

## Multiplexed diagnostics of AC switches using two STCC08

### Introduction

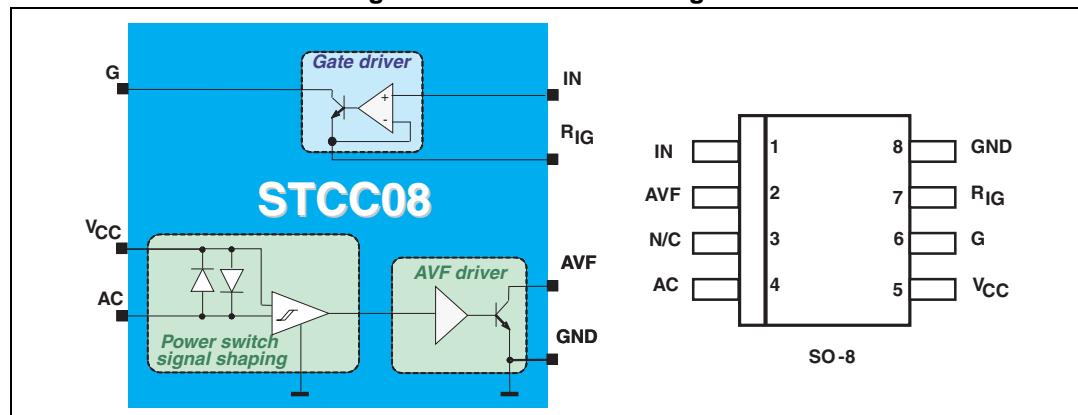
The aim of this application note is to present opportunities to reduce the number of input pins used on a microcontroller unit (MCU) to diagnose failures of several AC switches with the STCC08. This document deals with the multiplexed diagnostics of two STCC08 and gives technical recommendations on the implementation of this solution.

### STCC08 overview

The STCC08 has been designed to improve home appliance safety. This new device can drive an AC switch (Triac, ACST and ACS) with a gate current  $I_{GT}$  up to 10 mA and to send back to the microcontroller unit a signal image of the voltage across the controlled AC switch (this signal defines the AC switch state). The STCC08 has three functional blocks (see *Figure 1*).

- A "gate driver" block used to drive an AC switch and to interface directly the STCC08 with the MCU (CMOS compatible)
- A "power switch signal shaping" block used to measure the AC switch voltage in both AC line cycles
- An "AVF driver" block used to give an image of the AC switch voltage to the MCU (digital information)

**Figure 1. STCC08 block diagram**



For more information about the STCC08, please refer to the ST Application note AN2716.

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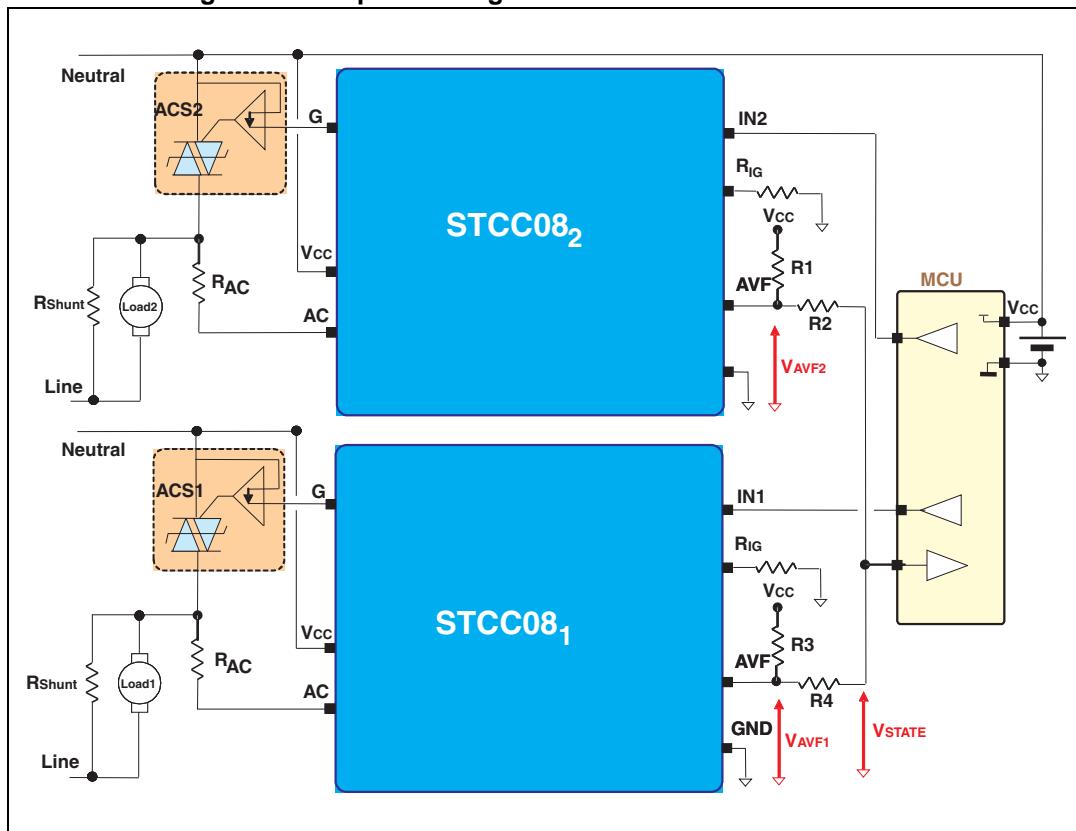
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# 1 Multiplexed diagnostics

## 1.1 Principle

The multiplexed diagnostic allows the detection of the state of several AC switches independently using only one MCU input. In this case, an analog/digital converter input (ADC) of the MCU should be used and must be configured with no pull-up resistor. In this document, only the multiplexed diagnostic of two STCC08 (STCC08<sub>1</sub> and STCC08<sub>2</sub>) is described (see [Figure 2](#)). Note that two output pins of an MCU should be used to control each STCC08 (IN1 and IN2).

**Figure 2. Multiplexed diagnostic schematic of two STCC08**



To distinguish the state of each AC switch (ACS1 and ACS2) a divider bridge is used. Resistors R<sub>1</sub>, R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub> are designed to convert the V<sub>AVF</sub> digital signal given by each STCC08 (V<sub>AVF1</sub> and V<sub>AVF2</sub>) into an analog signal (V<sub>STATE</sub>). Knowing the control state of each STCC08 (IN1 and IN2), the MCU is able to identify the state of each AC switch by analyzing the V<sub>STATE</sub> signal (see [Section 1.2](#)).

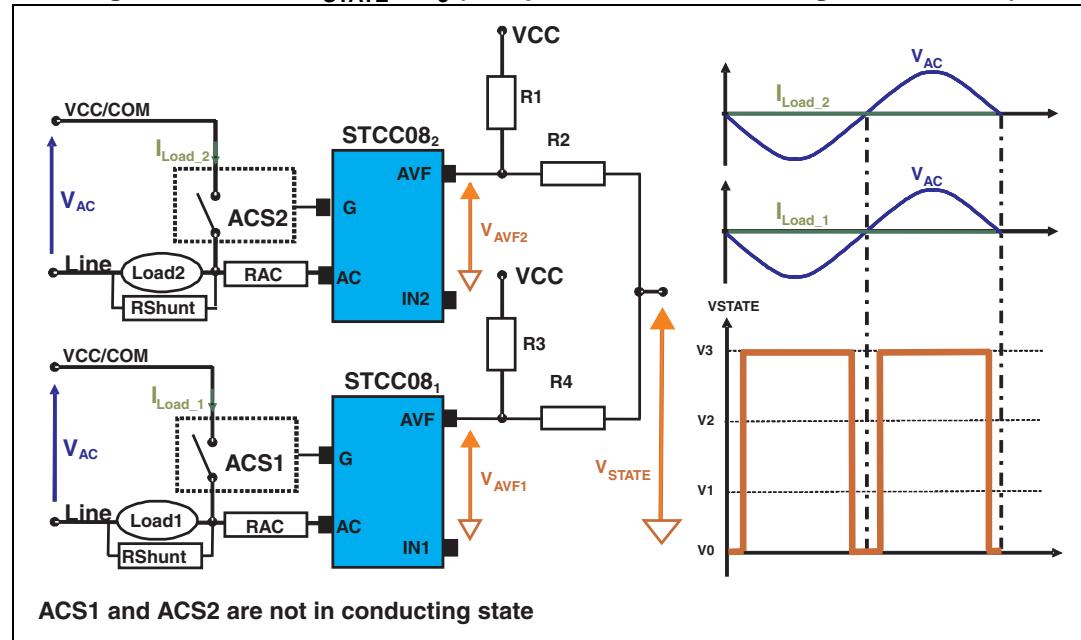
Note:

The STCC08 AVF output is an open collector output. Resistors R<sub>1</sub> and R<sub>3</sub> bias the STCC08 AVF output and limit the collector current to 5 mA. For further information, and in particular, resistor values for R<sub>AC</sub>, R<sub>shunt</sub>, and R<sub>IG</sub> refer to the ST Application note AN2716.

## 1.2 Failure mode detection of two AC switches

*Figure 3 to Figure 12* give the  $V_{STATE}$  signal level according to the state of each AC switch.  $V_0$ ,  $V_1$ ,  $V_2$  and  $V_3$  are levels reached by the parameter  $V_{STATE}$  and depends on  $R1$ ,  $R2$ ,  $R3$ , and  $R4$  resistor values. *Table 1* shows that we only need four different levels to define the state of each AC switch.

**Figure 3. Case 1:  $V_{STATE} = V_3$  (except at each zero crossing of the AC line)**



**Figure 4. Case 2:  $V_{STATE} = V_0$**

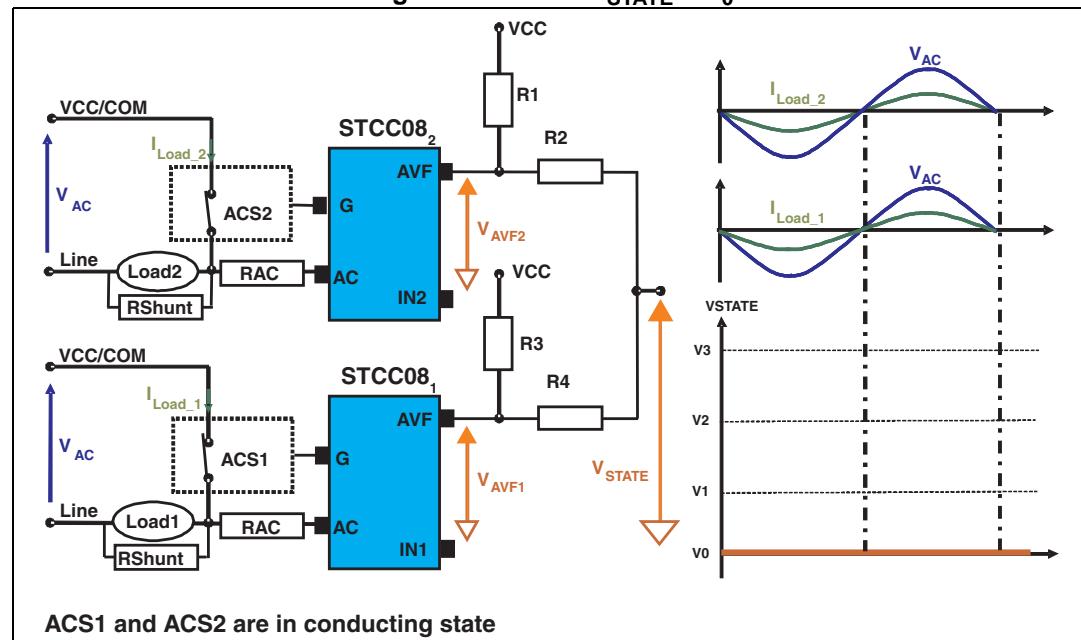
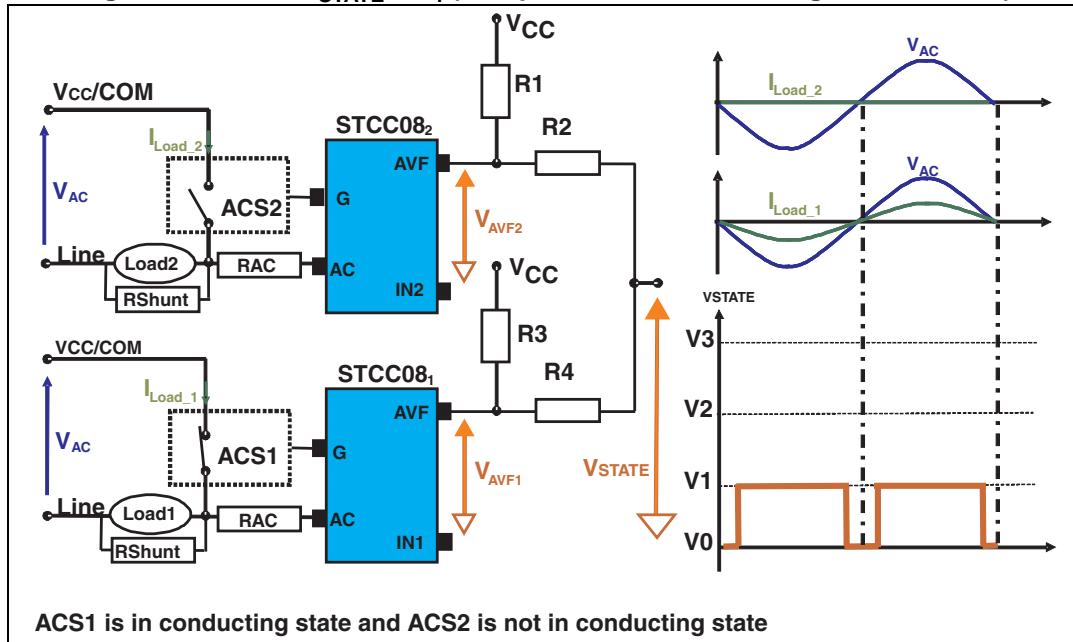
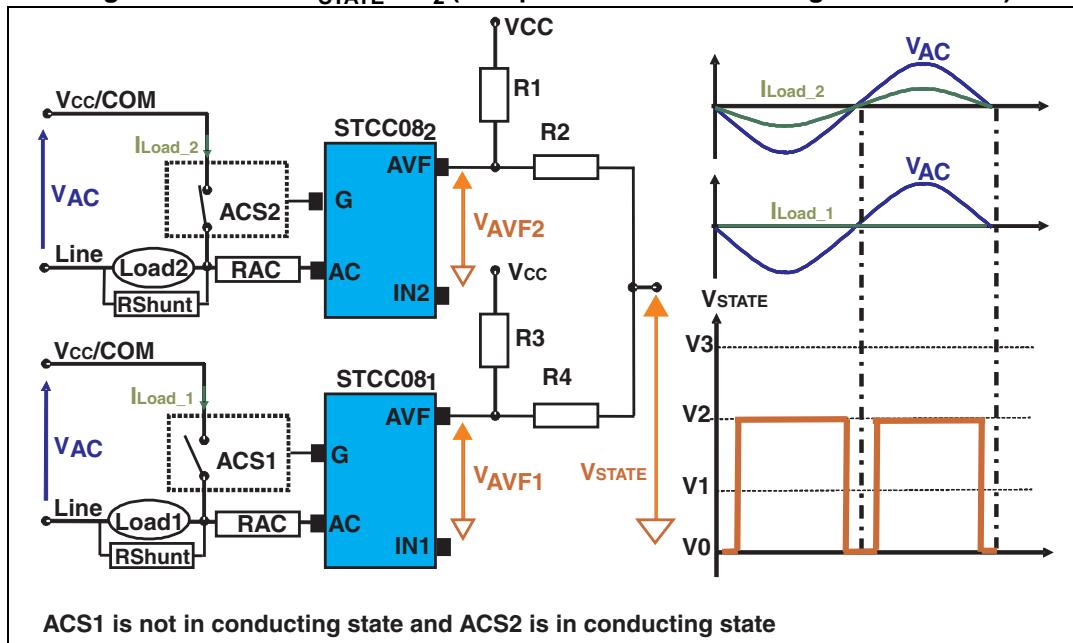
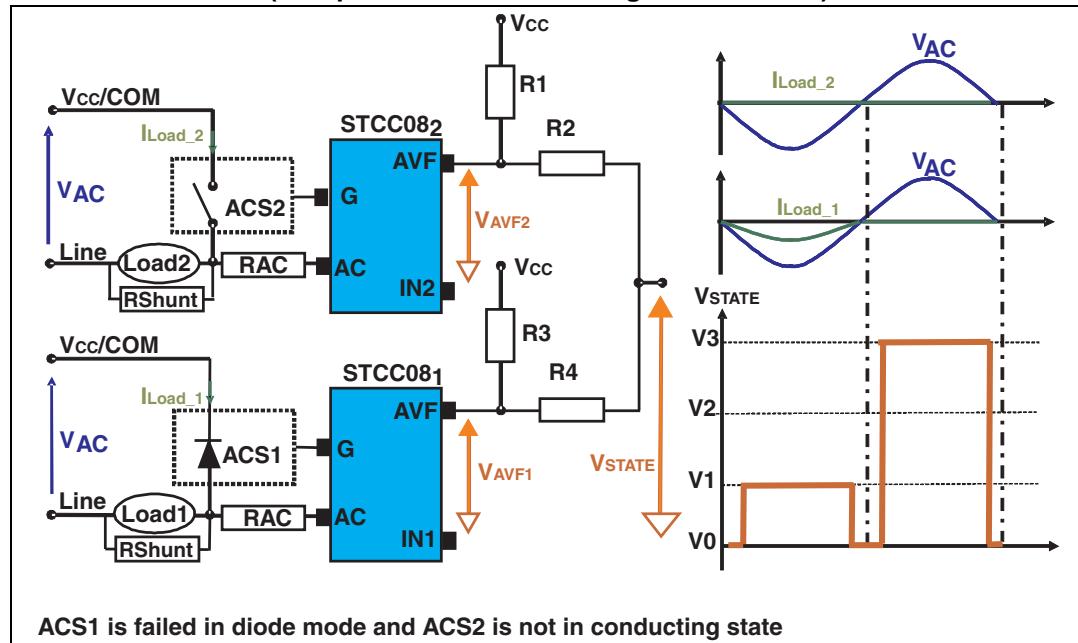
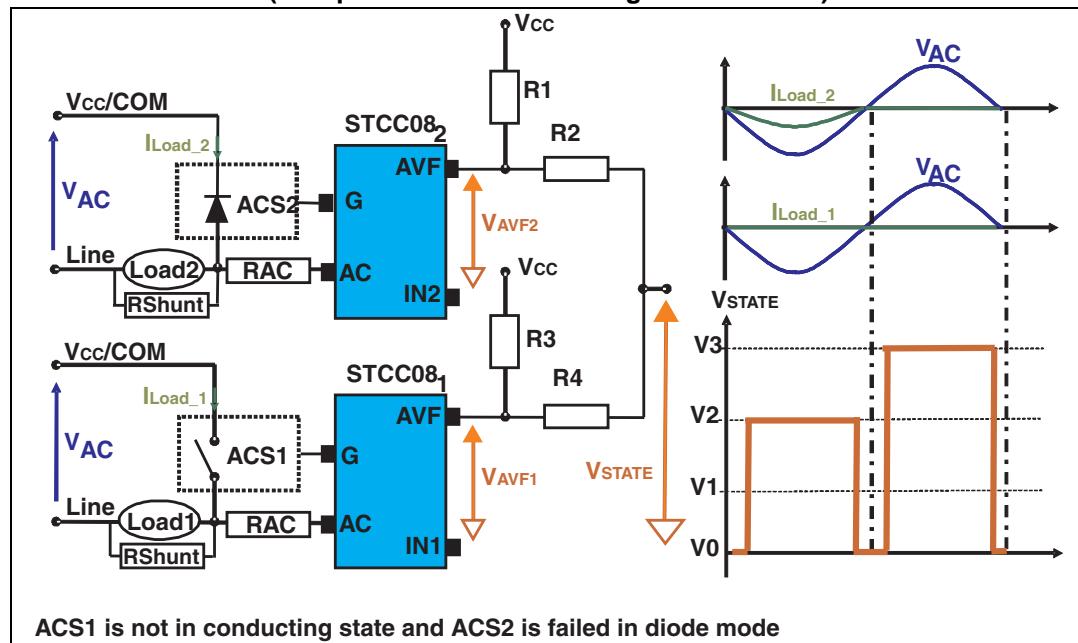


Figure 5. Case 3:  $V_{STATE} = V_1$  (except at each zero crossing of the AC line)Figure 6. Case 4:  $V_{STATE} = V_2$  (except at each zero crossing of the AC line)

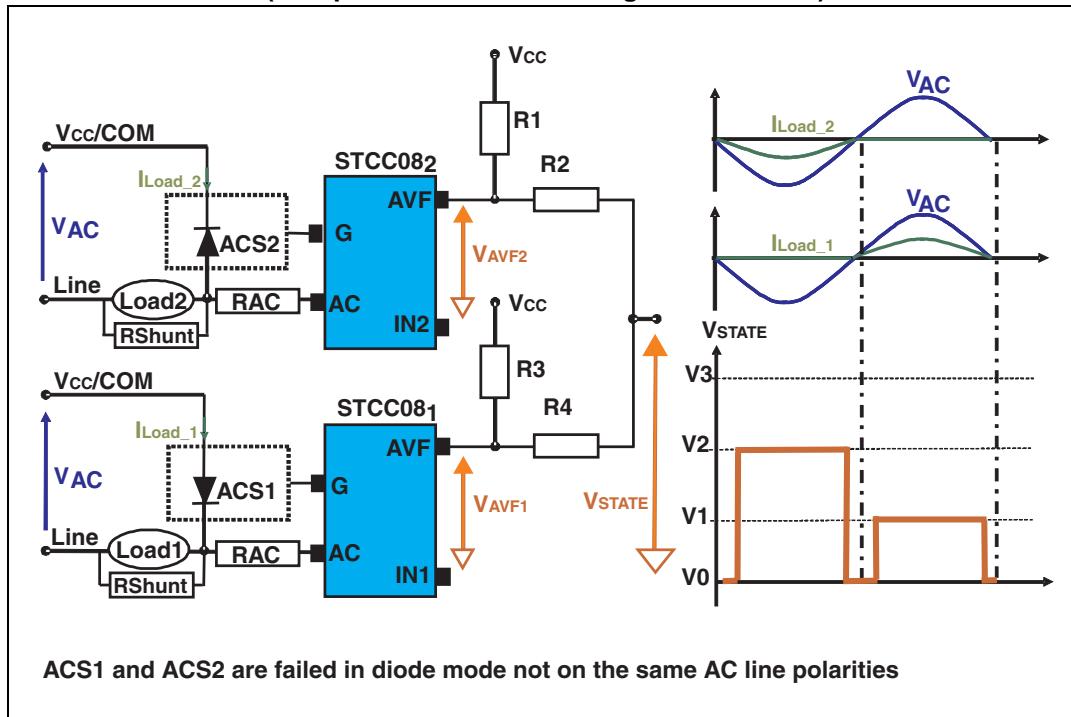
**Figure 7. Case 5:  $V_{STATE}$  toggles between  $V_1$  and  $V_3$  at each AC line cycle  
(except at each zero crossing of the AC line)**



**Figure 8. Case 6:  $V_{STATE}$  toggles between  $V_2$  and  $V_3$  at each AC line cycle  
(except at each zero crossing of the AC line)**

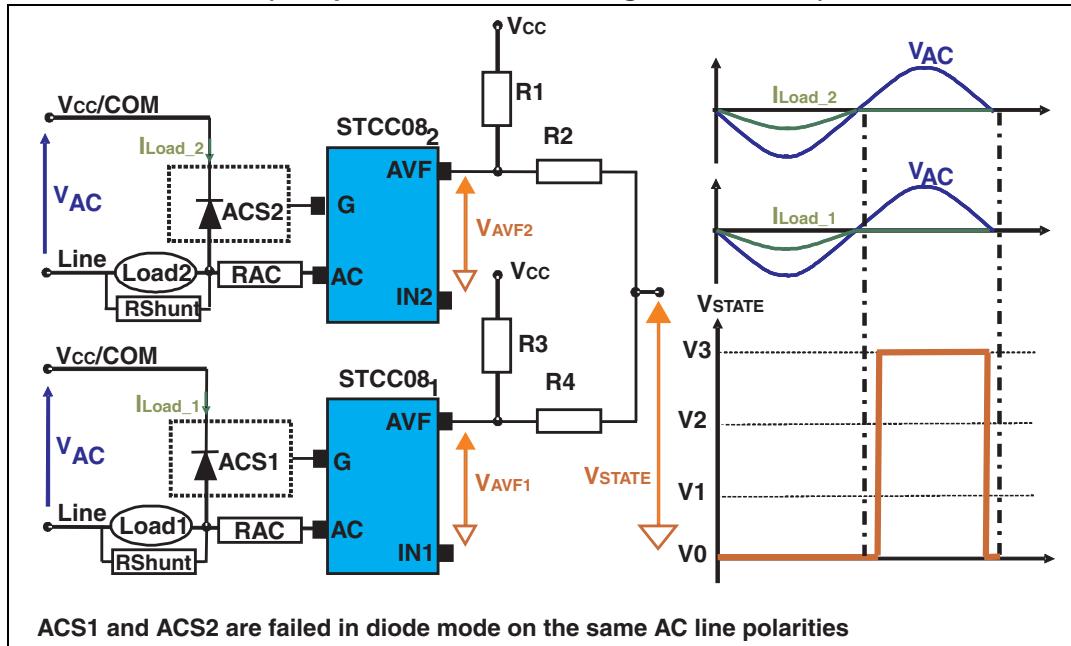


**Figure 9. Case 7:  $V_{STATE}$  toggles between  $V_1$  and  $V_2$  at each AC line cycle  
(except at each zero crossing of the AC line)**

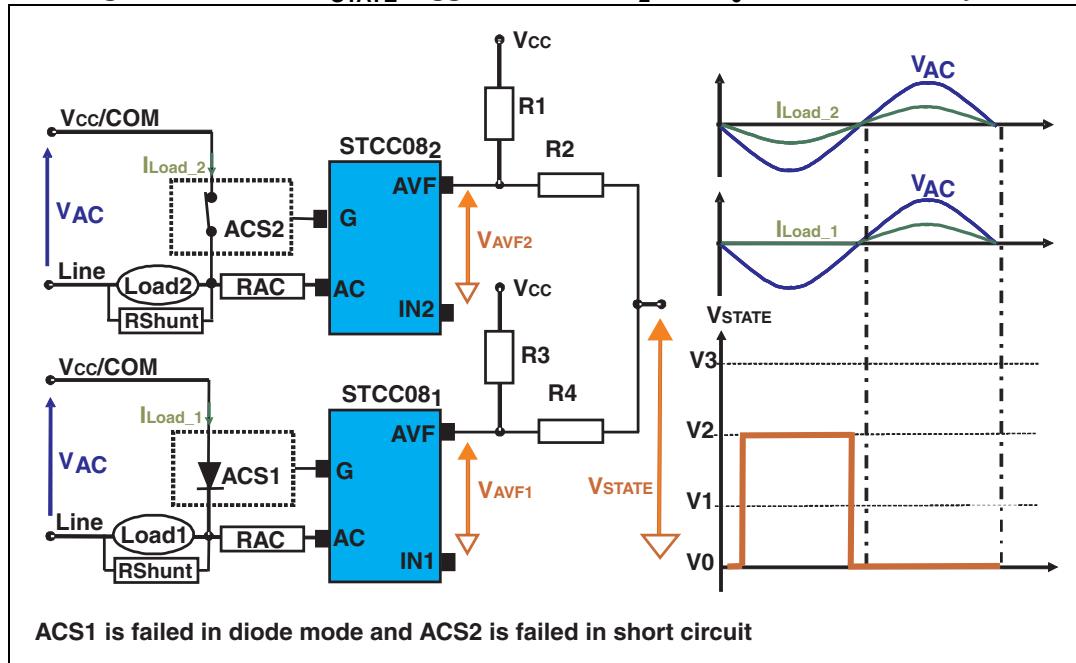
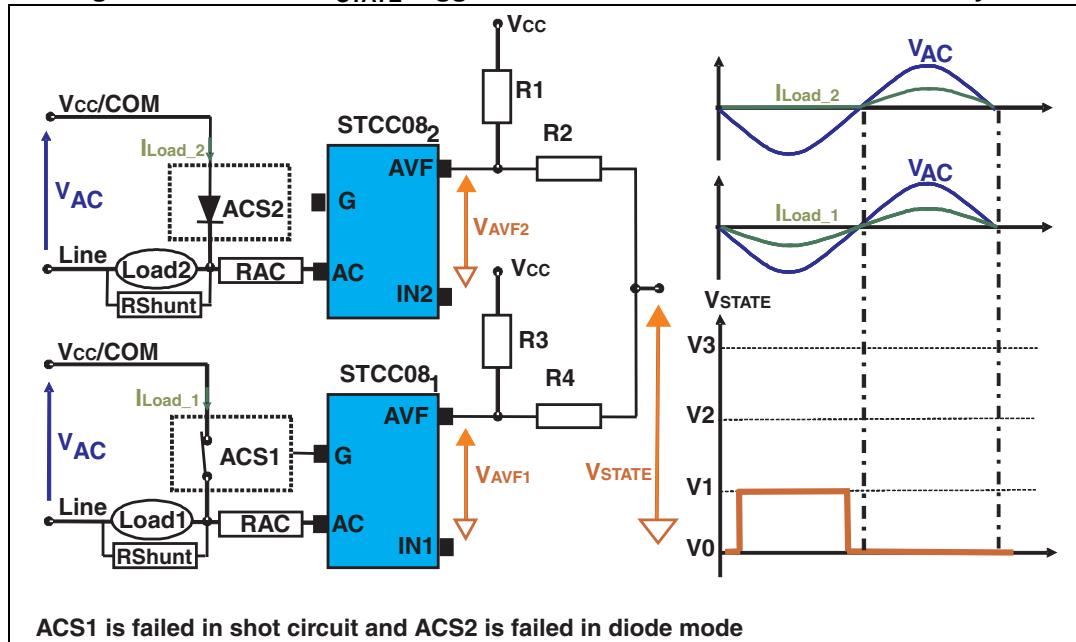


ACS1 and ACS2 are failed in diode mode not on the same AC line polarities

**Figure 10. Case 8:  $V_{STATE}$  toggles between  $V_0$  and  $V_3$  at each AC line cycle  
(except at each zero crossing of the AC line)**



ACS1 and ACS2 are failed in diode mode on the same AC line polarities

Figure 11. Case 9:  $V_{STATE}$  toggles between  $V_2$  and  $V_0$  at each AC line cycleFigure 12. Case 10:  $V_{STATE}$  toggles between  $V_1$  and  $V_0$  at each AC line cycle

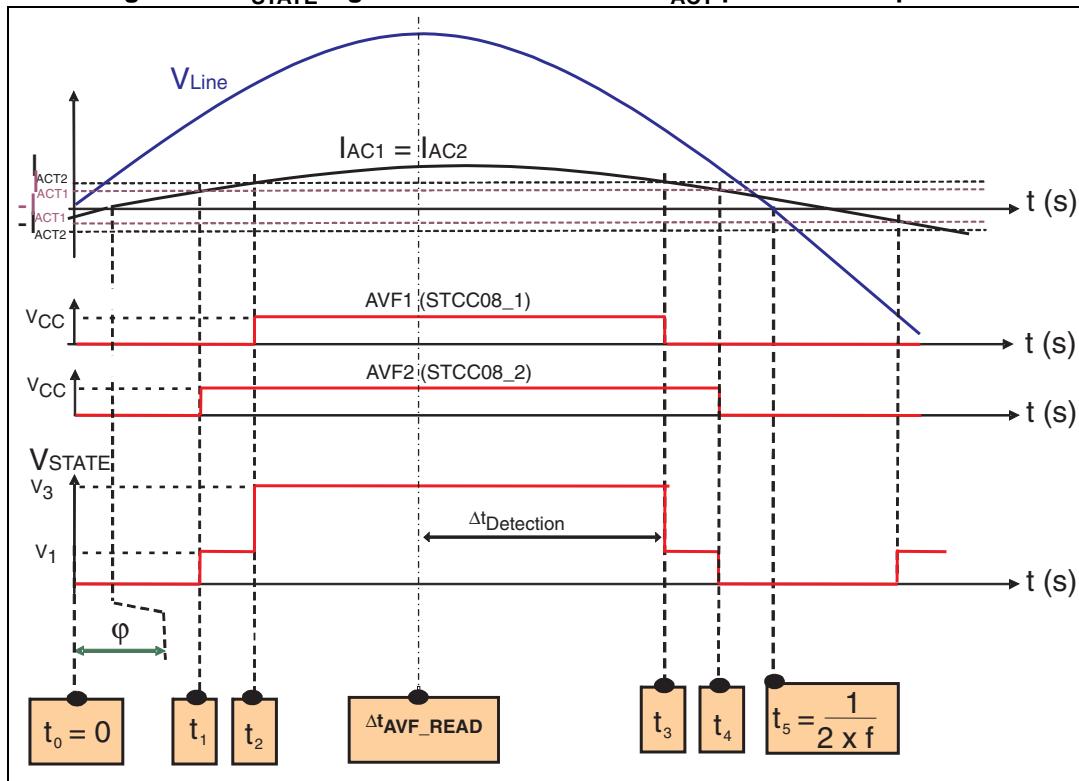
**Table 1. Variation of the  $V_{STATE}$  signal according to the AC switch states**

ACS1 state	ACS2 state	$V_{STATE}$ status
ON	ON	$V_{STATE} = V_0$
ON	OFF	$V_{STATE} = V_1$
OFF	ON	$V_{STATE} = V_2$
OFF	OFF	$V_{STATE} = V_3$

Knowing the control state of each STCC08 (IN1 and IN2) and according to [Table 1](#), the MCU is able to detect the AC switch state by analyzing  $V_{STATE}$  signal. [Appendix A](#) defines the states of each ACS according to the  $V_{STATE}$  signal level ( $V_0$ ,  $V_1$ ,  $V_2$  and  $V_3$ ) and the control state of each STCC08. In the case of failure of one of the AC switches, the MCU can place the application in a safe configuration by switching off an appliance front-end relay.

### 1.3 $V_{AVF}$ signal reading synchronization

The STCC08 AVF output signal is an image of the AC switch voltage. This signal toggles between  $V_{CC}$  and zero level (GND) according to whether the STCC08 AC input current ( $I_{AC}$ ) is higher or not than  $I_{ACT}$  (see AN2716). In case of multiplexed diagnostics the slight  $I_{ACT}$  electrical variation between ICs may result in the state of the AVF signal of each STCC08 (either  $V_{CC}$  or zero level) not changing at exactly the same time. This has an impact on the  $V_{STATE}$  signal and on the AC switches state detection (see [Figure 13](#)). Note that  $I_{ACT1}$  and  $I_{ACT2}$  define respectively the STTC08  $I_{AC}$  input current for STCC08<sub>1</sub> and STCC08<sub>2</sub> to allow  $V_{AVF}$  signal to toggle between  $V_{CC}$  and GND. For example, if the two STCC08 are not controlled ( $IN1 = IN2 = 0$ ) and AC1 and AC2 are not in conducting state the AC1 and AC2 can be interpreted (see [Table 1](#)) as failed in short circuit if  $V_{STATE}$  is read between  $t_0$  and  $t_1$  ( $V_{STATE} = V_0$ ).

Figure 13.  $V_{STATE}$  signal variation due to the  $I_{ACT}$  parameter dispersion

Note: It is recommended that the AVF signal be read during several AC line cycles around the AC line peak voltage.

The STCC08 AVF signal must be read after the AC line peak voltage ( $\Delta t_{AVF\_READ}$ ) and before the  $t_3$  (see AN2716).

## 2 V<sub>STATE</sub> level definition

According to the state of each AC switch, V<sub>0</sub>, V<sub>1</sub>, V<sub>2</sub> and V<sub>3</sub> levels are defined by equations [1](#), [2](#), [3](#) and [4](#) (see also [Appendix B](#)). In this document V<sub>AVF1\_L</sub> and V<sub>AVF2\_L</sub> are respectively the STCCO8<sub>1</sub> and STCCO8<sub>2</sub> AVF output at the low level. The minimum and maximum values of AVF at low level are respectively 0 V and 1 V.

### Equation 1

ACS1 and ACS2 are on

$$V_0 = \frac{(V_{AVF1\_L} \cdot R_2 + V_{AVF2\_L} \cdot R_4)}{R_2 + R_4}$$

### Equation 2

ACS1 is on and ACS2 is off

$$V_1 = \frac{V_{CC} \cdot R_4 + V_{AVF1\_L} \cdot (R_1 + R_2)}{R_1 + R_2 + R_4}$$

### Equation 3

ACS2 is on and ACS1 is off

$$V_2 = \frac{V_{CC} \cdot R_2 + V_{AVF2\_L} \cdot (R_3 + R_4)}{R_2 + R_3 + R_4}$$

### Equation 4

ACS1 and ACS2 are off

$$V_3 = V_{CC}$$

The tolerance of the resistors (R<sub>1</sub>, R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub>), the STCC08 output AVF signal electrical dispersion and the DC power supply characteristics induce a dispersion on V<sub>0</sub>, V<sub>1</sub>, V<sub>2</sub> and V<sub>3</sub> levels (see [Table 2](#)).

**Table 2. Variation of the V<sub>STATE</sub> signal according to the AC switch states**

ACS1 state	ACS2 state	V <sub>STATE</sub> status
ON	ON	V <sub>0_Min</sub> < V <sub>STATE</sub> < V <sub>0_Max</sub>
ON	OFF	V <sub>1_Min</sub> < V <sub>STATE</sub> < V <sub>1_Max</sub>
OFF	ON	V <sub>2_Min</sub> < V <sub>STATE</sub> < V <sub>2_Max</sub>
OFF	OFF	V <sub>3_Max</sub> > V <sub>STATE</sub> > V <sub>3_Min</sub>

Knowing the previous equations [1](#), [2](#), [3](#) and [4](#), the resistors standard value and the tolerance of the resistors, V<sub>x\_Max</sub> and V<sub>x\_Min</sub> (x = 0, 1, 2, or 3) values are defined respectively by equations [5](#), [6](#), [7](#), [8](#), [9](#), [10](#), [11](#) and [12](#).

$V_{CC\_Min}$  and  $V_{CC\_Max}$  are respectively the minimum and maximum power supply voltage of the application.  $X_{R\_Max}$  and  $X_{R\_Min}$  are the tolerances of the resistors. For example, with 5% resistor tolerance  $X_{R\_Max}$  and  $X_{R\_Min}$  are respectively 1.05 and 0.95.  $V_{AVF\_L\_Max}$  and  $V_{AVF\_L\_Min}$  values are fixed by the STCC08 AVF output electrical dispersion at low level with:

$$V_{AVF\_L\_Max} = V_{AVF1\_L\_Max} = V_{AVF2\_L\_Max} = 1 \text{ V}$$

and

$$V_{AVF\_L\_Min} = V_{AVF1\_L\_Min} = V_{AVF2\_L\_Min} = 0 \text{ V}$$

### Equation 5

ASC1 is on and ACS2 is on.

$$V_{0\_Max} = V_{AVF\_L\_Max} \cdot \frac{(R_2 + R_4) \cdot X_{R\_Max}}{(R_2 + R_4) \cdot X_{R\_Min}} = V_{AVF\_L\_Max} \cdot \frac{X_{R\_Max}}{X_{R\_Min}}$$

### Equation 6

ASC1 is on and ACS2 is on.

$$V_{0\_Min} = V_{AVF\_L\_Min} \cdot \frac{(R_2 + R_4) \cdot X_{R\_Min}}{(R_2 + R_4) \cdot X_{R\_Max}} = 0 \text{ V}$$

### Equation 7

ASC1 is on and ACS2 is off.

$$V_{1\_Max} = \frac{V_{CC\_Max} \cdot R_4 \cdot X_{R\_Max} + V_{AVF\_L\_Max} \cdot (R_1 + R_2) \cdot X_{R\_Max}}{(R_1 + R_2 + R_4) \cdot X_{R\_Min}}$$

### Equation 8

ASC1 is on and ACS2 is off.

$$V_{1\_Min} = \frac{V_{CC\_Min} \cdot R_4 \cdot X_{R\_Min} + V_{AVF\_L\_Min} \cdot (R_1 + R_2) \cdot X_{R\_Min}}{(R_1 + R_2 + R_4) \cdot X_{R\_Max}}$$

### Equation 9

ASC1 is off and ACS2 is on.

$$V_{2\_Max} = \frac{V_{CC\_Max} \cdot R_2 \cdot X_{R\_Max} + V_{AVF\_L\_Max} \cdot (R_3 + R_4) \cdot X_{R\_Max}}{(R_2 + R_3 + R_4) \cdot X_{R\_Min}}$$

**Equation 10**

ASC1 is off and ACS2 is on.

$$V_{2\_Min} = \frac{V_{CC\_Min} \cdot R_2 \cdot X_{R\_Min} + V_{AVF\_L\_Min} \cdot (R_3 + R_4) \cdot X_{R\_Min}}{(R_2 + R_3 + R_4) \cdot X_{R\_Max}}$$

**Equation 11**

ASC1 is off and ACS2 is off.

$$V_{3\_Max} = V_{CC\_Max}$$

**Equation 12**

ASC1 is off and ACS2 is off.

$$V_{3\_Min} = V_{CC\_Min}$$

### 3 Resistance settings

*Equation 13* shows how to select values for  $R_1$  and  $R_3$  resistances.  $I_{AVF\_Max}$  is the maximum current sunk by the STCC08 AVF pin and should be lower than 5 mA.

#### Equation 13

$$R_1 = R_3 = R \geq \frac{2 \cdot V_{CC\_Max}}{I_{AVF\_Max}}$$

Knowing the  $R_1$  and  $R_3$  resistor standard values, the tolerance of the resistors, the STCC08 AVF output electrical dispersion and the DC power supply characteristic,  $R_2$  and  $R_4$  resistances value should be chosen by using equations [14](#), [15](#), and [16](#) (see also [Appendix C](#)).

#### Equation 14

$$\Rightarrow V_{1\_Min} > V_{0\_Max}$$

$$\Rightarrow R_4 > \frac{(R + R_2) \cdot \left[ V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 - V_{AVF\_L\_Min} \right]}{V_{CC\_Min} - V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2}$$

#### Equation 15

$$\Rightarrow V_{2\_Min} > V_{1\_Max}$$

$$\Rightarrow R_4 < \frac{R_2 \cdot \left[ V_{CC\_Min} - V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 \right] - R \cdot \left[ V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 - V_{AVF\_L\_Min} \right]}{V_{CC\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 - V_{AVF\_L\_Min}}$$

#### Equation 16

$$\Rightarrow V_{3\_Min} > V_{2\_Max}$$

$$\Rightarrow R_4 > \frac{R_2 \cdot \left[ V_{CC\_Max} - V_{CC\_Min} \cdot \frac{X_{R\_Min}}{X_{R\_Max}} \right] - R}{V_{CC\_Min} \cdot \frac{X_{R\_Min}}{X_{R\_Max}} - V_{AVF\_L\_Max}}$$

**4****Detection windows digital value setting**

To detect the state of both AC switches, an MCU analog/digital converter input (ADC) should be used. The conversion result ( $N_{ADC}$ ) of the  $V_{STATE}$  signal depends on the ADC size (N) and of the MCU voltage reference ( $V_{Ref}$ ). Note that the ADC transfer function is considered as ideal (see [Equation 17](#)).

**Equation 17**

$$N_{ADC} = \frac{V_{STATE}}{V_{Ref}} \cdot 2^N$$

According to the state of the AC switches, the  $V_{STATE}$  signal is not directly dependent on the value of  $V_{CC}$  (see equations [1](#), [2](#) and [3](#)). This has an impact on the conversion result if the voltage reference of the ADC transfer function depends directly on  $V_{CC}$ . In this case, the detection levels to implement in the MCU firmware should be determined by taking into account the DC power supply variation with  $V_{REF} = V_{CC}$  (see equations [18](#), [19](#), [20](#), [21](#), [22](#), [23](#) and [24](#)).

**Equation 18**

ASC1 is on and ACS2 is on.

$$\left\{ \begin{array}{l} \Rightarrow N_0 = \frac{V_{AVF\_L}}{V_{CC}} \cdot \frac{(R_2 + R_4)}{(R_2 + R_4)} \cdot 2^N \\ \\ \Rightarrow N_{0\_Max} = \frac{V_{AVF\_L\_Max}}{V_{CC\_Min}} \cdot \frac{(R_2 + R_4) \cdot X_{R\_Max}}{(R_2 + R_4) \cdot X_{R\_Min}} \cdot 2^N = \frac{V_{AVF\_L\_Max}}{V_{CC\_Min}} \cdot \frac{X_{R\_Max}}{X_{R\_Min}} \cdot 2^N \end{array} \right.$$

**Equation 19**

ASC1 is on and ACS2 is off.

$$N_{0\_Min} = 0$$

**Equation 20**

ASC1 is on and ACS2 is off.

$$\left\{ \begin{array}{l} \Rightarrow N_1 = \left[ \frac{R_4 \cdot V_{CC} + V_{AVF\_L} \cdot (R_1 + R_2)}{V_{CC} \cdot (R_1 + R_2 + R_4)} \right] \cdot 2^N \\ \\ \Rightarrow N_{1\_Max} = \left[ R_4 + \frac{V_{AVF\_L\_Max} \cdot (R_1 + R_2)}{V_{CC\_Min}} \right] \cdot \frac{2^N \cdot X_{R\_Max}}{(R_1 + R_2 + R_4) \cdot X_{R\_Min}} \end{array} \right.$$

**Equation 21**

ASC1 is on and ACS2 is off.

$$\left\{ \begin{array}{l} \Rightarrow N_1 = \left[ \frac{R_4 \cdot V_{CC} + V_{AVF\_L} \cdot (R_1 + R_2)}{V_{CC} \cdot (R_1 + R_2 + R_4)} \right] \cdot 2^N \\ \\ \Rightarrow N_{1\_Min} = \left[ R_4 + \frac{V_{AVF\_L\_Min} \cdot (R_1 + R_2)}{V_{CC\_Max}} \right] \cdot \frac{2^N \cdot X_{R\_Min}}{(R_1 + R_2 + R_4) \cdot X_{R\_Max}} \end{array} \right.$$

**Equation 22**

ASC1 is off and ACS2 is on.

$$\left\{ \begin{array}{l} \Rightarrow N_2 = \left[ \frac{R_2 \cdot V_{CC} + V_{AVF\_L} \cdot (R_3 + R_4)}{V_{CC} \cdot (R_2 + R_3 + R_4)} \right] \cdot 2^N \\ \\ \Rightarrow N_{2\_Max} = \left[ R_2 + \frac{V_{AVF\_L\_Max} \cdot (R_3 + R_4)}{V_{CC\_Min}} \right] \cdot \frac{2^N \cdot X_{R\_Max}}{(R_2 + R_3 + R_4) \cdot X_{R\_Min}} \end{array} \right.$$

**Equation 23**

ASC1 is off and ACS2 is on.

$$\left\{ \begin{array}{l} \Rightarrow N_2 = \left[ \frac{R_2 \cdot V_{CC} + V_{AVF\_L} \cdot (R_3 + R_4)}{V_{CC} \cdot (R_2 + R_3 + R_4)} \right] \cdot 2^N \\ \\ \Rightarrow N_{1\_Min} = \left[ R_2 + \frac{V_{AVF\_L\_Min} \cdot (R_3 + R_4)}{V_{CC\_Max}} \right] \cdot \frac{2^N \cdot X_{R\_Min}}{(R_2 + R_3 + R_4) \cdot X_{R\_Max}} \end{array} \right.$$

**Equation 24**

ASC1 is off and ACS2 is off.

$$N_{3\_Max} = N_{3\_Min} > N_{2\_Max}$$

## 5 Application example

**Table 3. Defined values of the application**

Symbol	Value	Unit
I <sub>AVF_Max</sub>	5	mA
V <sub>CC_Min</sub>	4.5	V
V <sub>CC_Max</sub>	5.5	V
V <sub>AVF_L_Min</sub>	0	V
V <sub>AVF_L_Max</sub>	1	V
N (MCU ADC resolution)	10	bits

The first step is to calculate R<sub>1</sub> and R<sub>3</sub> resistor values using [Equation 13](#). The second step is to choose the R<sub>2</sub> and R<sub>4</sub> resistor values to fulfil equations [14](#) and [15](#) (see also [Table 4](#)).

**Table 4. R<sub>1</sub>, R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub> resistor values**

Resistor settings	Standard value (5% tolerance)
R <sub>1</sub> = R <sub>3</sub> > 1.1 kΩ	2.2 kΩ
R <sub>2</sub>	15 kΩ
R <sub>4</sub>	6.8 kΩ

The third step is to calculate the window detection levels (see [Table 5](#)) according to equations [5](#), [6](#), [7](#), [8](#), [9](#), [10](#), [11](#), [18](#), [19](#), [20](#), [21](#), [22](#), [23](#) and [24](#). The window detection digital levels will be stored in the MCU firmware to distinguish the state of each AC switch.

**Table 5. Detection window values**

Windows detection level	Analog values (Volts)		Equivalent digital values	
	Max.	Min.	Max.	Min.
V <sub>0</sub>	1.105	0	252	0
V <sub>1</sub>	2.514	1.154	501	262
V <sub>2</sub>	4.214	2.545	802	579
V <sub>3</sub>	5.5	4.5	1024	> 802

## 6 Conclusion

This application note illustrates how designers can diagnose the state of two AC switches with only one single microcontroller ADC input. The way to implement this solution in the application and the external resistor choice is described in this document.

This solution is used to detect the failure modes of two AC switches and to inform the MCU so that appropriate actions to put the system into a safe state can be taken. This function improves the system safety by detecting "diode mode" in both polarities of the AC mains, "short circuit" and "open circuit" of each AC switch independently.

The main benefit of this solution is to reduce the cost of the microcontroller when a platform needs to monitor several AC switches because it requires one less pin.

## Appendix A AC switch state deduction

**Table 6. AC switch states when IN1 = IN2 = 0**

IN1	IN2	V <sub>STATE</sub> value	ACS1 diagnostic	ACS2 diagnostic
0	0	V <sub>0</sub>	Shorted circuit	Shorted circuit
0	0	V <sub>1</sub>	Shorted circuit	OFF
0	0	V <sub>2</sub>	OFF	Shorted circuit
0	0	V <sub>3</sub>	OFF	OFF
0	0	Toggle between V <sub>3</sub> and V <sub>2</sub>	OFF	Diode mode
0	0	Toggle between V <sub>3</sub> and V <sub>1</sub>	Diode mode	OFF
0	0	Toggle between V <sub>3</sub> and V <sub>0</sub>	Diode mode	Diode mode
0	0	Toggle between V <sub>2</sub> and V <sub>1</sub>	Diode mode	Diode mode
0	0	Toggle between V <sub>2</sub> and V <sub>0</sub>	Diode mode	Shorted circuit
0	0	Toggle between V <sub>1</sub> and V <sub>0</sub>	Shorted circuit	Diode mode

**Table 7. AC switch states when IN1 = 0 and IN2 = 1**

IN1	IN2	V <sub>STATE</sub> value	ACS1 diagnostic	ACS2 diagnostic
0	1	V <sub>0</sub>	Shorted circuit	ON
0	1	V <sub>1</sub>	Shorted circuit	OPEN circuit
0	1	V <sub>2</sub>	OFF	ON
0	1	V <sub>3</sub>	OFF	OPEN circuit
0	1	Toggle between V <sub>3</sub> and V <sub>2</sub>	OFF	NA
0	1	Toggle between V <sub>3</sub> and V <sub>1</sub>	Diode mode	OPEN circuit
0	1	Toggle between V <sub>3</sub> and V <sub>0</sub>	Diode mode	NA
0	1	Toggle between V <sub>2</sub> and V <sub>1</sub>	Diode mode	NA
0	1	Toggle between V <sub>2</sub> and V <sub>0</sub>	Diode mode	ON
0	1	Toggle between V <sub>1</sub> and V <sub>0</sub>	Shorted circuit	NA

**Table 8. AC switch states when IN1 = 1 and IN2 = 0**

IN1	IN2	V <sub>STATE</sub> value	ACS1 diagnostic	ACS2 diagnostic
1	0	V <sub>0</sub>	ON	Shorted circuited
1	0	V <sub>1</sub>	ON	OFF
1	0	V <sub>2</sub>	Open circuit	Shorted circuited
1	0	V <sub>3</sub>	Open circuit	OFF
1	0	Toggle between V <sub>3</sub> and V <sub>2</sub>	Open circuit	Diode mode
1	0	Toggle between V <sub>3</sub> and V <sub>1</sub>	NA	OFF
1	0	Toggle between V <sub>3</sub> and V <sub>0</sub>	NA	Diode mode
1	0	Toggle between V <sub>2</sub> and V <sub>1</sub>	NA	Diode mode
1	0	Toggle between V <sub>2</sub> and V <sub>0</sub>	NA	Shorted circuit
1	0	Toggle between V <sub>1</sub> and V <sub>0</sub>	ON	Diode mode

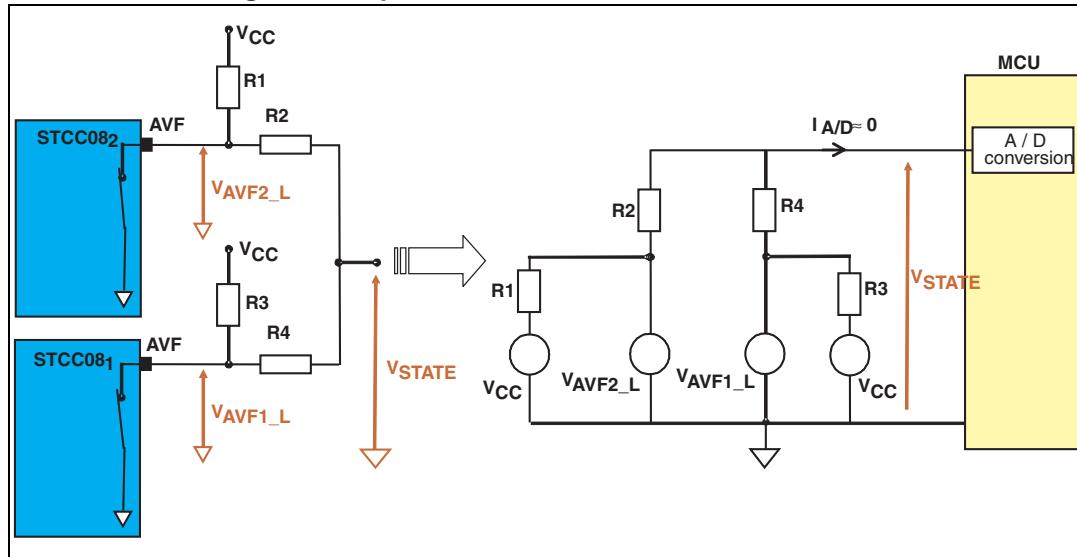
**Table 9. AC switch states when IN1 = IN2 = 1**

IN1	IN2	V <sub>STATE</sub> value	ACS1 diagnostic	ACS2 diagnostic
1	1	V <sub>0</sub>	ON	ON
1	1	V <sub>1</sub>	ON	OPEN circuit
1	1	V <sub>2</sub>	Open circuit	ON
1	1	V <sub>3</sub>	Open circuit	OPEN circuit
1	1	Toggle between V <sub>3</sub> and V <sub>2</sub>	Open circuit	NA
1	1	Toggle between V <sub>3</sub> and V <sub>1</sub>	NA	OPEN circuit
1	1	Toggle between V <sub>3</sub> and V <sub>0</sub>	NA	NA
1	1	Toggle between V <sub>2</sub> and V <sub>1</sub>	NA	NA
1	1	Toggle between V <sub>2</sub> and V <sub>0</sub>	NA	ON
1	1	Toggle between V <sub>1</sub> and V <sub>0</sub>	ON	NA

## Appendix B V<sub>STATE</sub> signal voltage definition

The V<sub>STATE</sub> voltage is defined according to the theorem of superposition applied on the linear circuits defined on Figures 14, 15, 16 and 17 (according to the state of each AC switch). The voltage resulting (V<sub>STATE</sub>) from each source is calculated separately, and the results are added algebraically. The input current of the MCU A/D conversion block (I<sub>A/D</sub>) is neglected.

**Figure 14. Equivalent circuit ACS1 and ACS2 are on**



**Equation 25**

$$V_{\text{STATE}} = V_0 = V_{\text{AVF1\_L}} \cdot V_{\text{AVF2\_L}} \cdot \frac{R_4}{R_4 + R_2}$$

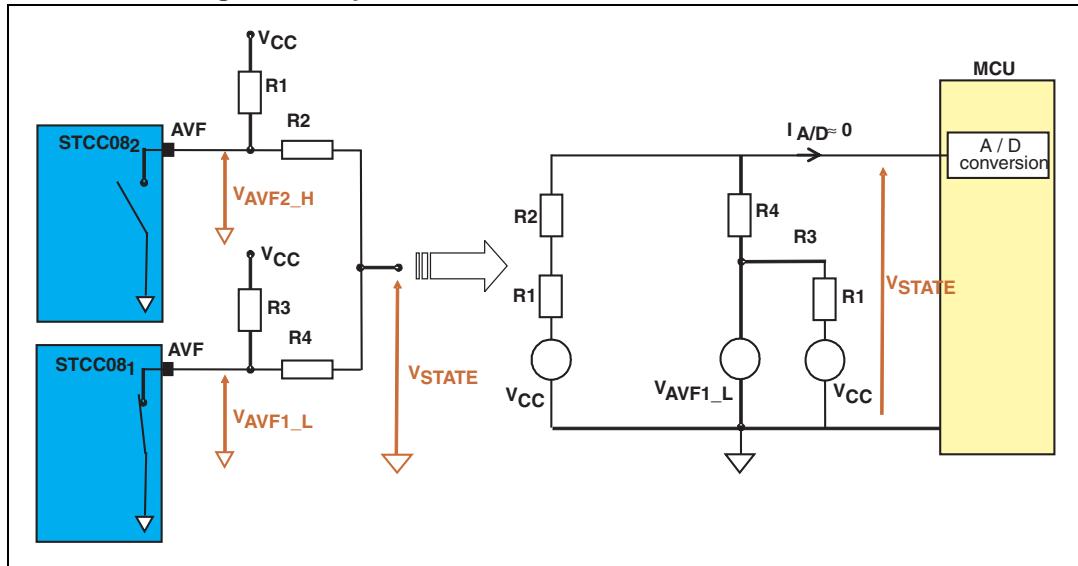
**Equation 26**

$$V_{0\text{-Max}} = V_{\text{AVF\_L\_Max}} \cdot \frac{(R_2 + R_4) \cdot X_{R\text{-Max}}}{(R_2 + R_4) \cdot X_{R\text{-Min}}}$$

**Equation 27**

$$V_{0\text{-Min}} = V_{\text{AVF\_L\_Min}} \cdot \frac{(R_2 + R_4) \cdot X_{R\text{-Min}}}{(R_2 + R_4) \cdot X_{R\text{-Max}}} = 0$$

Figure 15. Equivalent circuit ACS1 is on and ACS2 is off



Equation 28

$$V_{\text{STATE}} = V_1 = \frac{R_4}{R_4 + R_2 + R_1} \cdot V_{\text{CC}} + \frac{R_1 + R_2}{R_1 + R_2 + R_4} \cdot V_{\text{AVF1\_L}}$$

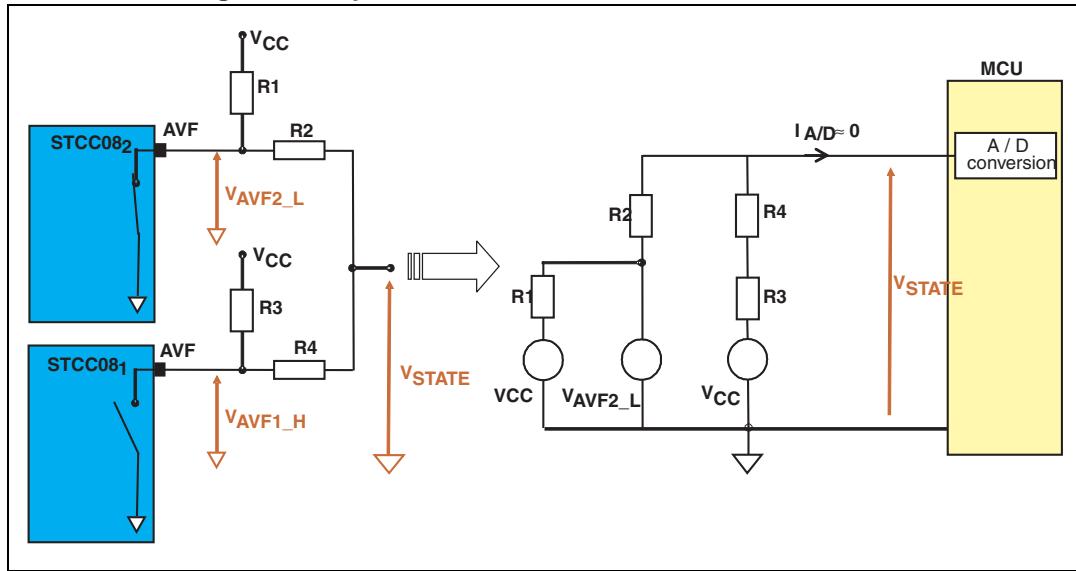
Equation 29

$$V_{1\text{-Max}} = \frac{V_{\text{CC\_Max}} \cdot R_4 \cdot X_{R\text{-Max}} + V_{\text{AVF\_L\_Max}} \cdot (R_1 + R_2) \cdot X_{R\text{-Max}}}{(R_1 + R_2 + R_4) \cdot X_{R\text{-Min}}}$$

Equation 30

$$V_{1\text{-Min}} = \frac{V_{\text{CC\_Min}} \cdot R_4 \cdot X_{R\text{-Min}} + V_{\text{AVF\_L\_Min}} \cdot (R_1 + R_2) \cdot X_{R\text{-Min}}}{(R_1 + R_2 + R_4) \cdot X_{R\text{-Max}}}$$

Figure 16. Equivalent circuit ACS2 is on and ACS1 is off

**Equation 31**

$$V_{\text{STATE}} = V_2 = \frac{R_2}{R_2 + R_4 + R_3} \cdot V_{\text{CC}} + \frac{R_3 + R_4}{R_3 + R_4 + R_2} \cdot V_{\text{AVF2\_L}}$$

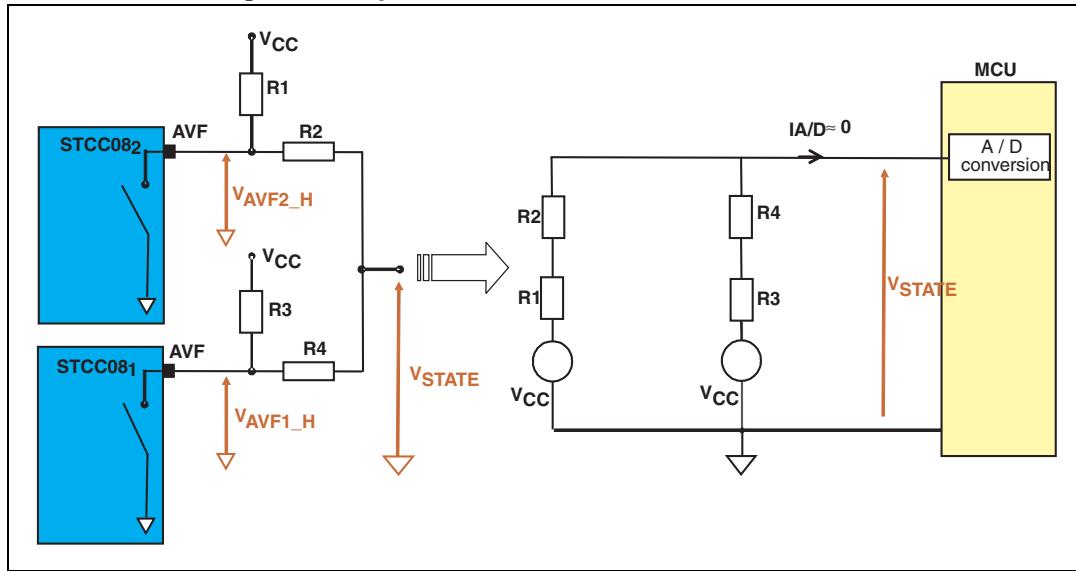
**Equation 32**

$$V_{2\text{-Max}} = \frac{V_{\text{CC\_Max}} \cdot R_2 \cdot X_{R\text{-Max}} + V_{\text{AVF\_L\_Max}} \cdot (R_3 + R_4) \cdot X_{R\text{-Max}}}{(R_2 + R_3 + R_4) \cdot X_{R\text{-Min}}}$$

**Equation 33**

$$V_{2\text{-Min}} = \frac{V_{\text{CC\_Min}} \cdot R_2 \cdot X_{R\text{-Min}} + V_{\text{AVF\_L\_Min}} \cdot (R_3 + R_4) \cdot X_{R\text{-Min}}}{(R_2 + R_3 + R_4) \cdot X_{R\text{-Max}}}$$

Figure 17. Equivalent circuit ACS1 and ACS2 are off



Equation 34

$$V_{\text{STATE}} = V_3 = V_{\text{CC}} \cdot \frac{R_3 + R_4}{R_1 + R_2 + R_3 + R_4} + V_{\text{CC}} \cdot \frac{R_1 + R_2}{R_1 + R_2 + R_3 + R_4} = V_{\text{CC}}$$

Equation 35

$$V_{3,\text{Max}} = V_{\text{CC},\text{Max}}$$

Equation 36

$$V_{3,\text{Min}} = V_{\text{CC},\text{Min}}$$

## Appendix C Resistor settings

*Figure 15*, and equations 37, 38 and 39 define conditions to identify the state of each AC switch.

### Equation 37

$$V_{1\_Min} > V_{0\_Max}$$

### Equation 38

$$V_{2\_Min} > V_{1\_Max}$$

### Equation 39

$$V_{2\_Max} < V_{3\_Min}$$

## C.1 First case: $V_{1\_Min} > V_{0\_Max}$

Equations 26 and 30 define respectively  $V_{0\_Max}$  and  $V_{1\_Min}$  (see *Appendix A*). To take into account  $R_1$  resistor's standardized values (see *Equation 13*), the resistor's tolerance ( $X_R$ ), the STCC08 AVF output electrical dispersion and the DC power supply characteristic, the condition on  $R_2$  and  $R_4$  resistors is defined in *Equation 42*.

### Equation 40

$$V_{1\_Min} > V_{0\_Max}$$

### Equation 41

$$\frac{V_{CC\_Min} \cdot R_4 \cdot X_{R\_Min} + V_{AVF\_L\_Min} \cdot \left( R_1 + R_2 \right) \cdot X_{R\_Min}}{\left( R_1 + R_2 + R_4 \right) \cdot X_{R\_Max}} > V_{AVF\_L\_Max}$$

### Equation 42

$$R_4 > \frac{\left( R_1 + R_2 \right) \cdot \left[ V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right) - V_{AVF\_L\_Min} \right]}{V_{CC\_Min} - V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)}$$

## C.2 Second case: $V_{2\_Min} > V_{1\_Max}$

Equations 29 and 33 define respectively  $V_{1\_Max}$  and  $V_{2\_Min}$  (see [Appendix A](#)). To take into account  $R_3$  resistor's standardized values, the resistor's tolerance ( $X_R$ ), the STCC08 AVF output electrical dispersion and the DC power supply characteristic, the condition on  $R_2$  and  $R_4$  resistors is defined by [Equation 46](#).

### Equation 43

$$V_{2\_Min} > V_{1\_Max}$$

### Equation 44

$$V_{2\_Min} = \frac{V_{CC\_Min} \cdot R_2 \cdot X_{R\_Min} + V_{AVF\_L\_Min} \cdot (R + R_4) \cdot X_{R\_Min}}{(R_2 + R_3 + R_4) \cdot X_{R\_Max}}$$

### Equation 45

$$V_{1\_Max} = \frac{V_{CC\_Max} \cdot R_4 \cdot X_{R\_Max} + V_{AVF\_L\_Max} \cdot (R_1 + R_2) \cdot X_{R\_Max}}{(R_1 + R_2 + R_4) \cdot X_{R\_Min}}$$

### Equation 46

$$R_4 < \frac{R_2 \cdot \left[ V_{CC\_Min} - V_{AVF\_L\_Max} \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 \right] - R_3 \cdot \left[ V_{AVF\_L\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 - V_{AVF\_L\_Min} \right]}{V_{CC\_Max} \cdot \left( \frac{X_{R\_Max}}{X_{R\_Min}} \right)^2 - V_{AVF\_L\_Min}}$$

### C.3 Third case: $V_{2\_Max} < V_{3\_Min}$

Equations 32 and 36 define respectively  $V_{2\_Max}$  and  $V_{3\_Min}$  (see [Appendix A](#)). To take into account  $R_3$  resistor's standardized values, the resistors' tolerance ( $X_R$ ), the STCC08 AVF output electrical dispersion and the DC power supply characteristic, the condition on  $R_2$  and  $R_4$  resistors is defined in [Equation 49](#).

#### Equation 47

$$V_{2\_Max} < V_{3\_Min}$$

#### Equation 48

$$\frac{V_{CC\_Max} \cdot R_2 \cdot X_{R\_Max} + V_{AVF\_L\_Max} \cdot (R_3 + R_4) \cdot X_{R\_Max}}{(R_2 + R_3 + R_4) \cdot X_{R\_Min}} < V_{CC\_Min}$$

#### Equation 49

$$R_4 > \frac{R_2 \cdot \left[ V_{CC\_Max} - V_{CC\_Min} \cdot \frac{X_{R\_Min}}{X_{R\_Max}} \right]}{V_{CC\_Min} \cdot \frac{X_{R\_Min}}{X_{R\_Max}} - V_{AVF\_L\_Max}} - R_3$$

## Revision history

**Table 10. Document revision history**

Date	Revision	Changes
08-Dec-2009	1	Initial release.
29-Jul-2014	2	Updated <a href="#">Figure 13</a> and the note below it.

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