and then from the gate to ground.

Estimate driver losses using the following equation:

$$
P_{\text {DRIVER }}=\left(C_{G A T E_{-} H}+C_{G A T E_{-} L}\right) \times V_{I N}{ }^{2} \times f_{S W}
$$

where:
$C_{G A T E-H}$ is the gate capacitance of the internal high-side switch. $C_{G A T E} L$ is the gate capacitance of the internal low-side switch. $f_{S W}$ is the switching frequency in PWM mode.
The typical values for the gate capacitances are 69 pF for $\mathrm{C}_{\text {GATE_H }}$ and 31 pF for $\mathrm{C}_{\text {GATE_L }}$.

## Transition Losses

Transition losses occur because the P-channel switch cannot turn on or turn off instantaneously. In the middle of a switch node transition, the power switch provides all of the inductor current. The source to drain voltage of the power switch is half of the input voltage, resulting in power loss. Transition losses increase with both load current and input voltage and occur twice for each switching cycle.
Use the following equation to estimate transition losses:

$$
P_{\text {TRAN }}=V_{\text {IN }} / 2 \times I_{\text {OUT }} \times\left(t_{R}+t_{F}\right) \times f_{S W}
$$

where:
$t_{R}$ is the rise time of the SW node.
$t_{F}$ is the fall time of the SW node.
The typical value for the rise and fall times, $\mathrm{t}_{\mathrm{R}}$ and $\mathrm{t}_{\mathrm{F}}$, is 2 ns .

## PRINTED CIRCUIT BOARD (PCB) LAYOUT RECOMMENDATIONS



## TYPICAL APPLICATION CIRCUITS

The ADP5301 can be used as a keep-alive, ultralow step-down power regulator to extend the battery life (see Figure 40) and as a batterypowered equipment or wireless sensor network controlled by a microcontroller or a processor (see Figure 41).


Figure 40. Typical ADP5301 Application with Li-Ion Battery


Figure 41. Typical ADP5301 Application with Two Alkaline/NiMH Batteries

## FACTORY PROGRAMMABLE OPTIONS

To order a device with options other than the default options, contact your local Analog Devices sales or distribution representative.
Table 8. Output Voltage VID Setting Options

| Option | Description |
| :--- | :--- |
| Option 0 | VID resistor to set the output voltage as: $1.2 \mathrm{~V}, 1.5 \mathrm{~V}, 1.8 \mathrm{~V}, 2.0 \mathrm{~V}, 2.1 \mathrm{~V}, 2.2 \mathrm{~V}, 2.3 \mathrm{~V}, 2.4 \mathrm{~V}, 2.5 \mathrm{~V}, 2.6 \mathrm{~V}, 2.7 \mathrm{~V}, 2.8 \mathrm{~V}, 2.9 \mathrm{~V}, 3.0 \mathrm{~V}, 3.3 \mathrm{~V}$, or |
|  | 3.6 V (default) |
| Option 1 | VID resistor to set the output voltage as: $0.8 \mathrm{~V}, 0.9 \mathrm{~V}, 1.0 \mathrm{~V}, 1.1 \mathrm{~V}, 1.3 \mathrm{~V}, 1.4 \mathrm{~V}, 1.6 \mathrm{~V}, 1.7 \mathrm{~V}, 1.9 \mathrm{~V}, 3.1 \mathrm{~V}, 3.4 \mathrm{~V}, 3.9 \mathrm{~V}, 4.2 \mathrm{~V}, 4.5 \mathrm{~V}$, or 5.0 V |

Table 9. Output Discharge Functionality Options

| Option | Description |
| :--- | :--- |
| Option 0 | Output discharge function disabled for buck regulator (default) |
| Option 1 | Output discharge function enabled for buck regulator |

Table 10. Soft Start Time Options

| Option | Description |
| :--- | :--- |
| Option 0 | $350 \mu \mathrm{~s}$ (default) |
| Option 1 | $2800 \mu \mathrm{~s}$ |

## OUTLINE DIMENSIONS



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Figure 42. 9-Ball Wafer Level Chip Scale Package [WLCSP] (CB-9-6)
Dimensions shown in millimeters
ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| ADP5301ACBZ-1-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 9-Ball WLCSP, Output Voltage Option 0 with Output Discharge | CB-9-6 |
| ADP5301ACBZ-2-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 9-Ball WLCSP, Output Voltage Option 0 Without Output Discharge | CB-9-6 |
| ADP5301ACBZ-3-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 9-Ball WLCSP, Output Voltage Option 1 with Output Discharge | CB-9-6 |
| ADP5301-EVALZ |  | Evaluation Board |  |

[^0]
[^0]:    ${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.

